NACA RM L56H22

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RESEARCH MEMORANDUM

PRESSURE DISTRIBUTIONS ON FOUR CANOPY-FUSELAGE CONFIGURATIONS AT TRANSONIC SPEEDS

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NATIONAL ADVISORY COMMITTEE
FOR AERONAUTICS

WASHINGTON

December 5, 1956
Declassified November 1, 1959

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SUMMARY

Pressure-distribution data have been obtained for a drooped-nose-fuselage forebody alone and for four canopy shapes mounted on this forebody. Two of the canopies had the same shape and size rearward of the windshield but one had a "flat" and the other a "vee" windshield. The remaining two canopies were located at different body stations, had smaller maximum cross-sectional areas, higher fineness ratios, and flat windshields. The models were tested at Mach numbers from 0.80 to 1.13 and at combined angles of attack and sideslip. The Reynolds number per foot varied from 3.54×10^6 to 3.87×10^6.

The data indicated that a flat-windshield canopy experienced lower pressures over a greater percentage of its projected frontal area than a comparable vee-windshield canopy. Localized regions of low pressure, however, were more severe for the vee-windshield canopy. Windshield shape had little effect on pressures measured over the rear one-third of the canopies. Integrated canopy pressure drag increments, which included only the interference of the fuselage on the canopy, were essentially the same for the small forward- and rearward-located canopies at the higher Mach numbers. However, comparison of the increments in canopy-plus-fuselage force data indicated that the interference of the canopy on the fuselage was principally responsible for higher drag due to the canopy in the rearward location.

INTRODUCTION

Among the problems associated with the design of piloted aircraft for flight in the transonic and supersonic speed ranges is that of determining the optimum shape and location of a cockpit canopy. Visibility requirement for take-off, landing, and combat purposes must be met with a minimum penalty in performance of the overall configuration. Sound structural desigr requires a knowledge of the magnitude and distribution of the aerodynamic

loads which would be expected to act upon the canopy during flight. A few papers presently available showing experimental pressure-distribution and drag results obtained in the transonic and supersonic speed ranges are listed in references 1 to 9.

In order to obtain additional aerodynamic data in the transonic and supersonic speed ranges, a series of airplane canopy models that simulate present designs used on high-speed aircraft were investigated at the Langley Laboratory. The objective of this program was to obtain force and pressure-distribution data for canopy-fuselage combinations and to evaluate the effects of changes in canopy shape, size, and location under various operating conditions of pitch, sideslip, and Mach number. Reported in reference 1 are the results of part of this program conducted in the Langley 4- by 4-foot supersonic pressure tunnel at Mach numbers of 1.41 and 2.01. Force and pressure measurements are presented for eight canopies mounted on a common drooped-nose-fuselage forebody. Reference 2 presents the results of force measurements on four of these canopies obtained in the Langley 8-foot transonic tunnel for a Mach number range from 0.80 to 1.13.

Reported herein are the pressure-distribution results obtained at transonic speeds for the fuselage forebody with and without the four canopy shapes tested in reference 2. The data presented supplement that of references 1 and 2. Two of the canopies were mounted well forward on the fuselage and had the same shape and size rearward of the windshield but one had a flat and the other a vee windshield. The two remaining canopies had smaller cross-sectional areas and higher fineness ratios than the first two and both had flat windshields. The two smaller canopies were located at different longitudinal positions on the fuselage.

The tests reported herein covered a Mach number range from 0.80 to 1.13, and angle-of-attack range from 0° to 10°, and an angle-of-sideslip range from -8° to 8°. The Reynolds number per foot varied from 3.54×10^6 to 3.87×10^6.

SYMBOLS

A_b	maximum cross-sectional area of fuselage forebody, 15.71 sq in.
A_{max}	maximum cross-sectional area of exposed canopy
a	major radius of fuselage cross-section ellipse
b	minor radius of fuselage cross-section ellipse, a/1.25

C_D drag coefficient, Drag/qA_b

$\Delta C_{D,A}$ incremental drag coefficient due to canopy, $\left(C_D - C_{D_{fuselage}}\right)\frac{A_b}{A_{max}}$

$\Delta C_{D,p}$ incremental pressure drag coefficient due to canopy obtained from pressure distributions (based on exposed canopy maximum cross-sectional area)

C_p local pressure coefficient, $\frac{p - p_o}{q}$

$C_{p,b}$ base-pressure coefficient, $\frac{p_b - p_o}{q}$

c major radius of canopy cross-section ellipse, measured from drooped center line of fuselage

d minor radius of canopy cross-section ellipse, c/2.5

h distance to top of round canopy, measured from straight center line of fuselage

l total canopy length

l_b total fuselage length, 25 inches

M free-stream Mach number

P.L. designation of canopy-fuselage parting line

p local static pressure

p_b static pressure at model base

p_o free-stream static pressure

q free-stream dynamic pressure

R Reynolds number per foot of length, $\rho V/\mu$

r radius of cross section of round canopy

u vertical coordinate of canopy cross section

v	horizontal coordinate of canopy cross section
V	free-stream velocity
x	distance measured from canopy nose along straight center line (positive rearward)
x_b	distance measured from fuselage nose along straight center line (positive rearward)
z	vertical distance from straight center line to drooped center line of fuselage (positive downward)
α	angle of attack, deg
β	angle of sideslip, deg
μ	free-stream viscosity
ρ	free-stream density
φ	lateral angle (positive when measured clockwise from plane of symmetry looking downstream)

APPARATUS AND INSTRUMENTATION

Tunnel

This investigation was conducted in the Langley 8-foot transonic tunnel, which has a dodecagonal slotted test section. This tunnel is capable of continuously variable operation through the speed range up to a Mach number of 1.15. The models were mounted in the tunnel on the conventional sting-support system. Detailed discussions of the design and calibration of this tunnel have been presented in references 10 and 11. The uniformity of the Mach number distribution in the model region is within ± 0.006.

Models

A drooped-nose-fuselage forebody and four canopy shapes mounted on this forebody were tested in this investigation. The dimensions of the models are presented in figure 1. These models were the same as those used and described in references 1 and 2. The fuselage forebody (fig. 1(a)) had elliptic cross sections throughout. The cross sections of canopies 1 and 2 (figs. 1(b) and 1(c)) behind the windshield were also

elliptic but canopy 1 had a flat windshield, whereas canopy 2 had a vee windshield. Both windshields were swept back 55° and the vee windshield had an opening angle of approximately 50°. Both canopies 1 and 2 were located well forward on the fuselage and had equivalent fineness ratios of approximately 7.0 (based on the ratio of the diameter of an equivalent body of revolution to the length of the canopy in the plane of symmetry). The ratio of the maximum cross-sectional area of canopies 1 and 2 to the maximum cross-sectional area of the fuselage was approximately 0.165. The method of derivation of the windshield shapes is illustrated in reference 1.

Canopies 3 and 4 (figs. 1(d) and 1(e)) had circular cross sections behind the windshield, lower windshield slopes, and were smaller in size. Both canopies had flat windshields swept back 65° but canopy 4 was located 3.75 inches farther downstream on the fuselage than canopy 3. The equivalent fineness ratio of canopy 3 was approximately 10.0, whereas that of canopy 4 was approximately 12.0. The ratio of the maximum cross-sectional area of the canopy to the maximum cross-sectional area of the fuselage was approximately 0.095 and 0.066 for canopies 3 and 4, respectively. Slight dissymmetry in construction of canopy 3 is indicated in figure 1(d) where the actual measured dimensions are presented.

Instrumentation

The location of pressure orifices on the five models used in this investigation is shown in figure 2. The fuselage alone was instrumented with two longitudinal rows of 21 orifices each, whereas each canopy had approximately 50 orifices. In all cases orifices were installed on only one side of the plane of symmetry so that both positive and negative sideslip angles were tested in order to determine the pressures on both the upstream and downstream sides of the model for a given sideslip angle. In general, the orifices were positioned so that pressure distributions could be obtained in two directions; laterally, for various model stations and longitudinally, in meridian planes. For each canopy, additional orifices were located near sharp breaks in the contour and along the parting line between canopy and fuselage. These orifices generally did not fall into the lateral and longitudinal pattern.

TESTS AND MEASUREMENTS

Tests

The five models were tested at stream Mach numbers of 0.80, 0.90, 0.95, 0.99, 1.02, 1.08, and 1.13. The maximum random error in measuring

stream Mach number is believed to be about 0.003. At each Mach number, the models were tested under conditions of combined pitch and sideslip which included angles of attack of approximately 0°, 5°, and 10° and angles of sideslip of approximately 0°, ±4°, and ±8°. The Reynolds number per foot varied from 3.54×10^6 to 3.87×10^6. (See fig. 3.)

Measurements

At each test point, canopy pressure distribution, model base pressure, and all pressure data relative to prevailing ambient test conditions were photographically recorded from multiple-tube manometers. The accuracy of measurement of the pressure coefficients reported herein is estimated to be within ±0.005. The matching of pressure distributions on the upstream and downstream sides of a canopy at a given angle of sideslip, however, is also subject to accumulative errors due to the accuracy of measurement and repeatability of Mach number, angle of attack, and angle of sideslip.

Figure 4 shows the variation of base-pressure coefficient with Mach number at approximately zero angle of attack and sideslip for the five models tested. A block of wood having the same cross-sectional shape as the model base and 1 foot long was fastened rigidly to the sting behind the model in order to reduce the flow expansion about the model base. The gap between the block of wood and the model was approximately 1/16 inch.

In order to facilitate sideslip-angle measurements, the model was rotated 90° before it was mounted on the sting-support system. The sideslip angle was then measured by an electrical strain-gage pendulum device mounted internally near the base of the support sting. Sting and model deflections occurring ahead of this point as a result of forces and moments acting on the model were determined from static tests. The corrections were applied to the indicated sideslip angle.

The angle of attack was obtained by inserting 0°-, 5°-, and 10°-bent couplings in the support sting. Corrections were applied for incremental change in angle of attack due to load. The maximum deflection due to load was approximately 0.3°. The angles of sideslip and attack reported herein are accurate within ±0.1°.

RESULTS AND DISCUSSION

The pressure-coefficient data for the five models tested are presented in tables I to V. These tables are arranged so that plots of pressure coefficient may be made longitudinally in meridian planes or laterally at a particular station. Since orifices were installed on only one side of the plane of symmetry of the models, both positive and negative sideslip angles

were tested in order to determine the pressures on both the upstream and downstream sides of the model for a given sideslip angle. Therefore, complete lateral plots can only be made for those conditions where the corresponding positive and negative sideslip angles are the same. Presented in figures 5 to 9 are representative plots of pressure coefficients against axial location along longitudinal meridians for all configurations.

Effect of Windshield Shape

Shown in figure 5 is a comparison of the pressure-coefficient distributions on the flat- and vee-windshield canopies 1 and 2 for representative conditions of pitch, sideslip, and Mach number. It can be seen that the pressure coefficients over the forward portion of the canopy were generally more positive for the vee than for the flat windshield. Moving downstream along a meridian line on the vee-windshield canopy, it can be seen that the pressure decreased gradually over the windshield and then showed a very rapid decrease to a very high, sharp suction pressure peak as the flow expanded about the downstream edges of the windshield which were located near the maximum cross-sectional area station. The pressure recovered very rapidly from the high suction peaks, however, and approached the free-stream value over the rear of the canopy. In the case of the flat windshield, the edges were located farther upstream. As a consequence, the flow expansion about the edges resulted in low pressures over a greater length of each meridian. The suction pressure peaks, which occurred at or near the maximum cross-sectional area station for both canopies, were generally much lower and less severe for the flat-windshield canopy. The pressure recovery downstream of the maximum-cross-sectional area station was gradual and the free-stream value was approached as in the case of the vee-windshield canopy. Windshield shape generally had little or no effect on the pressures over the rear one-third of the canopies.

The effect of the earlier flow expansion on the flat windshield is also shown in figures 10(a) and 10(b) where constant-pressure-coefficient contours are plotted on one-half the frontal projections of the flat- and vee-windshield canopies for Mach numbers of 0.80, 0.99, and 1.13. The flat windshield covered approximately one-third of the projected frontal area of the canopy, whereas the vee windshield covered approximately three-fourths. In a small region near the nose of the canopies, the pressure coefficients were more positive for the flat windshield but, over the much larger portion of frontal area, the vee windshield supported more positive pressure coefficients. The early flow expansion and resulting lower pressures over the frontal projection of the flat-windshield canopy indicate that it should have the drag advantage in this case. This is substantiated by force-data results obtained for these models and presented in references 1 and 2. Shown in figure 11 is a comparison of the drag of the models used in this investigation. This figure was taken from reference 2 and shows that the flat-windshield canopy 1 had consistently less drag than the

vee-windshield canopy 2 throughout the Mach number range. Comparison of somewhat different flat- and vee-windshield canopies in reference 4 showed greater drag for the flat windshields. In that case, however, the flat windshields contributed nearly all of the total canopy frontal area so that expansions around the windshield edges could not produce reductions in drag.

Effect of Canopy Location

Shown in figure 6 are the distributions of pressure coefficients along meridian lines for the forward-located and rearward-located small flat-windshield canopies 3 and 4. These curves show the general shape of the pressure variations in the axial direction for the two canopies at representative conditions of pitch, sideslip, and Mach number. It is obvious that the pressures acting on the frontal portion of the forward-located canopy 3 were considerably greater than those acting at corresponding points on the rearward canopy 4. (See also figs. 10(c) and 10(d).) However, because of differences in size and fineness ratio between the two canopies, these curves do not provide for an adequate evaluation of the effects of canopy location on the drag of the canopy-fuselage combinations.

In order to provide a better comparison of the drag of the two canopy positions, the pressure distributions over the front and rear exposed surfaces of the two canopies were integrated to determine an axial-force contribution. The pressure distributions obtained on the fuselage alone were then integrated over the area which would be covered by the canopies. This result was subtracted from the result of the canopy-exposed-surface integrations to produce an axial-force increment due to the canopy. The maximum cross-sectional areas of the canopies themselves (1.49 square inches for forward-located canopy 3 and 1.03 square inches for rearward-located canopy 4) were then used to convert the incremental forces to incremental drag coefficients due to the canopies. These results are plotted in figure 12 for Mach numbers of 0.80, 0.99, and 1.13. Also plotted in figure 12 are the incremental drag coefficients (based on canopy maximum cross-sectional area) taken from the force-data results of reference 2. The force-data results, which include all mutual interference effects between canopy and fuselage, indicate that the rearward canopy location produced the higher drag increment. The results of the pressure integrations, which include only the interference of the fuselage on the canopy, indicate that the pressure drag increments were essentially the same for the two positions except at a Mach number of 0.80 where the rearward-located canopy produced a somewhat lower pressure drag. It therefore appears that the interference of the canopy on the fuselage played a relatively large part in determining the total drag of the combination. By comparing the drag-coefficient increments obtained from force data with those obtained from pressure integrations for one particular canopy, it can be seen that, in the case of the forward-located canopy 3, the interference of the canopy on the fuselage was favorable at

all Mach numbers (ΔC_D was reduced), whereas, in the case of the rearward-located canopy 4, the interference of the canopy on the fuselage was apparently unfavorable at all Mach numbers (ΔC_D was increased). Although the present results were for canopies on a fuselage forebody, the results are consistent with the findings of reference 3 which shows that canopy-fuselage interference drag increases as the canopy is moved rearward to the maximum cross-sectional area station of a complete fuselage.

Effect of Mach Number

The effects of Mach number on the pressure coefficients of the canopies and fuselage are illustrated in figure 7. Increasing free-stream Mach number at transonic speeds produced small but consistent increases in pressure coefficient over the forward face of all the canopies tested. For the flat-windshield canopies (figs. 7(a), 7(c), and 7(d)), the suction pressure peaks rose and moved rearward slightly with increase in Mach number to about 0.90 or 0.95. As the Mach number was increased further to 1.13, the suction peaks remained in the vicinity of the maximum cross-sectional area station but their height was reduced consistently. For the vee-windshield canopy (fig. 7(b)), the sharp suction pressure peaks occurring over the upper portion of the canopy were highest at a Mach number of 0.80 and were lowered consistently with increase in Mach number to 1.13. For all canopies, the pressure recovery downstream of the maximum cross-sectional area station tended to become more gradual at the higher Mach numbers. Changes in Mach number had little effect on the level of pressures over the rear one-third of the canopies. Shown in figure 7(e) are the effects of Mach number on the pressure distribution over the fuselage alone.

Effect of Sideslip

The changes in longitudinal pressure-coefficient distributions due to sideslip are illustrated in figure 8. In these figures, negative sideslip angles indicate data that were measured on the windward side of the canopy, whereas positive sideslip angles indicate that measured on the leeward side. The effect of sideslip on the pressures on the windward side of all canopies was to increase the pressure over the forward portion and to reduce the pressure over the rearward portion. On the leeward side, rather large pressure reductions due to sideslip occurred over the forward portion of all canopies, whereas the pressures over the rear portion either remained the same or were slightly reduced because of the crossflow velocity increments. As to be expected at large sideslip on the leeward side, the vee-windshield canopy (fig. 8(b)) exhibited a localized region of low pressure just downstream of the sharp nose ($\varphi = 3^\circ$). On the leeward side, the flat-windshield canopies (figs. 8(a), 8(c), and 8(d)) showed rapid

expansion of the flow about the windshield edges with subsequent recompression immediately downstream. Shown in figure 8(e) are the effects of sideslip on the pressure distribution over the fuselage alone.

Effect of Angle of Attack

The effects of angle of attack on the longitudinal pressure distributions for the five models are illustrated in figure 9. At approximately zero sideslip, the effect of increasing angle of attack was to produce small reductions in pressure over the windshields and slightly higher suction pressure peaks over the upper portion of all canopies tested.

Under conditions of sideslip, the effect of increasing angle of attack on the pressures over the forward portion of the canopies was to reduce pressures on the windward side and to increase pressures on the leeward side particularly near the canopy-fuselage parting line. Pressures over the rear of the canopies either remained the same or were slightly reduced.

CONCLUSIONS

Pressure-distribution data have been obtained for a fuselage forebody alone and for four canopy shapes mounted on this forebody. The canopies, which varied in windshield shape, size, and location on the fuselage, were tested at Mach numbers from 0.80 to 1.13 and at combined angles of attack and sideslip. The Reynolds number per foot varied from 3.54×10^6 to 3.87×10^6. The data obtained indicated that:

1. The large forward-located flat-windshield canopy model used in this investigation experienced lower pressures over a greater percentage of its projected frontal area than the vee-windshield canopy.

2. The localized regions of low pressure produced by flow expansion about windshield edges were considerably more severe for the vee-windshield canopy. Lowest pressures occurred on the vee-windshield canopy at a Mach number of 0.80 and on the flat-windshield canopies at Mach numbers of 0.90 and 0.95.

3. Windshield shape had little effect on pressures measured over the rear one-third of the canopies.

4. Integrated canopy pressure drag increments, which included only the interference of the fuselage on the canopy, were essentially the same for the small forward- and rearward-located canopies at the higher Mach

numbers. However, comparison of the canopy-plus-fuselage force data indicated that the interference of the canopy on the fuselage was principally responsible for the higher drag due to the canopy in the rearward location.

Langley Aeronautical Laboratory,
National Advisory Committee for Aeronautics,
Langley Field, Va., July 31, 1956.

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TABLE I

PRESSURE COEFFICIENTS FOR FUSELAGE ALONE

(a) M = 0.80

ϕ, deg	Pressure coefficients for x_b/l_b of –																				
	0.160	0.200	0.240	0.280	0.320	0.360	0.400	0.440	0.480	0.520	0.560	0.600	0.640	0.680	0.720	0.760	0.800	0.840	0.880	0.920	0.960
$\alpha = -0.1^\circ$; $\beta = 0^\circ$																					
30.0	0.129	0.098	0.055	0.026	-0.030	-0.015	-0.060	-0.060	-0.064	-0.088	-0.081	-0.094	-0.079	-0.068	-0.036	-0.028	-0.017	-0.016	-0.018	-0.031	-0.039
00.0	.132	.106	.066	.040	.004	-.029	-.063	-.060	-.077	-.096	-.102	-.110	-.109	-.076	-.026	-.023	-.017	-.012	-.018	-.011	-.032
$\alpha = -0.1^\circ$; $\beta = -4.2^\circ$																					
30.0	0.147	0.125	0.086	0.054	-0.002	0.017	-0.038	-0.045	-0.062	-0.089	-0.090	-0.099	-0.073	-0.066	-0.040	-0.033	-0.023	-0.025	-0.024	-0.037	-0.043
00.0	.117	.090	.049	.028	-.014	-.045	-.081	-.078	-.089	-.096	-.110	-.119	-.132	-.100	-.052	-.045	-.038	-.032	-.035	-.030	-.049
-30.0	.085	.052	.006	-.015	-.038	-.040	-.083	-.071	-.088	-.116	-.105	-.111	-.093	-.079	-.046	-.036	-.025	-.024	-.024	-.035	-.043
$\alpha = -0.1^\circ$; $\beta = -8.4^\circ$																					
30.0	0.130	0.122	0.093	0.061	0.009	0.027	-0.032	-0.039	-0.060	-0.091	-0.093	-0.102	-0.084	-0.085	-0.061	-0.055	-0.046	-0.049	-0.048	-0.062	-0.065
00.0	.066	.037	-.000	-.020	-.050	-.075	-.124	-.113	-.138	-.141	-.167	-.173	-.189	-.155	-.107	-.098	-.090	-.083	-.084	-.076	-.092
-30.0	-.011	-.038	-.083	-.070	-.117	-.113	-.147	-.132	-.146	-.167	-.152	-.148	-.125	-.105	-.071	-.058	-.047	-.044	-.044	-.052	-.062
$\alpha = 5.1^\circ$; $\beta = 0^\circ$																					
30.0	0.061	0.044	0.008	-0.015	-0.027	-0.031	-0.077	-0.066	-0.081	-0.109	-0.103	-0.111	-0.090	-0.074	-0.047	-0.037	-0.028	-0.027	-0.026	-0.036	-0.045
00.0	.058	.043	.007	-.018	-.046	-.072	-.097	-.089	-.082	-.088	-.108	-.111	-.107	-.074	-.031	-.021	-.017	-.011	-.016	-.012	-.031
$\alpha = 5.1^\circ$; $\beta = -4.2^\circ$																					
30.0	0.065	0.056	0.024	0.009	-0.026	-0.016	-0.078	-0.071	-0.087	-0.122	-0.117	-0.133	-0.117	-0.105	-0.079	-0.069	-0.062	-0.061	-0.060	-0.069	-0.074
00.0	.040	.025	-.011	-.010	-.047	-.073	-.115	-.099	-.118	-.121	-.137	-.136	-.133	-.099	-.057	-.044	-.038	-.032	-.034	-.032	-.048
-30.0	.027	.008	-.022	-.024	-.058	-.052	-.095	-.083	-.094	-.117	-.105	-.106	-.084	-.064	-.036	-.025	-.017	-.017	-.018	-.024	-.036
$\alpha = 5.1^\circ$; $\beta = -8.4^\circ$																					
30.0	0.044	0.041	0.012	-0.001	-0.035	-0.027	-0.095	-0.088	-0.104	-0.143	-0.142	-0.165	-0.150	-0.143	-0.121	-0.114	-0.106	-0.105	-0.100	-0.112	-0.112
00.0	-.002	-.027	-.060	-.060	-.103	-.125	-.168	-.151	-.170	-.169	-.188	-.184	-.183	-.146	-.102	-.086	-.075	-.063	-.063	-.056	-.067
-30.0	-.047	-.046	-.083	-.078	-.107	-.109	-.135	-.119	-.126	-.139	-.124	-.118	-.094	-.071	-.046	-.037	-.032	-.034	-.036	-.047	-.060
$\alpha = 10.2^\circ$; $\beta = 0^\circ$																					
30.0	-0.001	-0.009	-0.031	-0.044	-0.074	-0.068	-0.116	-0.107	-0.112	-0.139	-0.129	-0.132	-0.109	-0.092	-0.062	-0.051	-0.042	-0.044	-0.044	-0.046	-0.057
00.0	-.003	-.011	-.040	-.043	-.065	-.091	-.129	-.100	-.111	-.112	-.120	-.110	-.102	-.065	-.028	-.019	-.017	-.015	-.014	-.011	-.025
$\alpha = 10.2^\circ$; $\beta = -4.2^\circ$																					
30.0	-0.007	-0.011	-0.038	-0.064	-0.090	-0.085	-0.140	-0.133	-0.140	-0.177	-0.166	-0.178	-0.153	-0.139	-0.112	-0.099	-0.089	-0.089	-0.082	-0.085	-0.089
00.0	-.016	-.027	-.058	-.062	-.088	-.112	-.150	-.123	-.133	-.134	-.142	-.129	-.119	-.082	-.048	-.040	-.039	-.037	-.039	-.038	-.054
-30.0	-.020	-.014	-.040	-.052	-.075	-.074	-.111	-.098	-.103	-.123	-.107	-.108	-.083	-.065	-.036	-.026	-.018	-.021	-.021	-.027	-.038
$\alpha = 10.2^\circ$; $\beta = -8.4^\circ$																					
30.0	-0.043	-0.035	-0.067	-0.092	-0.118	-0.115	-0.178	-0.169	-0.176	-0.218	-0.209	-0.229	-0.206	-0.193	-0.170	-0.158	-0.151	-0.147	-0.136	-0.139	-0.138
00.0	-.052	-.071	-.101	-.102	-.134	-.153	-.192	-.165	-.173	-.167	-.175	-.158	-.144	-.103	-.071	-.062	-.060	-.057	-.055	-.050	-.060
-30.0	-.074	-.068	-.094	-.098	-.112	-.116	-.132	-.120	-.123	-.132	-.117	-.114	-.086	-.068	-.043	-.030	-.019	-.020	-.012	-.026	-.029

TABLE I.- Continued

PRESSURE COEFFICIENTS FOR FUSELAGE ALONE

(b) M = 0.90

ϕ, deg	Pressure coefficients for x_b/l_b of –																				
	0.160	0.200	0.240	0.280	0.320	0.360	0.400	0.440	0.480	0.520	0.560	0.600	0.640	0.680	0.720	0.760	0.800	0.840	0.880	0.920	0.960
$\alpha = -0.1^\circ$; $\beta = 0^\circ$																					
30.0	0.138	0.108	0.060	0.024	-0.032	-0.017	-0.070	-0.072	-0.090	-0.115	-0.104	-0.120	-0.099	-0.079	-0.041	-0.030	-0.019	-0.020	-0.022	-0.034	-0.044
00.0	.146	.120	.074	.044	.004	-.032	-.072	-.068	-.087	-.117	-.122	-.145	-.137	-.087	-.021	-.021	-.018	-.015	-.023	-.016	-.040
$\alpha = -0.1^\circ$; $\beta = -4.2^\circ$																					
30.0	0.161	0.137	0.095	0.057	-0.004	0.016	-0.046	-0.053	-0.077	-0.106	-0.109	-0.130	-0.112	-0.077	-0.042	-0.034	-0.024	-0.026	-0.028	-0.040	-0.049
00.0	.135	.109	.064	.035	-.010	-.045	-.087	-.082	-.096	-.114	-.126	-.144	-.152	-.106	-.050	-.041	-.036	-.032	-.037	-.032	-.053
-30.0	.085	.055	.004	-.022	-.047	- 046	-.101	-.087	-.114	-.148	-.137	-.142	-.116	-.092	-.052	-.041	-.029	-.029	-.031	-.041	-.055
$\alpha = -0.1^\circ$; $\beta = -8.5^\circ$																					
30.0	0.147	0.136	0.102	0.068	0.010	0.029	-0.038	-0.046	-0.069	-0.105	-0.112	-0.132	-0.111	-0.096	-0.068	-0.060	-0.051	-0.053	-0.050	-0.065	-0.069
00.0	.084	.055	.014	-.013	-.049	-.073	-.133	-.122	-.147	-.155	-.182	-.196	-.214	-.165	-.110	-.097	-.090	-.085	-.087	-.079	-.099
-30.0	-.003	-.031	-.079	-.075	-.129	-.122	-.168	-.152	-.176	-.201	-.185	-.178	-.147	-.117	-.077	-.065	-.054	-.052	-.055	-.063	-.076
$\alpha = 5.1^\circ$; $\beta = 0^\circ$																					
30.0	0.073	0.055	0.016	-0.013	-0.033	-0.032	-0.088	-0.077	-0.096	-0.131	-0.121	-0.134	-0.108	-0.084	-0.050	-0.038	-0.030	-0.029	-0.030	-0.040	-0.052
00.0	.072	.057	.015	-.015	-.045	-.078	-.108	-.098	-.095	-.109	-.128	-.137	-.127	-.083	-.034	-.022	-.020	-.016	-.020	-.019	-.041
$\alpha = 5.1^\circ$; $\beta = -4.2^\circ$																					
30.0	0.079	0.073	0.036	0.013	-0.027	-0.015	-0.085	-0.079	-0.096	-0.136	-0.131	-0.153	-0.132	-0.111	-0.079	-0.068	-0.060	-0.059	-0.058	-0.068	-0.077
00.0	.060	.043	.003	-.004	-.042	-.072	-.119	-.104	- 121	-.132	-.148	-.154	-.144	-.102	-.055	-.040	-.035	-.031	-.035	-.033	-.054
-30.0	.033	.019	-.013	-.025	-.065	-.056	-.110	-.099	-.114	-.140	-.127	-.130	-.099	-.073	-.039	-.027	-.019	-.020	-.022	-.031	-.044
$\alpha = 5.1^\circ$; $\beta = -8.5^\circ$																					
30.0	0.061	0.055	0.020	0.002	-0.036	-0.025	-0.107	-0.100	-0.115	-0.164	-0.161	-0.192	-0.174	-0.159	-0.132	-0.121	-0.114	-0.111	-0.107	-0.119	-0.124
00.0	.013	-.014	-.051	-.057	-.105	-.132	-.183	-.166	-.186	-.193	-.211	-.212	-.206	-.157	-.106	-.088	- 078	-.068	- 067	-.060	- 075
-30.0	-.040	-.036	-.080	-.084	-.120	-.117	-.154	-.139	-.152	-.168	-.151	-.143	-.111	-.082	-.054	-.043	-.040	-.043	-.048	-.062	-.078
$\alpha = 10.2^\circ$; $\beta = 0^\circ$																					
30.0	0.009	0.001	-0.024	-0.042	-0.079	-0.068	-0.124	-0.116	-0.123	-0.152	-0.140	-0.146	-0.116	-0.090	-0.058	-0.046	-0.039	-0.039	-0.038	-0.045	-0.061
00.0	.009	.000	-.033	-.040	-.063	-.096	-.141	-.111	-.124	-.134	-.139	-.130	-.116	-.072	-.031	-.019	-.021	-.018	-.017	-.015	- 031
$\alpha = 10.2^\circ$; $\beta = -4.2^\circ$																					
30.0	0.016	0.008	-0.025	-0.052	-0.088	-0.078	-0.145	-0.134	-0.142	-0.179	-0.168	-0.184	-0.154	-0.127	-0.097	-0.084	-0.077	-0.073	-0.067	-0.073	-0.084
00.0	.009	-.002	-.039	-.051	-.077	-.105	-.151	-.122	-.134	-.142	-.149	-.141	-.124	-.080	-.044	-.032	-.034	-.036	-.039	-.038	-.056
-30.0																					
$\alpha = 10.2^\circ$; $\beta = -8.5^\circ$																					
30.0	-0.017	-0.015	-0.053	-0.081	-0.117	-0.110	-0.181	-0.173	-0.179	-0.223	-0.213	-0.241	-0.212	-0.186	-0.160	-0.148	-0.140	-0.134	-0.121	-0.129	-0.132
00.0	-.027	-.043	-.080	-.090	-.123	-.146	-.193	-.166	-.176	-.176	-.186	-.172	-.149	-.104	-.070	-.058	-.057	-.057	-.055	-.052	-.067
-30.0	-.063	-.056	-.090	-.102	-.123	-.120	-.148	-.138	-.145	-.160	-.146	-.137	-.104	-.079	-.048	-.033	-.021	-.025	-.017	-.030	-.034

TABLE I.- Continued

PRESSURE COEFFICIENTS FOR FUSELAGE ALONE

(c) M = 0.95

ø, deg	Pressure coefficients for x_b/l_b of —																				
	0.160	0.200	0.240	0.280	0.320	0.360	0.400	0.440	0.480	0.520	0.560	0.600	0.640	0.680	0.720	0.760	0.800	0.840	0.880	0.920	0.960
$\alpha = -0.1^\circ$; $\beta = 0^\circ$																					
30.0	0.159	0.131	0.080	0.040	-0.026	-0.007	-0.074	-0.074	-0.107	-0.133	-0.133	-0.153	-0.157	-0.111	-0.027	-0.026	-0.017	-0.021	-0.025	-0.036	-0.046
00.0	.159	.132	.083	.049	.006	-.032	-.083	-.075	-.100	-.139	-.147	-.173	-.202	-.130	.000	-.017	-.019	-.017	-.026	-.021	-.045
$\alpha = -0.1^\circ$; $\beta = -4.3^\circ$																					
30.0	0.173	0.150	0.105	0.065	-0.001	0.020	-0.052	-0.061	-0.085	-0.122	-0.138	-0.165	-0.176	-0.146	-0.026	-0.035	-0.027	-0.033	-0.035	-0.049	-0.052
00.0	.142	.113	.067	.033	-.015	-.051	-.105	-.100	-.118	-.153	-.175	-.184	-.226	-.148	-.045	-.045	-.046	-.040	-.048	-.042	-.067
-30.0	.107	.075	.021	-.013	-.040	-.045	-.109	-.086	-.128	-.164	-.150	-.175	-.173	-.102	-.044	-.036	-.027	-.031	-.034	-.045	-.062
$\alpha = -0.1^\circ$; $\beta = -8.5^\circ$																					
30.0	0.162	0.149	0.113	0.074	0.010	0.032	-0.043	-0.058	-0.077	-0.120	-0.140	-0.180	-0.180	-0.155	-0.070	-0.061	-0.053	-0.059	-0.059	-0.071	-0.072
00.0	.097	.066	.022	-.008	-.053	-.075	-.150	-.144	-.157	-.179	-.218	-.250	-.271	-.212	-.104	-.099	-.098	-.092	-.098	-.088	-.112
-30.0	.021	-.007	-.058	-.063	-.121	-.121	-.177	-.140	-.187	-.232	-.199	-.211	-.193	-.114	-.066	-.058	-.049	-.050	-.053	-.064	-.087
$\alpha = 5.1^\circ$; $\beta = 0^\circ$																					
30.0	0.087	0.069	0.024	-0.009	-0.032	-0.030	-0.100	-0.086	-0.107	-0.150	-0.148	-0.176	-0.161	-0.097	-0.050	-0.038	-0.032	-0.035	-0.037	-0.048	-0.066
00.0	.084	.068	.022	-.012	-.043	-.078	-.121	-.105	-.107	-.131	-.149	-.183	-.184	-.086	-.031	-.019	-.021	-.020	-.026	-.025	-.054
$\alpha = 5.1^\circ$; $\beta = -4.3^\circ$																					
30.0	0.094	0.087	0.047	0.023	-0.025	-0.009	-0.095	-0.090	-0.107	-0.154	-0.163	-0.195	-0.182	-0.140	-0.078	-0.067	-0.063	-0.065	-0.065	-0.074	-0.088
00.0	.071	.053	.010	.002	-.039	-.075	-.136	-.115	-.133	-.161	-.178	-.200	-.208	-.109	-.054	-.040	-.038	-.035	-.040	-.041	-.069
-30.0	.053	.035	.001	-.018	-.061	-.051	-.119	-.100	-.133	-.160	-.148	-.176	-.141	-.078	-.038	-.025	-.020	-.023	-.027	-.036	-.056
$\alpha = 5.1^\circ$; $\beta = -8.5^\circ$																					
30.0	0.076	0.071	0.032	0.008	-0.036	-0.023	-0.114	-0.117	-0.127	-0.178	-0.198	-0.237	-0.219	-0.217	-0.127	-0.118	-0.116	-0.120	-0.115	-0.124	-0.132
00.0	.029	.001	-.043	-.052	-.102	-.134	-.199	-.183	-.194	-.219	-.248	-.259	- 267	-.171	-.101	-.086	-.080	-.071	-.071	-.069	-.091
-30.0	-.023	-.020	-.069	-.078	-.119	-.115	-.170	-.140	-.171	-.201	-.175	-.186	-.141	-.084	-.052	-.043	-.041	-.046	-.054	-.071	-.093
$\alpha = 10.2^\circ$; $\beta = 0^\circ$																					
30.0	0.024	0.013	-0.017	-0.039	-0.081	-0.065	-0.137	-0.129	-0.137	-0.170	-0.179	-0.205	-0.156	-0.103	-0.058	-0.047	-0.043	-0.048	-0.049	-0.056	-0.080
00.0	.022	.013	-.023	-.034	-.058	-.098	-.155	-.119	-.135	-.153	-.169	-.184	-.147	-.072	-.027	-.016	-.020	-.020	-.021	-.022	-.043
$\alpha = 10.2^\circ$; $\beta = -4.3^\circ$																					
30.0	0.029	0.021	-0.017	-0.054	-0.095	-0.080	-0.161	-0.160	-0.165	-0.206	-0.222	-0.254	-0.212	-0.168	-0.103	-0.092	-0.089	-0.091	-0.085	-0.089	-0.107
00.0	.020	.006	-.038	-.051	-.080	-.119	-.176	-.141	-.154	-.174	-.194	-.202	-.163	-.089	-.049	-.040	-.044	-.045	-.051	-.055	-.079
-30.0	.004	.016	-.029	-.053	-.089	-.075	-.135	-.119	-.144	-.160	-.159	-.180	-.122	-.074	-.036	-.025	-.021	-.027	-.030	-.039	-.058
$\alpha = 10.2^\circ$; $\beta = -8.5^\circ$																					
30.0	-0.014	-0.007	-0.050	-0.090	-0.129	-0.121	-0.204	-0.215	-0.210	-0.254	-0.286	-0.318	-0.292	-0.271	-0.174	-0.165	-0.163	-0.163	-0.147	-0.148	-0.162
00.0	-.027	-.042	-.088	-.096	-.135	-.169	-.233	-.196	-.201	-.225	-.243	-.245	-.210	-.127	-.086	-.078	-.077	-.071	-.069	-.071	-.089
-30.0	-.037	-.031	-.072	-.088	-.118	-.109	-.159	-.136	-.164	-.182	-.168	-.183	-.124	-.079	-.045	-.031	-.022	-.028	-.022	-.037	-.048

TABLE I.- Continued

PRESSURE COEFFICIENTS FOR FUSELAGE ALONE

(d) M = 0.99

∅, deg	Pressure coefficients for x_b/l_b of —																				
	0.160	0.200	0.240	0.280	0.320	0.360	0.400	0.440	0.480	0.520	0.560	0.600	0.640	0.680	0.720	0.760	0.800	0.840	0.880	0.920	0.960
$\alpha = -0.1^\circ$; $\beta = 0^\circ$																					
30.0	0,178	0.149	0.096	0.050	-0.008	0.002	-0.064	-0.073	-0.104	-0.132	-0.143	-0.159	-0.165	-0.187	-0.140	-0.116	-0.077	-0.061	-0.047	-0.011	-0.003
00.0	.184	.159	.109	.069	.026	-.008	-.065	-.073	-.082	-.125	-.146	-.180	-.205	-.200	-.169	-.125	-.064	-.053	-.049	.008	.002
$\alpha = -0.1^\circ$; $\beta = -4.3^\circ$																					
30.0	0.197	0.173	0.126	0.078	0.017	0.033	-0.037	-0.052	-0.090	-0.114	-0.134	-0.161	-0.182	-0.202	-0.170	-0.126	-0.090	-0.075	-0.057	-0.021	-0.005
00.0	.172	.146	.098	.058	.009	-.022	-.079	-.089	-.109	-.139	-.159	-.188	-.222	-.217	-.168	-.123	-.096	-.073	-.060	-.006	-.018
-30.0	.122	.093	.039	-.003	-.019	-.043	-.104	-.092	-.116	-.169	-.167	-.189	-.193	-.209	-.159	-.122	-.088	-.069	-.055	-.025	-.025
$\alpha = -0.1^\circ$; $\beta = -8.6^\circ$																					
30.0	0.186	0.175	0.137	0.093	0.028	0.046	-0.023	-0.040	-0.086	-0.109	-0.138	-0.163	-0.192	-0.212	-0.179	-0.163	-0.132	-0.111	-0.089	-0.037	-0.020
00.0	.126	.098	.054	.018	-.044	-.050	-.124	-.123	-.158	-.164	-.200	-.237	-.277	-.279	-.229	-.187	-.155	-.127	-.098	-.040	-.063
-30.0	.035	.010	-.036	-.055	-.094	-.137	-.166	-.156	-.177	-.233	-.222	-.238	-.238	-.239	-.184	-.141	-.108	-.085	-.060	-.040	-.060
$\alpha = 5.1^\circ$; $\beta = 0^\circ$																					
30.0	0.108	0.091	0.045	0.006	-0.011	-0.011	-0.090	-0.085	-0.106	-0.138	-0.150	-0.177	-0.183	-0.193	-0.149	-0.119	-0.084	-0.061	-0.026	-0.010	-0.029
00.0	.107	.091	.045	.006	-.024	-.057	-.110	-.110	-.092	-.119	-.155	-.184	-.209	-.195	-.132	-.093	-.073	-.045	-.014	.005	-.023
$\alpha = 5.1^\circ$; $\beta = -4.3^\circ$																					
30.0	0.115	0.109	0.066	0.037	-0.006	0.008	-0.082	-0.086	-0.121	-0.144	-0.157	-0.191	-0.200	-0.219	-0.186	-0.160	-0.118	-0.095	-0.064	-0.034	-0.046
00.0	.097	.080	.036	.020	-.017	-.052	-.118	-.118	-.127	-.140	-.173	-.200	-.230	-.214	-.154	-.111	-.086	-.057	-.026	-.010	-.038
-30.0	.068	.055	.020	-.004	-.045	-.043	-.115	-.106	-.124	-.161	-.164	-.182	-.186	-.185	-.137	-.102	-.071	-.048	-.018	-.008	-.030
$\alpha = 5.1^\circ$; $\beta = -8.6^\circ$																					
30.0	0.100	0.095	0.054	0.028	-0.010	-0.013	-0.096	-0.101	-0.140	-0.171	-0.189	-0.228	-0.247	-0.271	-0.252	-0.236	-0.188	-0.161	-0.127	-0.077	-0.086
00.0	.054	.028	-.017	-.030	-.098	-.114	-.175	-.181	-.204	-.204	-.237	-.265	-.298	-.282	-.217	-.163	-.123	-.085	-.054	-.038	-.064
-30.0	-.002	.007	-.043	-.065	-.093	-.109	-.157	-.146	-.164	-.200	-.193	-.206	-.206	-.193	-.144	-.110	-.082	-.060	-.042	-.050	-.075
$\alpha = 10.3^\circ$; $\beta = 0^\circ$																					
30.0	0.046	0.037	0.003	-0.022	-0.060	-0.034	-0.131	-0.125	-0.141	-0.172	-0.172	-0.201	-0.206	-0.200	-0.156	-0.122	-0.087	-0.069	-0.047	-0.031	-0.049
00.0	.046	.037	-.003	-.017	-.030	-.078	-.150	-.117	-.127	-.155	-.172	-.191	-.217	-.181	-.121	-.087	-.067	-.046	-.023	-.001	-.018
$\alpha = 10.3^\circ$; $\beta = -4.3^\circ$																					
30.0	0.055	0.047	0.008	-0.029	-0.069	-0.058	-0.140	-0.143	-0.169	-0.189	-0.194	-0.235	-0.238	-0.242	-0.205	-0.169	-0.123	-0.100	-0.071	-0.045	-0.063
00.0	.049	.037	-.010	-.026	-.046	-.087	-.155	-.136	-.143	-.161	-.180	-.198	-.224	-.191	-.135	-.100	-.079	-.061	-.042	-.025	-.046
-30.0	.024	.034	-.014	-.046	-.071	-.057	-.135	-.125	-.137	-.170	-.167	-.188	-.189	-.179	-.130	-.099	-.065	-.050	-.025	-.013	-.025
$\alpha = 10.3^\circ$; $\beta = -8.6^\circ$																					
30.0	0.011	0.020	-0.024	-0.072	-0.094	-0.113	-0.180	-0.194	-0.224	-0.251	-0.264	-0.311	-0.320	-0.341	-0.316	-0.278	-0.217	-0.193	-0.154	-0.094	-0.109
00.0	-.001	-.013	-.062	-.080	-.129	-.131	-.207	-.204	-.205	-.212	-.233	-.250	-.267	-.229	-.175	-.142	-.118	-.097	-.072	-.052	-.065
-30.0	-.026	-.015	-.058	-.088	-.094	-.096	-.150	-.146	-.159	-.187	-.185	-.204	-.203	-.190	-.142	-.107	-.067	-.051	-.010	-.004	-.008

TABLE I.- Continued

PRESSURE COEFFICIENTS FOR FUSELAGE ALONE

(e) M = 1.02

∅, deg	Pressure coefficients for x_b/l_b of –																				
	0.160	0.200	0.240	0.280	0.320	0.360	0.400	0.440	0.480	0.520	0.560	0.600	0.640	0.680	0.720	0.760	0.800	0.840	0.880	0.920	0.960
$\alpha = -0.1^\circ$; $\beta = 0^\circ$																					
30.0	0.212	0.184	0.132	0.081	0.023	0.022	-0.028	-0.041	-0.077	-0.110	-0.123	-0.147	-0.160	-0.181	-0.144	-0.124	-0.094	-0.083	-0.076	-0.082	-0.072
00.0	.214	.187	.137	.093	.040	.015	-.037	-.049	-.067	-.110	-.132	-.168	-.195	-.193	-.167	.131	-.087	-.072	-.075	-.062	-.068
$\alpha = -0.1^\circ$; $\beta = -4.3^\circ$																					
30.0	0.228	0.206	0.159	0.110	0.043	0.055	-0.006	-0.017	-0.061	-0.089	-0.112	-0.142	-0.169	-0.191	-0.165	-0.134	-0.102	-0.097	-0.086	-0.093	-0.081
00.0	.201	.174	.126	.084	.020	-.008	-.051	-.063	-.090	-.122	-.146	-.181	-.213	-.211	-.169	-.138	-.114	-.099	-.096	-.083	-.089
-30.0	.163	.133	.078	.035	-.006	-.025	-.059	-.059	-.090	-.141	-.141	-.166	-.172	-.191	-.154	-.127	-.099	-.088	-.082	-.085	-.084
$\alpha = -0.1^\circ$; $\beta = -8.6^\circ$																					
30.0	0.218	0.206	0.168	0.123	0.052	0.071	-0.005	-0.016	-0.058	-0.082	-0.117	-0.143	-0.177	-0.201	-0.176	-0.164	-0.145	-0.136	-0.120	-0.127	-0.110
00.0	.156	.126	.081	.046	-.027	-.045	-.110	-.097	-.137	-.147	-.189	-.230	-.272	-.277	-.237	-.209	-.176	-.160	-.153	-.138	-.141
-30.0	.071	.048	.003	-.020	-.100	-.107	-.135	-.126	-.147	-.205	-.198	-.218	-.219	-.226	-.181	-.148	-.123	-.108	-.102	-.104	-.114
$\alpha = 5.1^\circ$; $\beta = 0^\circ$																					
30.0	0.140	0.123	0.074	0.033	0.019	0.003	-0.060	-0.061	-0.095	-0.123	-0.136	-0.166	-0.172	-0.191	-0.156	-0.133	-0.106	-0.094	-0.087	-0.089	-0.092
00.0	.139	.121	.072	.031	-.005	-.024	-.079	-.090	-.084	-.105	-.143	-.171	-.199	-.190	-.139	-.104	-.090	-.072	-.070	-.066	-.083
$\alpha = 5.1^\circ$; $\beta = -4.3^\circ$																					
30.0	0.147	0.143	0.099	0.065	0.023	0.020	-0.053	-0.058	-0.100	-0.129	-0.146	-0.178	-0.191	-0.216	-0.190	-0.175	-0.144	-0.131	-0.121	-0.124	0.114
00.0	.126	.108	.063	.049	-.012	-.024	-.090	-.094	-.116	-.131	-.165	-.191	-.223	-.214	-.165	-.128	-.109	-.092	-.088	-.082	-.100
-30.0	.106	.090	.056	.022	-.009	-.023	-.078	-.079	-.103	-.137	-.144	-.166	-.169	-.178	-.137	-.111	-.088	-.077	-.072	-.075	-.087
$\alpha = 5.1^\circ$; $\beta = -8.6^\circ$																					
30.0	0.133	0.129	0.088	0.058	0.003	0.012	-0.073	-0.075	-0.120	-0.149	-0.174	-0.209	-0.229	-0.257	-0.247	-0.240	-0.208	-0.190	-0.175	-0.179	-0.159
00.0	.088	.063	.018	.000	-.079	-.097	-.147	-.150	-.184	-.187	-.223	-.250	-.284	-.276	-.222	-.177	-.151	-.128	-.120	-.111	-.128
-30.0	.032	.042	-.006	-.036	-.079	-.093	-.125	-.118	-.138	-.174	-.173	-.189	-.189	-.186	-.147	-.121	-.104	-.097	-.098	-.111	-.133
$\alpha = 10.2^\circ$; $\beta = 0^\circ$																					
30.0	0.078	0.069	0.033	-0.001	-0.033	-0.035	-0.105	-0.109	-0.132	-0.162	-0.170	-0.199	-0.206	-0.215	-0.175	-0.149	-0.118	-0.111	-0.107	-0.107	-0.120
00.0	.077	.067	.024	.005	-.024	-.048	-.119	-.106	-.113	-.137	-.160	-.178	-.204	-.179	-.129	-.100	-.090	-.077	-.074	-.073	-.091
$\alpha = 10.2^\circ$; $\beta = -4.3^\circ$																					
30.0	0.078	0.078	0.034	-0.016	-0.053	-0.056	-0.125	-0.133	-0.167	-0.195	-0.204	-0.244	-0.253	-0.274	-0.239	-0.212	-0.172	-0.161	-0.151	-0.145	-0.145
00.0	.070	.062	.008	-.012	-.055	-.074	-.138	-.131	-.141	-.159	-.182	-.200	-.225	-.198	-.151	-.124	-.114	-.104	-.106	-.108	-.129
-30.0	.061	.072	.026	-.013	-.034	-.038	-.103	-.102	-.117	-.149	-.153	-.175	-.178	-.180	-.138	-.114	-.089	-.083	-.083	-.085	-.099
$\alpha = 10.2^\circ$; $\beta = -8.6^\circ$																					
30.0	0.044	0.058	0.012	-0.039	-0.092	-0.086	-0.156	-0.163	-0.202	-0.233	-0.248	-0.291	-0.308	-0.333	-0.314	-0.289	-0.240	-0.226	-0.209	-0.199	-0.185
00.0	.030	.022	-.027	-.049	-.116	-.119	-.176	-.175	-.190	-.194	-.216	-.234	-.255	-.224	-.178	- 152	-.140	-.129	-.125	-.122	-.139
-30.0	.007	.020	-.023	-.061	-.075	-.088	-.123	-.120	-.135	-.165	-.167	-.186	- 187	-.183	-.143	-.116	-.084	-.079	-.065	-.077	-.081

TABLE I.- Continued

PRESSURE COEFFICIENTS FOR FUSELAGE ALONE

(f) M = 1.08

ø, deg	Pressure coefficients for x_b/l_b of —																				
	0.160	0.200	0.240	0.280	0.320	0.360	0.400	0.440	0.480	0.520	0.560	0.600	0.640	0.680	0.720	0.760	0.800	0.840	0.880	0.920	0.960
$\alpha = -0.1^\circ$; $\beta = 0^\circ$																					
30.0	0.211	0.198	0.155	0.109	0.023	0.035	-0.012	-0.020	-0.039	-0.073	-0.071	-0.096	-0.100	-0.129	-0.094	-0.079	-0.053	-0.040	-0.028	-0.032	-0.021
00.0	.218	.209	.168	.129	.061	.023	-.011	-.019	-.027	-.058	-.079	-.116	-.143	-.142	-.121	-.083	-.041	-.030	-.026	-.017	-.014
$\alpha = -0.1^\circ$; $\beta = -4.3^\circ$																					
30.0	0.234	0.225	0.186	0.138	0.061	0.067	0.014	0.003	-0.026	-0.051	-0.065	-0.094	-0.115	-0.141	-0.112	-0.088	-0.060	-0.049	-0.037	-0.047	-0.026
00.0	.210	.199	.160	.120	.041	.017	-.026	-.032	-.043	-.069	-.089	-.122	-.153	-.155	-.117	-.085	-.061	-.049	-.050	-.026	.016
-30.0	.158	.145	.107	.066	-.003	.007	-.050	-.047	-.057	-.104	-.095	-.120	-.123	-.144	-.110	-.085	-.058	-.042	-.029	.023	.008
$\alpha = -0.1^\circ$; $\beta = -8.6^\circ$																					
30.0	0.228	0.222	0.190	0.152	0.079	0.095	0.023	0.010	-0.021	-0.043	-0.072	-0.099	-0.121	-0.143	-0.129	-0.120	-0.094	-0.077	-0.032	-0.037	-0.030
00.0	.165	.145	.111	.091	.013	-.015	-.082	-.074	-.095	-.109	-.139	-.178	-.210	-.216	-.179	-.148	-.096	-.064	-.063	-.060	-.074
-30.0	.075	.068	.043	.011	-.086	-.077	-.119	-.102	-.103	-.159	-.154	-.165	-.162	-.171	-.122	-.061	-.037	-.035	-.044	-.057	-.075
$\alpha = 5.1^\circ$; $\beta = 0^\circ$																					
30.0	0.140	0.138	0.102	0.062	0.031	0.009	-0.025	-0.025	-0.053	-0.082	-0.094	-0.119	-0.119	-0.131	-0.101	-0.084	-0.058	-0.042	-0.031	-0.025	0.005
00.0	.142	.139	.101	.060	.001	-.010	-.039	-.045	-.038	-.065	-.105	-.129	-.145	-.135	-.089	-.058	-.045	-.030	-.023	-.007	.021
$\alpha = 5.1^\circ$; $\beta = -4.3^\circ$																					
30.0	0.153	0.166	0.129	0.089	0.045	0.041	-0.021	-0.016	-0.053	-0.087	-0.104	-0.129	-0.139	-0.159	-0.135	-0.120	-0.090	-0.073	-0.062	-0.043	-0.018
00.0	.133	.134	.103	.074	.009	-.006	-.047	-.045	-.065	-.088	-.123	-.145	-.161	-.155	-.109	-.069	-.055	-.039	-.015	.006	-.012
-30.0	.104	.120	.093	.049	-.007	-.010	-.051	-.047	-.070	-.096	-.096	-.116	-.116	-.122	-.088	-.064	-.041	-.014	.018	.005	-.013
$\alpha = 5.1^\circ$; $\beta = -8.6^\circ$																					
30.0	0.144	0.145	0.117	0.088	0.036	0.042	-0.041	-0.043	-0.081	-0.105	-0.134	-0.163	-0.177	-0.202	-0.194	-0.183	-0.140	-0.098	-0.082	-0.099	-0.092
00.0	.096	.080	.052	.038	-.046	-.064	-.121	-.113	-.137	-.146	-.179	-.201	-.226	-.216	-.153	-.087	-.061	-.049	-.052	-.055	-.075
-30.0	.038	.071	.031	-.007	-.065	-.071	-.097	-.087	-.093	-.129	-.123	-.137	-.133	-.123	-.063	-.039	-.035	-.040	-.050	-.071	-.089
$\alpha = 10.3^\circ$; $\beta = 0^\circ$																					
30.0	0.074	0.085	0.065	0.023	0.003	-0.019	-0.053	-0.055	-0.080	-0.110	-0.116	-0.136	-0.134	-0.135	-0.102	-0.080	-0.051	-0.032	-0.006	-0.005	-0.031
00.0	.075	.084	.054	.030	-.006	-.017	-.066	-.061	-.075	-.102	-.120	-.132	-.148	-.124	-.076	-.047	-.037	-.015	.020	.016	-.010
$\alpha = 10.3^\circ$; $\beta = -4.3^\circ$																					
30.0	0.089	0.096	0.070	0.019	-0.003	-0.023	-0.067	-0.070	-0.107	-0.137	-0.145	-0.168	-0.173	-0.181	-0.151	-0.126	-0.092	-0.060	-0.031	-0.027	-0.041
00.0	.088	.085	.057	.024	-.022	-.015	-.068	-.073	-.089	-.107	-.126	-.138	-.153	-.132	-.086	-.057	-.040	-.015	-.011	-.010	-.039
-30.0	.054	.097	.055	.007	-.016	-.043	-.057	-.062	-.080	-.106	-.104	-.120	-.119	-.116	-.080	-.055	-.001	-.001	-.005	-.015	-.031
$\alpha = 10.3^\circ$; $\beta = -8.6^\circ$																					
30.0	0.066	0.072	0.042	0.003	-0.043	-0.041	-0.112	0.115	-0.154	-0.178	-0.191	-0.223	-0.232	-0.246	-0.222	-0.183	-0.128	-0.117	-0.109	-0.116	-0.114
00.0	.047	.048	.019	-.005	-.072	-.074	-.122	-.119	-.135	-.139	-.159	-.170	-.177	-.140	-.089	-.068	-.063	-.058	-.062	-.060	-.079
-30.0	-.007	.047	.011	-.027	-.057	-.077	-.083	-.084	-.094	-.118	-.122	-.134	-.127	-.096	-.060	-.044	-.024	-.031	-.020	-.029	-.034

TABLE I.- Concluded

PRESSURE COEFFICIENTS FOR FUSELAGE ALONE

(g) M = 1.13

∅, deg	Pressure coefficients for x_b/l_b of –																				
	0.160	0.200	0.240	0.280	0.320	0.360	0.400	0.440	0.480	0.520	0.560	0.600	0.640	0.680	0.720	0.760	0.800	0.840	0.880	0.920	0.960
$\alpha = -0.1^\circ$; $\beta = 0^\circ$																					
30.0	0.195	0.183	0.153	0.120	0.037	0.050	0.000	-0.007	-0.025	-0.067	-0.069	-0.093	-0.106	-0.123	-0.100	-0.083	-0.058	-0.053	-0.046	-0.050	0.042
00.0	.199	.189	.159	.134	.071	.031	-.010	-.010	-.027	-.066	-.087	-.116	-.141	-.132	-.119	-.093	-.058	-.043	-.044	-.031	-.037
$\alpha = -0.1^\circ$; $\beta = -4.3^\circ$																					
30.0	0.217	0.204	0.179	0.146	0.067	0.082	0.023	0.012	-0.020	-0.053	-0.073	-0.099	-0.110	-0.130	-0.105	-0.096	-0.069	-0.069	-0.061	-0.064	-0.056
00.0	.189	.170	.143	.126	.052	.015	-.029	-.033	-.050	-.070	-.105	-.128	-.154	-.155	-.126	-.112	-.090	-.074	-.070	-.058	-.058
-30.0	.147	.129	.108	.097	.011	.023	-.034	-.026	-.046	-.095	-.098	-.124	-.123	-.144	-.110	-.092	-.067	-.055	-.047	-.051	-.049
$\alpha = -0.1^\circ$; $\beta = -8.6^\circ$																					
30.0	0.212	0.200	0.180	0.145	0.086	0.099	0.036	0.019	-0.021	-0.052	-0.068	-0.092	-0.119	-0.140	-0.130	-0.125	-0.100	-0.102	-0.090	-0.094	-0.082
00.0	.149	.119	.096	.092	.025	-.009	-.077	-.076	-.105	-.116	-.140	-.178	-.215	-.220	-.194	-.182	-.151	-.128	-.117	-.102	-.101
-30.0	.078	.049	.031	.024	-.063	-.052	-.104	-.100	-.109	-.153	-.155	-.167	-.166	-.178	-.145	-.107	-.082	-.075	-.071	-.073	-.073
$\alpha = 5.1^\circ$; $\beta = 0^\circ$																					
30.0	0.131	0.125	0.110	0.073	0.030	0.025	-0.021	-0.027	-0.057	-0.089	-0.094	-0.108	-0.113	-0.137	-0.116	-0.102	-0.079	-0.067	-0.062	-0.062	-0.055
00.0	.127	.120	.107	.071	.012	-.011	-.045	-.058	-.065	-.075	-.103	-.108	-.135	-.133	-.100	-.074	-.065	-.049	-.043	-.034	-.040
$\alpha = 5.1^\circ$; $\beta = -4.3^\circ$																					
30.0	0.143	0.147	0.127	0.095	0.042	0.045	-0.027	-0.024	-0.060	-0.094	-0.098	-0.121	-0.130	-0.154	-0.139	-0.133	-0.113	-0.099	-0.092	-0.094	-0.080
00.0	.120	.109	.099	.083	.017	-.008	-.063	-.058	-.082	-.090	-.112	-.135	-.158	-.149	-.119	-.094	-.082	-.067	-.058	-.045	-.050
-30.0	.093	.096	.087	.057	-.004	-.001	-.044	-.044	-.062	-.098	-.097	-.118	-.119	-.127	-.102	-.083	-.061	-.047	-.041	-.044	-.047
$\alpha = 5.1^\circ$; $\beta = -8.6^\circ$																					
00.0	0.073	0.046	0.025	-0.008	-0.017	-0.070	-0.118	-0.118	-0.116	-0.137	-0.170	-0.199	-0.217	-0.212	-0.167	-0.132	-0.118	-0.100	-0.090	-0.079	-0.090
-30.0	.037	.042	.027	.004	-.060	-.058	-.091	-.086	-.097	-.128	-.127	-.141	-.141	-.139	-.108	-.089	-.074	-.070	-.069	-.077	-.090
$\alpha = 10.3^\circ$; $\beta = 0^\circ$																					
30.0	0.079	0.078	0.077	0.038	-0.024	-0.022	-0.071	-0.072	-0.089	-0.103	-0.110	-0.135	-0.142	-0.157	-0.129	-0.113	-0.090	-0.078	-0.068	-0.058	-0.068
00.0	.080	.072	.059	.028	-.013	-.035	-.078	-.071	-.073	-.079	-.102	-.118	-.134	-.126	-.094	-.068	-.064	-.048	-.036	-.026	-.034
$\alpha = 10.3^\circ$; $\beta = -4.3^\circ$																					
30.0	0.080	0.088	0.067	0.027	-0.029	-0.031	-0.091	-0.099	-0.109	-0.134	-0.148	-0.170	-0.181	-0.200	-0.178	-0.166	-0.142	-0.127	-0.103	-0.088	-0.085
00.0	.076	.070	.062	.024	-.033	-.049	-.096	-.078	-.090	-.103	-.121	-.133	-.148	-.138	-.110	-.089	-.087	-.073	-.063	-.055	-.073
-30.0	.055	.080	.062	.020	-.028	-.037	-.059	-.057	-.077	-.099	-.097	-.116	-.117	-.128	-.100	-.082	-.058	-.052	-.048	-.042	-.051
$\alpha = 10.3^\circ$; $\beta = -8.6^\circ$																					
30.0	0.062	0.051	0.025	-0.005	-0.063	-0.047	-0.121	-0.130	-0.161	-0.181	-0.198	-0.229	-0.247	-0.275	-0.261	-0.253	-0.226	-0.204	-0.168	-0.147	-0.134
00.0	.035	.016	.008	-.019	-.093	-.090	-.140	-.132	-.142	-.147	-.163	-.173	-.186	-.173	-.143	-.119	-.111	-.099	-.088	-.081	-.090
-30.0	-.004	.033	.018	-.017	-.057	-.070	-.079	-.075	-.091	-.115	-.118	-.133	-.127	-.132	-.107	-.091	-.060	-.055	-.038	-.036	-.036

TABLE II

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(a) M = 0.80; $\alpha = 0^{\circ}$

β, deg	∅, deg	Pressure coefficients for x/l of –																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0.4	P.L.		0.183					0.022	0.030	-0.084			-0.154	-0.141	-0.080		-0.028	0.029
	57.5		.183			0.253		-.000	.020					-.141				
	45.0	0.492								-.082					-.080			
	30.0			0.550		.405	0.209	.101	-.031			-0.233		-.190	-.098			
	15.0							.283	.056	-.109		-.312	-.365	-.231	-.134	-0.032	-.028	
	10.0																	
	07.0									-.001								
	03.0								.313			-.289	-.363	-.237	-.108	-.044	-.004	
	00.0				0.566			.415			-0.119		-.346			-.052	.001	.029
-3.9	P.L.		0.366					0.131	0.112	-0.004			-0.101	-0.105	-0.068		-0.081	0.010
	57.5		.366			0.379		.122	.112					-.105				
	45.0	0.552								.012					-.068			
	30.0			0.576		.489	0.364	.242	.099			-0.137		-.159	-.090			
	15.0							.395	.209	.033		-.208	-.311	-.213	-.146	-0.056	-.081	
	10.0																	
	07.0									.101								
	03.0								.331			-.254	-.359	-.265	-.141	-.073	-.032	
	00.0				0.557			.403			-0.141		-.384			-.074	-.016	.010
4.7	00.0				0.555			0.400			-0.111		-0.406			-0.105	-0.021	0.001
	03.0								0.273			-0.374	-.427	-0.261	-0.151	-.080	-.023	
	07.0									-0.156								
	10.0																	
	15.0							.133	-.119	-.275		-.426	-.427	-.263	-.141	-.032	-.018	
	30.0			0.495		0.282	-0.044	-.066	-.168			-.314		-.212	-.104			
	45.0	0.386								-.166					-.088			
	57.5		-0.047			.113		-.126	-.072					-.165				
	P.L.		-.047					-.082	-.049	-.157			-.197	-.165	-.088		-.018	.001
-8.2	P.L.		0.500					0.239	0.200	0.082			-0.037	-0.061	-0.052		-0.158	-0.019
	57.5		.500			0.478		.239	.197					-.061				
	45.0	0.565								.105					-.052			
	30.0			0.564		.526	0.471	.359	.212			-0.050		-.128	-.077			
	15.0							.435	.313	.144		-.131	-.273	-.214	-.185	-0.100	-.158	
	10.0																	
	07.0									.133								
	03.0								.305			-.280	-.448	-.401	-.252	-.183	-.099	
	00.0				0.519			.359			-0.213		-.516			-.172	-.056	-.019
9.1	00.0				0.515			0.350			-0.134		-0.552			-0.240	-0.063	-0.028
	03.0								0.192			-0.535	-.551	-0.391	-0.270	-.172	-.066	
	07.0									-0.375								
	10.0																	
	15.0							-.097	-.410	-.497		-.583	-.506	-.310	-.171	-.067	-.117	
	30.0			0.413		0.110	-0.435	-.274	-.340			-.407		-.233	-.112			
	45.0	0.238								-.264					-.093			
	57.5		-0.354			-.082		-.274	-.170					-.185				
	P.L.		-.354					-.205	-.132	-.228			-.230	-.185	-.093		-.117	-.028

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(b) $M = 0.80$; $\alpha = 5.1^\circ$

β, deg	∅, deg	Pressure coefficients for x/l of –																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0.0	P.L.		0.219					0.054	0.044	-0.063			-0.184	-0.198	-0.135		-0.051	0.021
	57.5		.219			0.274		.024	.020					-.198				
	45.0	0.462								-.079					-.135			
	30.0			0.496		.356	0.208	.109	-.017			-0.257		-.235	-.137			
	15.0							.233	.035	-.132		-.372	-.422	-.266	-.170	-0.065	-.051	
	10.0																	
	07.0									-.075								
	03.0								.224			-.408	-.421	-.284	-.127	-.053	-.019	
	00.0				0.504			.327			-0.232		-.427			-.060	-.009	.021
-4.3	P.L.		0.368					0.150	0.121	0.010			-0.129	-0.166	-0.131		-0.118	0.001
	57.5		.368			0.373		.126	.105					-.166				
	45.0	0.503								.001					-.131			
	30.0			0.510		.421	0.341	.208	.091			-0.178		-.220	-.140			
	15.0							.321	.154	-.014		-.290	-.396	-.274	-.213	-0.108	-.118	
	10.0																	
	07.0									.005								
	03.0								.231			-.378	-.452	-.351	-.174	-.088	-.044	
	00.0				0.492			.313			-0.267		-.461			-.083	-.038	.001
4.3	00.0				0.489			0.309			-0.209		-0.482			-0.098	-0.037	-0.004
	03.0								0.185			-0.504	-.511	-0.292	-0.156	-.080	-.047	
	07.0									-0.225								
	10.0																	
	15.0							.083	-.149	-.289		-.485	-.455	-.268	-.147	-.043	-.031	
	30.0			0.449		0.238	0.015	-.046	-.149			-.338		-.234	-.126			
	45.0	0.370								-.166					-.133			
	57.5		-0.001			.137		-.099	-.065					-.215				
	P.L.		-.001					-.048	-.032	-.137			-.228	-.215	-.133		-.031	-.004
-8.6	P.L.		0.483					0.253	0.209	0.100			-0.056	-0.119	-0.116		-0.197	-0.021
	57.5		.483			0.455		.237	.198					-.119				
	45.0	0.479								.099					-.116			
	30.0			0.487		.448	0.416	.337	.202			-0.089		-.191	-.137			
	15.0							.352	.250	.093		-.214	-.373	-.297	-.286	-0.173	-.197	
	10.0																	
	07.0									.026								
	03.0								.208			-.412	-.535	-.499	-.298	-.183	-.075	
	00.0				0.444			.268			-0.337		-.654			-.139	-.067	-.021
8.6	00.0				0.438			0.268			-0.235		-0.644			-0.183	-0.067	-0.027
	03.0								0.108			-0.674	-.658	-0.391	-0.244	-.143	-.082	
	07.0									-0.431								
	10.0																	
	15.0							-.109	-.365	-.477		-.635	-.494	-.288	-.157	-.058	-.075	
	30.0			0.373		0.083	-0.298	-.236	-.287			-.429		-.243	-.121			
	45.0	0.235								-.245					-.129			
	57.5		-0.252			-.018		-.219	-.154					-.225				
	P.L.		-.252					-.149	-.108	-.200			-.257	-.225	-.129		-.075	-.027

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(c) M = 0.80; α = 10.2°

β, deg	Ø, deg	Pressure coefficients for x/l of –																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0	P.L.		0.244					0.068	0.043	-0.050			-0.210	-0.256	-0.193		-0.064	0.043
	57.5		.244			0.268		.032	.028					-.256				
	45.0	0.422								-.075					-.193			
	30.0			0.440		.305	0.195	.095	-.014			-0.283		-.284	-.179			
	15.0							.174	.016	-.159		-.424	-.474	-.300	-.202	-0.090	-.064	
	10.0																	
	07.0									-.143								
	03.0								.138			-.511	-.451	-.318	-.129	-.060	-.028	
	00.0				0.430			.239			-0.339		-.411			-.061	-.006	.043
-4.3	P.L.		0.373					0.154	0.116	0.026			-0.149	-0.219	-0.194		-0.121	0.005
	57.5		.373			0.353		.126	.107					-.219				
	45.0	0.438								.007					-.194			
	30.0			0.441		.358	0.297	.210	.085			-0.207		-.272	-.191			
	15.0							.245	.119	-.049		-.351	-.469	-.335	-.280	-.155	-.121	
	10.0																	
	07.0									-.075								
	03.0								.141			-.487	-.484	-.403	-.192	-.097	-.049	
	00.0				0.418			.222			-0.381		-.480			-.100	-.047	.005
4.3	00.0				0.415			0.220			-0.330		-0.470			-0.098	-0.046	0.005
	03.0								0.105			-0.579	-.478	-0.318	-0.149	-.087	-.060	
	07.0									-0.236								
	10.0																	
	15.0							.079	-.093	-.259		-.485	-.465	-.284	-.177	-.071	-.061	
	30.0			0.411		0.221	0.060	-.012	-.092			-.328		-.270	-.165			
	45.0	0.361								-.121					-.181			
	57.5		0.103			.180		-.046	-.029					-.261				
	P.L.		.103					-.002	-.016	-.098			-.240	-.261	-.181		-.061	.005
-8.6	P.L.		0.443					0.243	0.198	0.099			-0.085	-0.180	-0.187		-0.189	-0.014
	57.5		.443			0.401		.210	.178					-.180				
	45.0	0.389								.074					-.187			
	30.0			0.415		.358	0.343	.290	.159			-0.145		-.259	-.199			
	15.0							.241	.172	.016		-.303	-.478	-.379	-.361	-0.231	-.189	
	10.0																	
	07.0									-.088								
	03.0								.114			-.543	-.601	-.536	-.294	-.147	-.068	
	00.0				0.384			.185			-0.437		-.665			-.143	-.062	-.014
8.6	00.0				0.363			0.174			-0.348		-0.642			-0.154	-0.068	-0.019
	03.0								0.026			-0.764	-.603	-0.359	-0.215	-.149	-.083	
	07.0									-0.451								
	10.0																	
	15.0							-.131	-.328	-.452		-.647	-.469	-.273	-.149	-.055	-.087	
	30.0			0.325		0.052	-0.239	-.207	-.240			-.426		-.262	-.144			
	45.0	0.231								-.220					-.164			
	57.5		-0.166			.018		-.176	-.126					-.274				
	P.L.		-.166					-.106	-.096	-.177			-.282	-.274	-.164		-.087	-.019

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(d) $M = 0.90$; $\alpha = 0^\circ$

β, deg	ø, deg	Pressure coefficients for x/l of –																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0.1	P.L.		0.226					0.054	0.066	-0.069			-0.228	-0.228	-0.081		-0.036	0.024
	57.5		.226			0.294		.033	.055					-.228				
	45.0	0.529								-.051					-.081			
	30.0			0.579		.438	0.262	.139	.013			-0.210		-.320	-.088			
	15.0							.331	.102	-.059		-.327	-.504	-.481	-.114	-0.035	-.036	
	10.0																	
	07.0									.058								
	03.0								.348			-.305	-.508	-.527	-.079	-.041	-.010	
	00.0				0.620			.452			-0.068		-.506			-.052	.001	.024
-4.2	P.L.		0.411					0.168	0.150	0.016			-0.151	-0.158	-0.083		-0.093	0.001
	57.5		.411			0.422		.158	.146					-.158				
	45.0	0.588								.042					-.083			
	30.0			0.604		.525	0.413	.282	.141			-0.116		-.211	-.099			
	15.0							.431	.249	.079		-.199	-.443	-.321	-.153	-0.065	-.093	
	10.0																	
	07.0									.145								
	03.0								.365			-.309	-.461	-.512	-.135	-.081	-.041	
	00.0				0.593			.436			-0.101		-.503			-.080	-.023	.001
4.5	00.0				0.598			0.434			-0.057		-0.578			-0.096	-0.019	0.002
	03.0								0.319			-0.398	-.602	-0.574	-0.108	-.072	-.023	
	07.0									-0.094								
	10.0																	
	15.0							.187	-.074	-.222		-.484	-.578	-.583	-.100	-.028	-.017	
	30.0			0.533		0.329	0.021	-.015	-.133			-.315		-.372	-.077			
	45.0	0.438								-.141					-.074			
	57.5		0.001			.161		-.098	-.041					-.270				
	P.L.		.001					-.057	-.015	-.143			-.318	-.270	-.074		-.017	.002
-8.6	P.L.		0.545					0.280	0.242	0.109			-0.060	-0.099	-0.074		-0.167	-0.030
	57.5		.545			0.519		.280	.238					-.099				
	45.0	0.594								.142					-.074			
	30.0			0.594		.558	0.515	.402	.261			-0.021		-.169	-.102			
	15.0							.472	.354	.188		-.106	-.366	-.293	-.240	-0.114	-.167	
	10.0																	
	07.0									.183								
	03.0								.344			-.277	-.571	-.597	-.250	-.193	-.100	
	00.0				0.567			.398			-0.160		-.685			-.173	-.068	-.030
8.8	00.0				0.565			0.393			-0.081		-0.701			-0.226	-0.066	-0.033
	03.0								0.244			-0.514	-.833	-0.741	-0.221	-.155	-.071	
	07.0									-0.299								
	10.0																	
	15.0							-0.014	-.355	-.454		-.635	-.693	-.656	-.132	-.079	-.138	
	30.0			0.461		0.177	-0.366	-.207	-.314			-.418		-.391	-.080			
	45.0	0.312								-.236					-.074			
	57.5		-0.321			-.017		-.251	-.143					-.319				
	P.L.		-.321					-.187	-.103	-.217			-.397	-.319	-.074		-.138	-.033

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(e) $M = 0.90$; $\alpha = 5.1^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of —																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0	P.L.		0.257					0.081	0.072	-0.043			-0.242	-0.374	-0.139		-0.056	0.18
	57.5		.257			0.314		.050	.050					-.374				
	45.0	0.504								-.053					-.139			
	30.0			0.534		.396	0.241	.143	.015			-0.228		-.457	-.129			
	15.0							.265	.072	-.085		-.379	-.587	-.537	-.142	-0.066	-.056	
	10.0																	
	07.0									-.024								
	03.0								.260			-.449	-.592	-.654	-.090	-.056	-.026	
	00.0				0.539			.356			-0.169		-.598			-.061	-.016	.018
-4.3	P.L.		0.409					0.178	0.148	0.031			-0.165	-0.271	-0.154		-0.124	-0.004
	57.5		.409			0.414		.156	.135					-.271				
	45.0	0.544								.030					-.154			
	30.0			0.550		.463	0.376	.240	.124			-0.149		-.389	-.150			
	15.0							.351	.192	.031		-.266	-.547	-.469	-.204	-0.113	-.124	
	10.0																	
	07.0									.053								
	03.0								.267			-.448	-.547	-.650	-.144	-.090	-.051	
	00.0				0.526			.344			-0.206		-.620			-.085	-.044	-.004
4.3	00.0				0.525			0.343			-0.141		-0.652			-0.097	-0.042	-0.007
	03.0								0.223			-0.533	-.732	-0.682	-0.107	-.082	-.052	
	07.0									-0.164								
	10.0																	
	15.0							.123	-.104	-.239		-.503	-.647	-.617	-.101	-.042	-.038	
	30.0			0.494		0.284	0.052	-.008	-.116			-.325		-.503	-.099			
	45.0	0.421								-.140					-.114			
	57.5		0.039			.183		-.075	-.034					-.439				
	P.L.		.039					-.023	-.006	-.121			-.312	-.439	-.114		-.038	-.007
-8.7	P.L.		0.522					0.281	0.238	0.120			-0.078	-0.175	-0.159		-0.195	-0.024
	57.5		.522			0.495		.265	.228					-.175				
	45.0	0.523								.125					-.159			
	30.0			0.529		.489	0.450	.366	.233			-0.065		-.280	-.174			
	15.0							.385	.284	.135		-.181	-.485	-.432	-.331	-0.178	-.195	
	10.0																	
	07.0									.079								
	03.0								.249			-.429	-.654	-.724	-.255	-.164	-.078	
	00.0				0.482			.306			-0.267		-.779			-.134	-.071	-.024
8.7	00.0				0.479			0.306			-0.165		-0.784			-0.163	-0.069	-0.030
	03.0								0.151			-0.610	-.910	-0.787	-0.202	-.146	-.085	
	07.0									-0.371								
	10.0																	
	15.0							-.046	-.322	-.433		-.639	-.719	-.630	-.134	-.059	-.107	
	30.0			0.424		0.141	-0.268	-.197	-.254			-.414		-.496	-.096			
	45.0	0.303								-.219					-.107			
	57.5		-0.223			.034		-.197	-.126					-.491				
	P.L.		-.223					-.130	-.082	-.186			-.372	-.491	-.107		-.107	-.030

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(f) M = 0.90; α = 10.2°

β, deg	∅, deg	Pressure coefficients for x/l of –																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0	P.L.		0.280					0.095	0.069	-0.024			-0.228	-0.401	-0.200		-0.068	0.041
	57.5		.280			0.305		.057	.059					-.401				
	45.0	0.460								-.041					-.200			
	30.0			0.476		.339	0.230	.125	.020			-0.240		-.536	-.160			
	15.0							.203	.054	-.114		-.388	-.653	-.588	-.165	-0.090	-.068	
	10.0									-.085								
	07.0								.174			-.555	-.660	-.688	-.100	-.063	-.036	
	03.0										-0.270		-.635			-.061	-.014	.041
	00.0				0.465			.266										
-4.3	P.L.		0.410					0.184	0.148	0.054			-0.153	-0.313	-0.253		-0.115	0.005
	57.5		.410			0.392		.156	.141					-.313				
	45.0	0.480								.041					-.253			
	30.0			0.482		.398	0.329	.243	.120			-0.163		-.448	-.204			
	15.0							.274	.156	-.002		-.309	-.612	-.573	-.255	-0.154	-.115	
	10.0									-.018								
	07.0								.181			-.527	-.651	-.746	-.163	-.101	-.052	
	03.0										-.318		-.678			-.107	-.047	.005
	00.0				0.459			.255										
4.3	00.0				0.452			0.252			-0.259		-0.723			-0.104	-0.047	0.004
	03.0								0.142			-0.606	-.728	-0.679	-0.126	-.094	-.066	
	07.0									-0.184								
	10.0																	
	15.0							.099	-.071	-.226		-.469	-.668	-.613	-.133	-.064	-.069	
	30.0			0.454		0.249	0.082	.004	-.071			-.305		-.557	-.138			
	45.0	0.403								-.099					-.170			
	57.5		0.121			.207		-.033	-.007					-.456				
	P.L.		.121					.017	.005	-.082			-.277	-.456	-.170		-.069	.004
-8.7	P.L.		0.490					0.279	0.235	0.133			-0.077	-0.218	-0.263		-0.178	-0.012
	57.5		.490			0.444		.247	.215					-.218				
	45.0	0.432								.115					-.263			
	30.0			0.458		.404	0.379	.326	.200			-0.097		-.355	-.267			
	15.0							.276	.214	.070		-.244	-.578	-.545	-.452	-0.230	-.178	
	10.0																	
	07.0									-.023								
	03.0								.157			-.522	-.737	-.852	-.259	-.144	-.069	
	00.0				0.428			.221			-0.361		-.837			-.142	-.067	-.012
8.7	00.0				0.406			0.213			-0.285		-0.807			-0.148	-0.070	-0.019
	03.0								0.076			-0.673	-.919	-0.658	-0.260	-.138	-.085	
	07.0									-0.385								
	10.0																	
	15.0							-.063	-.288	-.386		-.590	-.728	-.616	-.133	-.063	-.104	
	30.0			0.384		0.113	-0.184	-.164	-.192			-.392		-.595	-.126			
	45.0	0.295								-.179					-.153			
	57.5		-0.111			.077		-.145	-.090					-.523				
	P.L.		-.111					-.079	-.067	-.151			-.341	-.523	-.153		-.104	-.019

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(g) M = 0.95; α = 0°

β, deg	ø, deg	Pressure coefficients for x/l of –																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0.3	P.L.		0.255					0.070	0.087	-0.040			-0.232	-0.362	-0.265		-0.036	0.017
	57.5		.255			0.326		.052	.078					-.362				
	45.0	0.568								-.024					-.265			
	30.0			0.617		.474	0.278	.166	.029			-0.176		-.439	-.291			
	15.0							.346	.129	-.026		-.296	-.474	-.507	-.370	-0.002	-.036	
	10.0																	
	07.0									.080								
	03.0								.379			-.299	-.465	-.521	-.405	-.004	-.012	
	00.0				0.628			.473			-0.028		-.457			-.011	-.007	.017
-4.0	P.L.		0.435					0.183	0.167	0.037			-0.153	-0.272	-0.196		-0.093	-0.005
	57.5		.435			0.445		.174	.167					-.272				
	45.0	0.622								.065					-.196			
	30.0			0.639		.555	0.427	.300	.156			-0.086		-.362	-.231			
	15.0							.450	.274	.104		-.180	-.417	-.429	-.350	-0.034	-.093	
	10.0																	
	07.0									.177								
	03.0								.397			-.270	-.436	-.537	-.413	-.040	-.037	
	00.0				0.618			.461			-0.058		-.479			-.036	-.026	-.005
4.7	00.0				0.621			0.463			-0.009		-0.535			-0.061	-0.023	-0.007
	03.0								0.345			-0.349	-.580	-0.566	-0.455	-.038	-.029	
	07.0									-0.054								
	10.0																	
	15.0							.215	-.028	-.177		-.439	-.528	-.577	-.393	.004	-.026	
	30.0			0.574		0.364	0.031	.014	-.102			-.269		-.506	-.299			
	45.0	0.479								-.091					-.285			
	57.5		0.026			.197		-.074	-.010					-.427				
	P.L.		.026					-.039	.012	-.102			-.295	-.427	-.285		-.026	-.007
-8.5	P.L.		0.571					0.295	0.257	0.128			-0.065	-0.165	-0.142		-0.158	-0.024
	57.5		.571			0.546		.297	.258					-.165				
	45.0	0.637								.158					-.142			
	30.0			0.637		.599	0.535	.422	.275			0.004		-.274	-.176			
	15.0							.497	.384	.215		-.072	-.361	-.367	-.364	-0.071	-.158	
	10.0																	
	07.0									.218								
	03.0								.382			-.241	-.520	-.651	-.510	-.134	-.088	
	00.0				0.595			.431			-0.111		-.627			-.103	-.065	-.024
9.2	00.0				0.584			0.424			-0.038		-0.646			-0.161	-0.068	-0.036
	03.0								0.278			-0.447	-.767	-0.714	-0.569	-.112	-.072	
	07.0									-0.250								
	10.0																	
	15.0							.032	-.386	-.408		-.573	-.629	-.660	-.397	-.078	-.131	
	30.0			0.507		0.219	-0.354	-.182	-.322			-.375		-.585	-.295			
	45.0	0.365								-.190					-.293			
	57.5		-0.331			.023		-.213	-.107					-.492				
	P.L.		-.331					-.161	-.067	-.175			-.364	-.492	-.293		-.131	-.036

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(h) $M = 0.95$; $\alpha = 5.1^\circ$

β, deg	ø, deg	Pressure coefficients for x/l of –																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0	P.L.		0.290					0.108	0.105	-0.009			-0.208	-0.373	-0.343		-0.053	0.017
	57.5		.290			0.348		.079	.086					-.373				
	45.0	0.536								-.014					-.343			
	30.0			0.565		.429	0.271	.175	.051			-0.189		-.477	-.341			
	15.0							.293	.109	-.037		-.316	-.534	-.542	-.416	-0.026	-.053	
	10.0																	
	07.0									.025								
	03.0								.293			-.402	-.549	-.602	-.408	-.012	-.026	
	00.0				0.567			.385			-0.115		-.549			-.014	-.018	.017
-4.4	P.L.		0.436					0.203	0.178	0.059			-0.143	-0.308	-0.306		-0.118	-0.006
	57.5		.436			0.441		.181	.163					-.308				
	45.0	0.572								.061					-.306			
	30.0			0.578		.491	0.399	.265	.152			-0.102		-.422	-.304			
	15.0							.373	.220	.071		-.224	-.517	-.495	-.428	-0.065	-.118	
	10.0																	
	07.0									.095								
	03.0								.299			-.391	-.531	-.636	-.472	-.048	-.053	
	00.0							.370			-0.142		-.591			-.048	-.045	-.006
4.4	00.0				0.547			0.368			-0.092		-0.619			-0.057	-0.046	-0.012
	03.0								0.252			-0.482	-.716	-0.658	-0.447	-.053	-.066	
	07.0									-0.129								
	10.0																	
	15.0							.144	-.087	-.198		-.458	-.603	-.629	-.389	-.009	-.039	
	30.0			0.522		0.311	0.072	.011	-.087			-.284		-.544	-.362			
	45.0	0.451								-.107					-.383			
	57.5		0.057			.209		-.054	-.005					-.443				
	P.L.		.057					-.002	.024	-.089			-.285	-.443	-.383		-.039	-.012
-8.8	P.L.		0.552					0.311	0.270	0.155			-0.052	-0.192	-0.232		-0.187	-0.027
	57.5		.552			0.526		.296	.262					-.192				
	45.0	0.550								.162					-.232			
	30.0			0.556		.521	0.478	.399	.267			-0.018		-.319	-.252			
	15.0							.412	.320	.179		-.120	-.443	-.450	-.480	-0.124	-.187	
	10.0																	
	07.0									.126								
	03.0								.282			-.371	-.616	-.779	-.629	-.123	-.076	
	00.0				0.509			.334			-0.210		-.759			-.121	-.070	-.027
8.8	00.0				0.507			0.335			-0.119		-0.740			-0.130	-0.071	-0.034
	03.0								0.181			-0.556	-.867	-0.762	-0.562	-.128	-.082	
	07.0									-0.334								
	10.0																	
	15.0							-.009	-.323	-.421		-.570	-.664	-.687	-.376	-.028	-.110	
	30.0			0.458		0.172	-0.248	-.200	-.195			-.370		-.592	-.347			
	45.0	0.342								-.194					-.392			
	57.5		-0.218			.067		-.182	-.087					-.499				
	P.L.		-.218					-.107	-.045	-.156			-.344	-.499	-.392		-.110	-.034

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(i) $M = 0.95$; $\alpha = 10.3°$

β, deg	∅, deg	Pressure coefficients for x/l of –																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0	P.L.		0.311					0.121	0.102	0.011			-0.184	-0.375	-0.441		-0.064	0.054
	57.5		.311			0.339		.088	.093					-.375				
	45.0	0.492								-.001					-.441			
	30.0			0.505		.372	0.259	.156	.056			-0.191		-.504	-.408			
	15.0							.232	.091	-.069		-.337	-.589	-.563	-.487	-0.062	-.064	
	10.0																	
	07.0									-.032								
	03.0								.210			-.489	-.595	-.661	-.389	-.040	-.034	
	00.0				0.496			.296			-0.224		-.580			-.032	-.004	.054
-4.3	P.L.		0.444					0.215	0.182	0.091			-0.112	-0.292	-0.381		-0.103	0.007
	57.5		.444			0.426		.188	.178					-.292				
	45.0	0.509								.084					.381			
	30.0			0.512		.430	0.361	.275	.158			-0.106		-.424	-.377			
	15.0							.302	.195	.045		-.244	-.554	-.549	-.547	-0.126	-.103	
	10.0																	
	07.0									.034								
	03.0								.216			-.459	-.611	-.728	-.524	-.097	-.051	
	00.0				0.489			.284			-0.260		-.652			-.114	-.054	.007
4.3	00.0				0.480			0.283			-0.210		-0.662			-0.094	-0.053	0.010
	03.0								0.178			-0.533	-.683	-0.680	-0.399	-.082	-.071	
	07.0									-0.133								
	10.0																	
	15.0							.125	-.041	-.175		-.416	-.614	-.605	-.435	-.039	-.056	
	30.0			0.485		0.277	0.108	.027	-.040			-.260		-.531	-.415			
	45.0	0.432								-.066					-.456			
	57.5		0.143			.234		-.009	.021					-.425				
	P.L.		.143					.042	.038	-.049			-.238	-.425	-.456		-.056	.010
-8.8	P.L.		0.513					0.303	0.261	0.160			-0.049	-0.215	-0.322		-0.159	-0.012
	57.5		.513			0.470		.269	.241					-.215				
	45.0	0.464								.144					-.322			
	30.0			0.490		.433	0.406	.350	.229			-0.056		-.366	-.334			
	15.0							.302	.241	.105		-.197	-.533	-.536	-.569	-0.273	-.159	
	10.0																	
	07.0									.022								
	03.0								.193			-.460	-.672	-.828	-.650	-.169	-.067	
	00.0				0.461			.254			-0.294		-.786			-.180	-.060	-.012
8.8	00.0				0.433			0.239			-0.242		-0.761			-0.178	-0.069	-0.021
	03.0								0.104			-0.627	-.897	-0.778	-0.494	-.217	-.081	
	07.0									-0.372								
	10.0																	
	15.0							-.050	-.259	-.400		-.541	-.674	-.664	-.395	-.043	-.085	
	30.0			0.412		0.131	-0.184	-.152	-.174			-.346		-.585	-.420			
	45.0	0.322								-.157					-.483			
	57.5		-0.117			.096		-.131	-.064					-.489				
	P.L.		-.117					-.062	-.039	-.124			-.304	-.489	-.483		-.085	-.021

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(j) $M = 0.99$; $\alpha = 0^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of —																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0.2	P.L.		0.293					0.108	0.128	0.003			-0.186	-0.325	-0.252		-0.079	-0.031
	57.5		.293			0.362		.090	.119					-.325				
	45.0	0.599								.023					-.252			
	30.0			0.645		.506	0.317	.207	.073			-0.128		-.395	-.269			
	15.0							.385	.170	.021		-.250	-.421	-.461	-.348	-0.083	-.079	
	10.0																	
	07.0									.127								
	03.0								.413			-.255	-.414	-.463	-.372	-.084	-.055	
	00.0				0.659			.506			0.017		-.411			-.094	-.048	-.031
-4.2	P.L.		0.468					0.219	0.207	0.080			-0.113	-0.244	-0.192		-0.138	-0.055
	57.5		.468			0.480		.211	.206					-.244				
	45.0	0.652								.109					-.192			
	30.0			0.669		.584	0.462	.336	.197			-0.038		-.326	-.217			
	15.0							.484	.308	.149		-.133	-.364	-.388	-.327	-0.143	-.138	
	10.0																	
	07.0									.218								
	03.0								.431			-.222	-.383	-.485	-.389	-.129	-.082	
	00.0				0.647			.492			-0.012		-.428			-.121	-.070	-.055
4.6	00.0				0.649			0.495			0.035		-0.484			-0.163	-0.071	-0.059
	03.0								0.376			-0.308	-0.539	-0.517	-0.436	-0.129	-0.077	
	07.0									-0.022								
	10.0																	
	15.0							.243	.010	-.144		-.390	-.485	-.536	-.397	-.077	-.066	
	30.0			0.601		0.394	0.066	.048	-.068			-.227		-.474	-.320			
	45.0	0.509								-.050					-.302			
	57.5		0.054			.226		-.046	.025					-.396				
	P.L.		.054					-.008	.049	-.060			-.256	-.396	-.302		-.066	-.059
-8.6	P.L.		0.603					0.332	0.298	0.168			-0.027	-0.142	-0.121		-0.222	-0.081
	57.5		.603			0.577		.332	.296					-.142				
	45.0	0.663								.201					-.121			
	30.0			0.662		.623	0.567	.457	.316			0.051		-.234	-.155			
	15.0							.529	.412	.257		-.024	-.311	-.321	-.346	-0.251	-.222	
	10.0																	
	07.0									.256								
	03.0								.414			-.194	-.466	-.617	-.487	-.267	-.143	
	00.0				0.620			.459			-0.062		-.574			-.216	-.125	-.081
9.1	00.0				0.613			0.457			0.003		-0.591			-0.305	-0.133	-0.094
	03.0								0.313			-0.398	-.726	-0.640	-0.542	-.226	-.133	
	07.0									-0.213								
	10.0																	
	15.0							.071	-.366	-.421		-.482	-.573	-.607	-.453	-.154	-.148	
	30.0			0.539		0.254	-0.319	-.161	-.320			-.316		-.541	-.350			
	45.0	0.401								-.142					-.335			
	57.5		-0.320			.063		-.176	-.095					-.448				
	P.L.		-.320					-.127	-.042	-.122			-.318	-.448	-.335		-.148	-.094

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(k) M = 0.99; $\alpha = 5.2^\circ$

β, deg	∅, deg	Pressure coefficients for x/l of —																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0	P.L.		0.330					0.147	0.150	0.038			-0.160	-0.318	-0.317		-0.104	-0.041
	57.5		.330			0.388		.121	.131					-.318				
	45.0	0.569								.035					-.317			
	30.0			0.595		.468	0.312	.219	.096			-0.135		-.423	-.310			
	15.0							.332	.155	.019		-.251	-.476	-.485	-.378	-0.132	-.104	
	10.0																	
	07.0									.077								
	03.0								.331			-.340	-.483	-.540	-.389	-.117	-.077	
	00.0				0.596			.417			-0.068		-.486			-.122	-.068	-.041
-4.4	P.L.		0.476					0.244	0.221	0.107			-0.093	-0.252	-0.275		-0.175	-0.067
	57.5		.476			0.482		.224	.208					-.252				
	45.0	0.606								.110					-.275			
	30.0			0.610		.530	0.438	.307	.197			-0.049		-.367	-.275			
	15.0							.411	.267	.122		-.158	-.449	-.449	-.398	-0.210	-.175	
	10.0																	
	07.0									.145								
	03.0								.338			-.329	-.466	-.580	-.441	-.158	-.108	
	00.0				0.587			.406			-0.087		-.530			-.155	-.104	-.067
4.4	00.0				0.579			0.403			-0.044		-0.547			-0.169	-0.105	-0.076
	03.0								0.294			-0.405	-.628	-0.580	-0.427	-.158	-.127	
	07.0									-0.070								
	10.0																	
	15.0							.195	-.020	-.129		-.380	-.526	-.560	-.387	-.111	-.090	
	30.0			0.559		0.358	0.124	.064	-.034			-.221		-.489	-.342			
	45.0	0.492								-.052					-.359			
	57.5		0.112			.259		-.006	.044					-.391				
	P.L.		.112					.040	.070	-.037			-.233	-.391	-.359		-.090	-.076
-8.9	P.L.		0.583					0.344	0.306	0.191			-0.010	-0.168	-0.208		-0.253	-0.094
	57.5		.583			0.558		.329	.297					-.168				
	45.0	0.583								.197					-.208			
	30.0			0.586		.555	0.510	.432	.302			0.027		-.286	-.226			
	15.0							.440	.352	.220		-.070	-.393	-.401	-.427	-0.355	-.253	
	10.0																	
	07.0									.169								
	03.0								.318			-.313	-.538	-.702	-.573	-.249	-.142	
	00.0				0.541			.370			-0.148		-.672			-.242	-.136	-.094
8.9	00.0				0.541			0.373			-0.070		-0.653			-0.253	-0.137	-0.102
	03.0								0.224			-0.472	-.755	-0.683	-0.536	-.245	-.149	
	07.0									-0.261								
	10.0																	
	15.0							.050	-.265	-.309		-.493	-.583	-.607	-.405	-.134	-.152	
	30.0			0.498		0.226	-0.185	-.147	-.164			-.302		-.527	-.352			
	45.0	0.391								-.130					-.379			
	57.5		-0.164			.125		-.144	-.038					-.440				
	P.L.		-.164					-.070	.003	-.094			-.287	-.440	-.379		-.152	-.102

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(i) M = 0.99; α = 10.3°

β, deg	ϕ, deg	Pressure coefficients for x/l of —																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0	P.L.		0.345					0.161	0.143	0.055			-0.134	-0.321	-0.393		-0.132	-0.011
	57.5		.345			0.372		.125	.133					-.321				
	45.0	0.523								.043					-.393			
	30.0			0.539		.407	0.293	.193	.097			-0.139		-.443	-.369			
	15.0							.266	.132	-.024		-.276	-.522	-.508	-.444	-0.186	-.132	
	10.0																	
	07.0									.018								
	03.0								.249			-.427	-.531	-.591	-.368	-.154	-.099	
	00.0				0.526			.329			-0.169		-.516			-.152	-.070	-.011
-4.4	P.L.		0.476					0.250	0.220	0.132			-0.063	-0.248	-0.341		-0.182	-0.071
	57.5		.476			0.459		.224	.215					-.248				
	45.0	0.539								.125					-.341			
	30.0			0.542		.464	0.393	.310	.197			-0.060		-.372	-.337			
	15.0							.334	.233	.089		-.187	-.494	-.498	-.499	-0.305	-.182	
	10.0																	
	07.0									.078								
	03.0								.253			-.397	-.555	-.675	-.504	-.217	-.132	
	00.0				0.519			.316			-0.203		-.596			-.223	-.140	-.071
4.4	00.0				0.510			0.316			-0.158		-0.594			-0.209	-0.139	-0.069
	03.0								0.218			-0.461	-0.614	-0.618	-0.391	-0.199	-0.152	
	07.0									-0.089								
	10.0																	
	15.0							.168	.012	-.131		-.347	-.547	-.546	-.413	-.159	-.133	
	30.0			0.516		0.317	0.146	.070	.009			-.201		-.471	-.378			
	45.0	0.469								-.015					-.412			
	57.5		0.185			.277		.034	.069					-.364				
	P.L.		.185					.082	.080	-.001			-.187	-.364	-.412		-.133	-.069
-8.8	P.L.		0.552					0.342	0.303	0.207			0.005	-0.168	-0.277		-0.239	-0.092
	57.5		.552			0.510		.313	.287					-.168				
	45.0	0.497								.195					-.277			
	30.0			0.524		.473	0.443	.391	.273			0.002		-.309	-.286			
	15.0							.340	.287	.157		-.136	-.464	-.474	-.524	-0.467	-.239	
	10.0																	
	07.0									.073								
	03.0								.233			-.393	-.611	-.780	-.639	-.278	-.152	
	00.0				0.495			.288			-0.242		-.733			-.282	-.147	-.092
8.8	00.0				0.469			0.279			-0.179		-0.677			-0.280	-0.163	-0.098
	03.0								0.147			-0.544	-.783	-0.695	-0.470	-.294	-.175	
	07.0									-0.293								
	10.0																	
	15.0							.010	-.187	-.337		-.467	-.595	-.593	-.381	-.145	-.169	
	30.0			0.452		0.180	-0.131	-.109	-.104			-.284		-.528	-.383			
	45.0	0.373								-.102					-.437			
	57.5		-0.066			.147		-.088	-.006					-.422				
	P.L.		-.066					-.017	.011	-.075			-.251	-.422	-.437		-.169	-.098

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(m) M = 1.02; $\alpha = 0^{\circ}$

β, deg	∅, deg	Pressure coefficients for x/l of –																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0	P.L.		0.344					0.145	0.170	0.047			-0.143	-0.272	-0.217		-0.077	-0.020
	57.5		.344			0.413		.137	.165					-.272				
	45.0	0.630								.072					-.217			
	30.0			0.663		.557	0.357	.261	.120			-0.075		-.342	-.231			
	15.0							.415	.212	.074		-.189	-.361	-.404	-.307	-0.070	-.077	
	10.0																	
	07.0									.174								
	03.0								.449			-.209	-.359	-.418	-.327	-.072	-.047	
	00.0				0.666			.530			0.057		-.353			-.082	-.042	-.020
-4.4	P.L.		0.512					0.260	0.252	0.125			-0.068	-0.191	-0.160		-0.155	-0.047
	57.5		.512			0.524		.259	.254					-.191				
	45.0	0.681								.158					-.160			
	30.0			0.687		.632	0.501	.389	.244			0.014		-.266	-.178			
	15.0							.512	.351	.197		-.075	-.305	-.335	-.285	-0.139	-.155	
	10.0																	
	07.0									.261								
	03.0								.460			-.172	-.336	-.441	-.348	-.126	-.077	
	00.0				0.653			.520			0.024		-.382			-.116	-.065	-.047
4.4	00.0				0.660			0.521			0.074		-0.413			-0.144	-0.060	-0.047
	03.0								0.414			-0.259	-.469	-0.457	-0.383	-.111	-.066	
	07.0									0.045								
	10.0																	
	15.0							.291	.048	-.082		-.319	-.420	-.469	-.349	-.057	-.059	
	30.0			0.634		0.450	0.131	.113	-.015					-.409	-.276			
	45.0	0.548								.002					-.260			
	57.5		0.114			.284		.011	.077					-.338				
	P.L.		.114					.037	.099	-.011			-.205	-.338	-.260		-.059	-.047
-8.9	P.L.		0.641					0.369	0.339	0.211			0.016	-0.092	-0.085		-0.249	-0.075
	57.5		.641			0.619		.379	.342					-.092				
	45.0	0.687								.247					-.085			
	30.0			0.675		.670	0.601	.505	.357			0.100		-0.178	-0.114			
	15.0							.555	.450	.301		.033	-.255	-.266	-.297	-0.218	-.249	
	10.0																	
	07.0									.295								
	03.0								.444			-.146	-.410	-.566	-.454	-.290	-.143	
	00.0				0.630			.488			-0.019		-.519			-.221	-.127	-.075
8.9	00.0				0.630			0.489			0.044		-0.522			-0.304	-0.116	-0.077
	03.0								0.349			-0.343	-.655	-0.568	-0.483	-.210	-.118	
	07.0									-0.143								
	10.0																	
	15.0							.122	-.253	-.357		-.419	-.507	-.542	-.412	-.123	-.134	
	30.0			0.578		0.312	-0.234	-.071	-.238			-.252		-.479	-.311			
	45.0	0.442								-.092					-.295			
	57.5		-0.251			.126		-.112	-.055					-.391				
	P.L.		-.251					-.076	-.003	-.076			-.265	-.391	-.295		-.134	-.077

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(n) $M = 1.02$; $\alpha = 5.2^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of —																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0	P.L.		0.362					0.182	0.188	0.078			-0.118	-0.274	-0.282		-0.096	-0.029
	57.5		.362			0.427		.158	.168					-.274				
	45.0	0.600								.076					-.282			
	30.0			0.623		.503	0.345	.259	.134			-0.088		-.378	-.271			
	15.0							.363	.194	.062		-.200	-.427	-.436	-.337	-0.112	-.096	
	10.0																	
	07.0									.116								
	03.0								.365			-.289	-.428	-.490	-.348	-.098	-.066	
	00.0				0.623			.447			-0.027		-.434			-.103	-.057	-.029
-4.4	P.L.		0.506					0.277	0.258	0.146			-0.055	-0.209	-0.242		-0.169	-0.059
	57.5		.506			0.515		.258	.245					-.209				
	45.0	0.634								.148					-.242			
	30.0			0.637		.564	0.469	.344	.236			-0.008		-.322	-.241			
	15.0							.441	.303	.162		-.111	-.395	-.405	-.356	-0.198	-.169	
	10.0																	
	07.0									.184								
	03.0								.368			-.279	-.411	-.527	-.399	-.143	-.099	
	00.0				0.610			.434			-0.049		-.475			-.138	-.095	-.059
4.4	00.0				0.605			0.434			-0.004		-0.490			-0.151	-0.094	-0.064
	03.0								0.328			-0.351	-.568	-0.525	-0.386	-.137	-.117	
	07.0									-0.025								
	10.0																	
	15.0							.232	.024	-.092		-.320	-.473	-.506	-.349	-.090	-.080	
	30.0			0.588		0.398	0.161	.102	.009			-.174		-.438	-.304			
	45.0	0.525								-.008					-.321			
	57.5		0.148			.302		.035	.084					-.343				
	P.L.		.148					.077	.110	.005			-.188	-.343	-.321		-.080	-.064
-8.9	P.L.		0.611					0.376	0.343	0.228			0.028	-0.131	-0.171		-0.249	-0.084
	57.5		.611			0.588		.362	.330					-.131				
	45.0	0.613								.233					-.171			
	30.0			0.614		.589	0.541	.465	.334			0.068		-.246	-.191			
	15.0							.472	.385	.256		-.025	-.344	-.356	-.377	-0.317	-.249	
	10.0																	
	07.0									.206								
	03.0								.354			-.263	-.480	-.640	-.520	-.232	-.133	
	00.0				0.571			.403			-0.104		-.610			-.220	-.127	-.084
8.9	00.0				0.570			0.404			-0.031		-0.596			-0.238	-0.130	-0.091
	03.0								0.259			-0.420	-.687	-0.631	-0.490	-.228	-.141	
	07.0									-0.218								
	10.0																	
	15.0							.093	-.217	-.271		-.431	-.526	-.551	-.373	-.115	-.141	
	30.0			0.530		0.269	-0.143	-.101	-.152			-.253		-.478	-.319			
	45.0	0.427								-.077					-.347			
	57.5		-0.135			.173		-.099	-.010					-.394				
	P.L.		-.135					-.031	.033	-.044			-.240	-.394	-.347		-.141	-.091

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(o) M = 1.02; $\alpha = 10.3^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of –																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0	P.L.		0.364					0.182	0.167	0.079			-0.105	-0.291	-0.363		-0.128	-0.005
	57.5		.364			0.398		.147	.157					-.291				
	45.0	0.543								.069					-.363			
	30.0			0.558		.430	0.312	.215	.121			-0.113		-.410	-.333			
	15.0							.287	.155	-.002		-.243	-.488	-.477	-.415	-0.174	-.128	
	10.0																	
	07.0									.045								
	03.0								.270			-.393	-.495	-.552	-.346	-.141	-.093	
	00.0				0.544			.349			-0.139		-.480			-.139	-.066	-.005
-4.4	P.L.		0.491					0.267	0.240	0.151			-0.039	-0.225	-0.315		-0.173	-0.064
	57.5		.491			0.477		.242	.234					-.225				
	45.0	0.560								.144					-.315			
	30.0			0.563		.485	0.412	.329	.215			-0.036		-.350	-.314			
	15.0							.355	.252	.103		-.160	-.461	-.464	-.460	-0.274	-.173	
	10.0																	
	07.0									.104								
	03.0								.277			-.361	-.507	-.615	-.453	-.196	-.123	
	00.0				0.539			.339			-0.170		-.537			-.203	-.132	-.064
4.4	00.0				0.527			0.335			-0.127		-0.556			-0.199	-0.138	-0.067
	03.0								0.239			-0.431	-.583	-0.578	-0.365	-.187	-.149	
	07.0									-0.069								
	10.0																	
	15.0							.185	.032	-.122		-.322	-.513	-.517	-.384	-.143	-.127	
	30.0			0.534		0.338	0.164	.089	.028			-.175		-.445	-.354			
	45.0	0.488								.007					-.388			
	57.5		0.198			.298		.052	.090					-.337				
	P.L.		.198					.101	.101	.020			-.164	-.337	-.388		-.127	-.067
-8.8	P.L.		0.565					0.356	0.319	0.224			0.025	-0.150	-0.257		-0.233	-0.085
	57.5		.565			0.524		.327	.303					-.150				
	45.0	0.516								.211					-.257			
	30.0			0.541		.493	0.457	.406	.289			0.023		-.287	-.267			
	15.0							.359	.305	.170		-.111	-.435	-.445	-.486	-0.439	-.233	
	10.0																	
	07.0									.096								
	03.0								.254			-.362	-.570	-.725	-.592	-.262	-.147	
	00.0				0.512			.308			-0.207		-.676			-.269	-.142	-.085
8.8	00.0				0.489			0.303			-0.145		-0.626			-0.262	-0.156	-0.092
	03.0								0.174			-0.495	-.717	-0.646	-0.435	-.272	-.169	
	07.0									-0.242								
	10.0																	
	15.0							.051	-.151	-.290		-.420	-.551	-.554	-.364	-.132	-.161	
	30.0			0.478		0.216	-0.084	-.068	-.073			-.246		-.488	-.359			
	45.0	0.401								-.064					-.408			
	57.5		-0.027			.185		-.053	.022					-.387				
	P.L.		-.027					.013	.036	-.039			-.219	-.387	-.408		-.161	-.092

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(p) M = 1.08; $\alpha = 0^{\circ}$

β, deg	ø, deg	Pressure coefficients for x/l of —																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0	P.L.		0.390					0.183	0.218	0.110			-0.086	-0.210	-0.180		-0.039	0.023
	57.5		.390			0.454		.180	.213					-.210				
	45.0									.146					-.180			
	30.0			0.690		.594	0.397	.305	.170			-0.009		-.290	-.186			
	15.0							.451	.260	.133		-.117	-.290	-.336	-.256	-0.049	-.039	
	10.0																	
	07.0									.230								
	03.0								.483			-.142	-.280	-.343	-.272	-.054	-.008	
	00.0				0.686			.566			0.113		-.290			-.063	-.002	.023
-4.4	P.L.		0.562					0.302	0.302	0.189			-0.007	-0.123	-0.121		-0.145	-0.001
	57.5		.562			0.573		.310	.308					-.123				
	45.0	0.717								.224					-.121			
	30.0			0.716		.673	0.541	.437	.301			0.085		-.192	-.127			
	15.0							.547	.406	.260		.000	-.232	-.266	-.234	-0.122	-.145	
	10.0																	
	07.0									.315								
	03.0								.497			-.102	-.290	-.391	-.311	-.136	-.043	
	00.0				0.693			.559			0.078		-.331			-.111	-.034	-.001
4.4	00.0				0.685			0.551			0.117		-0.344			-0.128	-0.019	-0.002
	03.0								0.451			-0.181	-.367	-0.383	-0.320	-.096	-.023	
	07.0									0.114								
	10.0																	
	15.0							.332	.129	-.022		-.215	-.326	-.370	-.288	-.040	-.029	
	30.0			0.662		0.501	0.195	.178	.041			-.076		-.323	-.216			
	45.0	0.591								.067					-.210			
	57.5		0.184			.349		.076	.143					-.254				
	P.L.		.184					.088	.159	.058			-.136	-.254	-.210		-.029	-.002
-8.8	P.L.		0.682					0.405	0.383	0.265			0.072	-0.042	-0.051		-0.225	-0.006
	57.5		.682			0.660		.418	.386					-.042				
	45.0	0.718								.302					-.051			
	30.0			0.700		.708	0.637	.545	.404			0.165		-.124	-.077			
	15.0							.589	.495	.356		.092	-.183	-.206	-.235	-0.169	-.225	
	10.0																	
	07.0									.349								
	03.0								.488			-.081	-.337	-.482	-.429	-.319	-.093	
	00.0				0.665			.532			0.046		-.442			-.212	-.080	-.006
8.8	00.0				0.658			0.527			0.093		-0.442			-0.289	-0.070	-0.005
	03.0								0.396			-0.271	-.561	-0.523	-0.420	-.184	-.070	
	07.0									-0.076								
	10.0																	
	15.0							.146	-.179	-.306		-.382	-.423	-.453	-.360	-.082	-.094	
	30.0			0.615		0.366	-0.174	-.015	-.196			-.187		-.407	-.258			
	45.0	0.499								-.049					-.242			
	57.5		-0.204			.189		-.056	-.022					-.317				
	P.L.		-.204					-.014	.028	-.026			-.204	-.317	-.242		-.094	-.005

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(q) M = 1.08; $\alpha = 5.2^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of –																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0	P.L.		0.397					0.218	0.235	0.131			-0.060	-0.214	-0.242		-0.060	0.019
	57.5		.397			0.462		.195	.215					-.214				
	45.0	0.635								.129					-.242			
	30.0			0.654		.538	0.379	.290	.181			-0.026		-.313	-.222			
	15.0							.394	.240	.121		-.126	-.352	-.368	-.282	-0.084	-.060	
	10.0																	
	07.0									.172								
	03.0								.408			-.227	-.354	-.412	-.294	-.070	-.031	
	00.0				0.652			.481			0.028		-.358			-.076	-.022	.019
-4.4	P.L.		0.545					0.316	0.306	0.201			0.010	-0.143	-0.194		-0.130	-0.006
	57.5		.545			0.557		.301	.295					-.143				
	45.0	0.673								.208					-.194			
	30.0			0.672		.604	0.505	.390	.286			0.051		-.251	-.191			
	15.0							.478	.356	.224		-.042	-.305	-.335	-.292	-0.170	-.130	
	10.0																	
	07.0									.244								
	03.0								.416			-.201	-.325	-.445	-.335	-.113	-.058	
	00.0				0.648			.475			0.008		-.398			-.105	-.055	-.006
4.4	00.0				0.634			0.471			0.048		-0.406			-0.123	-0.051	-0.014
	03.0								0.372			-0.278	-.488	-0.444	-0.334	-.105	-.076	
	07.0									0.028								
	10.0																	
	15.0							.272	.085	-.036		-.245	-.390	-.427	-.295	-.055	-.034	
	30.0			0.622		0.438	0.183	.147	.073			-.106		-.367	-.252			
	45.0	0.568								.050					-.273			
	57.5		0.185			.347		.077	.142					-.274				
	P.L.		.185					.118	.166	.063			-.123	-.274	-.273		-.034	-.014
-8.8	P.L.		0.648					0.414	0.387	0.280			0.085	-0.065	-0.118		-0.200	-0.010
	57.5		.648			0.626		.402	.378					-.065				
	45.0	0.654								.288					-.118			
	30.0			0.651		.633	0.575	.508	.383			0.133		-.181	-.135			
	15.0							.510	.434	.314		.041	-.263	-.282	-.311	-0.265	-.200	
	10.0																	
	07.0									.265								
	03.0								.402			-.188	-.403	-.564	-.458	-.209	-.076	
	00.0				0.609			.445			-0.037		-.533			-.189	-.071	-.010
8.8	00.0				0.606			0.445			0.023		-0.525			-0.205	-0.068	-0.016
	03.0								0.308			-0.358	-.639	-0.551	-0.439	-.194	-.078	
	07.0									-0.161								
	10.0																	
	15.0							.138	-.197	-.266		-.350	-.447	-.476	-.323	-.074	-.068	
	30.0			0.570		0.308	-0.137	-.038	-.142			-.184		-.409	-.269			
	45.0	0.477								-.033					-.291			
	57.5		-0.127			.214		-.038	.004					-.322				
	P.L.		-.127					.027	.053	.002			-.174	-.322	-.291		-.068	-.016

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(r) M = 1.08; $\alpha = 10.3^\circ$

β, deg	ø, deg	Pressure coefficients for x/l of —																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0	P.L.		0.410					0.231	0.224	0.144			-0.035	-0.202	-0.285		-0.077	0.062
	57.5		.410			0.447		.198	.216					-.202				
	45.0	0.587								.136					-.285			
	30.0			0.600		.476	0.361	.267	.182			-0.036		-.322	-.268			
	15.0							.333	.217	.071		-.150	-.389	-.395	-.337	-0.130	-.077	
	10.0																	
	07.0									.118								
	03.0								.329			-.295	-.403	-.451	-.281	-.096	-.044	
	00.0				0.585			.394			-0.055		-.396			-.097	-.018	.062
-4.3	P.L.		0.539					0.319	0.299	0.219			0.035	-0.142	-0.230		-0.120	0.018
	57.5		.539			0.528		.296	.297					-.142				
	45.0	0.604								.215					-.230			
	30.0			0.606		.534	0.458	.382	.278			0.042		-.253	-.231			
	15.0							.403	.315	.173		-.070	-.361	-.373	-.381	-0.256	-.120	
	10.0																	
	07.0									.174								
	03.0								.336			-.269	-.417	-.536	-.400	-.154	-.070	
	00.0				0.581			.386			-0.091		-.458			-.160	-.080	.018
4.3	00.0				0.571			0.383			-0.048		-0.450			-0.147	-0.088	0.016
	03.0								0.299			-0.333	-.484	-0.480	-0.305	-.137	-.091	
	07.0									0.007								
	10.0																	
	15.0							.240	.105	-.052		-.226	-.410	-.420	-.314	-.094	-.069	
	30.0			0.581		0.389	0.219	.149	.097			-.088		-.356	-.275			
	45.0	0.538								.075					-.311			
	57.5		0.251			.351		.110	.157					-.250				
	P.L.		.251					.153	.165	.089			-.085	-.250	-.311		-.069	.016
-8.8	P.L.		0.614					0.407	0.378	0.290			0.099	-0.077	-0.176		-0.136	-0.002
	57.5		.614			0.577		.382	.363					-.077				
	45.0	0.566								.279					-.176			
	30.0			0.589		.549	0.509	.459	.350			0.103		-.202	-.192			
	15.0							.414	.367	.243		-.019	-.337	-.350	-.389	-0.398	-.136	
	10.0																	
	07.0									.169								
	03.0								.319			-.263	-.468	-.619	-.502	-.203	-.067	
	00.0				0.563			.365			-0.116		-.577			-.214	-.064	-.002
8.8	00.0				0.534			0.351			-0.078		-0.548			-0.207	-0.084	-0.018
	03.0								0.224			-0.423	-.675	-0.576	-0.395	-.230	-.102	
	07.0									-0.214								
	10.0																	
	15.0							.092	-.163	-.232		-.348	-.465	-.472	-.298	-.063	-.086	
	30.0			0.525		0.253	-0.058	-.017	-.067			-.172		-.411	-.287			
	45.0	0.450								-.010					-.334			
	57.5		-0.014			.228		.010	.045					-.311				
	P.L.		-.014					.068	.067	.021			-.149	-.311	-.334		-.086	-.018

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(s) $M = 1.13$; $\alpha = 0^\circ$

β, deg	ø, deg	Pressure coefficients for x/l of –																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0	P.L.		0.382					0.178	0.242	0.141			-0.048	-0.177	-0.166		-0.050	0.026
	57.5		.382			0.461		.180	.233					-.177				
	45.0	0.677								.166					-.166			
	30.0			0.703		.599	0.401	.312	.185			0.020		-.256	-.171			
	15.0							.455	.277	.165		-.074	-.249	-.294	-.238	-0.057	-.050	
	10.0																	
	07.0									.259								
	03.0								.510			-.109	-.257	-.307	-.248	-.067	-.018	
	00.0				0.702			.575			0.148		-.248			-.076	-.012	.026
-4.4	P.L.		0.557					0.297	0.321	0.206			0.026	-0.105	-0.116		-0.159	0.001
	57.5		.557			0.576		.304	.322					-.105				
	45.0	0.732								.241					-.116			
	30.0			0.730		.679	0.547	.441	.311			.113		-.175	-.122			
	15.0							.557	.419	.286		.036	-.201	-.248	-.222	-0.122	-.159	
	10.0																	
	07.0									.344								
	03.0								.525			-.070	-.257	-.345	-.276	-.152	-.053	
	00.0				0.701			.571			0.124		-.308			-.130	-.043	.001
4.4	00.0				0.697			0.564			0.144		-0.300			-0.148	-0.037	-0.008
	03.0								0.471			-0.166	-.345	-0.346	-0.293	-.113	-.042	
	07.0									0.109								
	10.0																	
	15.0							.339	.096	-.028		-.193	-.305	-.343	-.276	-.041	-.035	
	30.0			0.668		0.494	0.175	.179	.008			-.064		-.309	-.206			
	45.0	0.603								.078					-.198			
	57.5		0.144			.343		.075	.101					-.229				
	P.L.		.144					.080	.133	.072			-.103	-.229	-.198		-.035	-.008
-8.9	P.L.		0.690					0.411	0.406	0.286			0.100	-0.025	-0.044		-0.230	-0.028
	57.5		.690			0.669		.424	.407					-.025				
	45.0	0.738								.326					-.044			
	30.0			0.721		.721	0.647	.556	.423			0.195		-.100	-.062			
	15.0							.602	.516	.386		.131	-.147	-.189	-.207	-0.167	-.230	
	10.0																	
	07.0									.382								
	03.0								.520			-.046	-.284	-.430	-.415	-.376	-.100	
	00.0				0.681			.545			0.096		-.386			-.255	-.092	-.028
8.9	00.0				0.682			0.543			0.133		-0.391			-0.353	-0.094	-0.038
	03.0								0.431			-0.228	-.515	-0.528	-0.391	-.221	-.096	
	07.0									-0.035								
	10.0																	
	15.0							.189	-.179	-.280		-.372	-.391	-.412	-.340	-.098	-.105	
	30.0			0.638		0.372	-0.191	.003	-.192			-.160		-.371	-.236			
	45.0	0.534								-.031					-.228			
	57.5		-0.250			.201		-.044	-.024					-.279				
	P.L.		-.250					-.008	.027	-.009			-.164	-.279	-.228		-.105	-.038

TABLE II.- Continued

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(t) $M = 1.13$; $\alpha = 5.2^{\circ}$

β, deg	ϕ, deg	Pressure coefficients for x/l of —																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0	P.L.		0.396					0.222	0.255	0.162			-0.023	-0.184	-0.222		-0.059	0.018
	57.5		.396			0.446		.191	.235					-.184				
	45.0	0.640								.167					-.222			
	30.0			0.665		.528	0.384	.283	.200			0.015		-.270	-.204			
	15.0							.405	.255	.152		-.103	-.304	-.333	-.277	-0.099	-.059	
	10.0																	
	07.0									.211								
	03.0								.432			-.188	-.316	-.360	-.274	-.083	-.028	
	00.0				0.671			.492			0.058		-.327			-.089	-.017	.018
-4.4	P.L.		0.555					0.318	0.324	0.225			0.043	-0.121	-0.179		-0.137	-0.006
	57.5		.555			0.553		.302	.312					-.121				
	45.0	0.682								.234					-.179			
	30.0			0.679		.608	0.510	.402	.301			0.083		-.216	-.181			
	15.0							.484	.373	.251		-.011	-.267	-.309	-.288	-0.187	-.137	
	10.0																	
	07.0									.277								
	03.0								.434			-.166	-.337	-.410	-.322	-.136	-.062	
	00.0				0.657			.480			0.028		-.363			-.123	-.060	-.006
4.4	00.0				0.651			0.484			0.063		-0.377			-0.135	-0.062	-0.015
	03.0								0.384			-0.242	-.431	-0.401	-0.320	-.115	-.088	
	07.0									0.051								
	10.0																	
	15.0							.287	.088	-.012		-.210	-.346	-.385	-.287	-.058	-.044	
	30.0			0.635		0.434	0.181	.157	.043			-.066		-.334	-.233			
	45.0	0.582								.082					-.251			
	57.5		0.185			.333		.086	.121					-.239				
	P.L.		.185					.127	.157	.096			-.083	-.239	-.251		-.044	-.015
-8.9	P.L.		0.665					0.422	0.405	0.305			0.111	-0.038	-0.107		-0.229	-0.040
	57.5		.665			0.639		.413	.400					-.038				
	45.0	0.663								.318					-.107			
	30.0			0.661		.643	0.588	.518	.405			0.170		-.144	-.118			
	15.0							.520	.458	.346		.079	-.227	-.250	-.292	-0.279	-.229	
	10.0																	
	07.0									.296								
	03.0								.422			-.147	-.379	-.527	-.491	-.230	-.103	
	00.0				0.627			.455			-0.008		-.488			- 206	-.098	-.040
8.9	00.0				0.624			0.466			0.047		-0.467			-0.223	-0.106	-0.050
	03.0								0.339			-0.310	-.558	-0.543	-0.412	-.206	-.118	
	07.0									-0.112								
	10.0																	
	15.0							.148	-.173	-.249		-.326	-.399	-.425	-.316	-.082	-.118	
	30.0			0.588		0.305	-0.137	.004	-.128			-.148		-.368	-.249			
	45.0	0.503								-.008					-.271			
	57.5		-0.150			.205		-.002	.015					-.283				
	P.L.		-.150					.050	.063	.029			-.135	-.283	-.271		-.118	-.050

TABLE II.- Concluded

PRESSURE COEFFICIENTS FOR LARGE FLAT-WINDSHIELD CANOPY 1

(u) $M = 1.13$; $\alpha = 10.3^\circ$

β, deg	ø, deg	Pressure coefficients for x/l of –																
		0.000	0.001	0.004	0.006	0.017	0.046	0.092	0.164	0.216	0.240	0.260	0.311	0.356	0.440	0.600	0.828	0.988
0	P.L.		0.407					0.233	0.235	0.161			-0.011	-0.172	-0.263		-0.081	0.045
	57.5		.407			0.446		.196	.232					-.172				
	45.0	0.589								.153					-.263			
	30.0			0.598		.469	0.368	.268	.202			-0.003		-.286	-.260			
	15.0							.337	.234	.120		-.117	-.350	-.371	-.320	-0.137	-.081	
	10.0																	
	07.0									.147								
	03.0								.346			-.255	-.369	-.412	-.280	-.096	-.049	
	00.0				0.595			.399			-0.022		-.386			-.095	-.021	.045
-4.4	P.L.		0.541					0.314	0.306	0.226			0.047	-0.121	-0.216		-0.127	-0.007
	57.5		.541			0.531		.288	.300					-.121				
	45.0	0.615								.220					-.216			
	30.0			0.614		.540	0.459	.380	.280			0.053		-.240	-.232			
	15.0							.401	.312	.201		-.050	-.330	-.358	-.353	-0.236	-.127	
	10.0																	
	07.0									.195								
	03.0								.345			-.244	-.395	-.480	-.358	-.152	-.083	
	00.0				0.593			.391			-0.052		-.426			-.158	-.097	-.007
4.4	00.0				0.575			0.387			-0.022		-0.429			-0.151	-0.105	-0.014
	03.0								0.299			-0.309	-.464	-0.432	-0.292	-.140	-.105	
	07.0									0.014								
	10.0																	
	15.0							.232	.079	-.014		-.200	-.375	-.394	-.293	-.091	-.079	
	30.0			0.585		0.383	0.212	.145	.067			-.067		-.333	-.264			
	45.0	0.540								.084					-.297			
	57.5		0.238			.352		.109	.134					-.226				
	P.L.		.238					.157	.147	.101			-.066	-.226	-.297		-.079	-.014
-8.6	P.L.		0.617					0.408	0.389	0.306			0.126	-0.054	-0.147		-0.182	-0.039
	57.5		.617			0.580		.379	.375					-.054				
	45.0	0.570								.297					-.147			
	30.0			0.595		.551	0.509	.463	.364			0.129		-.163	-.169			
	15.0							.419	.379	.283		.021	-.298	-.311	-.363	-0.396	-.182	
	10.0																	
	07.0									.200								
	03.0								.337			-.217	-.429	-.582	-.510	-.222	-.109	
	00.0				0.571			.371			-0.085		-.554			-.226	-.108	-.039
8.6	00.0				0.548			0.361			-0.046		-0.513			-0.225	-0.130	-0.044
	03.0								0.247			-0.374	-.606	-0.521	-0.376	-.237	-.158	
	07.0									-0.173								
	10.0																	
	15.0							.110	-.123	-.192		-.300	-.412	-.429	-.291	-.084	-.130	
	30.0			0.542		0.262	-0.036	.018	-.060			-.137		-.372	-.272			
	45.0	0.474								.011					-.317			
	57.5		-0.008			.247		.038	.050					-.273				
	P.L.		-.008					.093	.073	.037			-.119	-.273	-.317		-.130	-.044

TABLE III

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(a) M = 0.80; $\alpha = 0^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0	P.L.	0.426	0.341	0.308	0.269	0.225	0.145	-0.030		-0.136		-0.237			-0.183	-0.110	-0.026	-0.038	0.052
	57.5						.145								-.183				
	51.0						.189	-.005											
	48.0							.009											
	45.0				.269				-0.077			-.389				-.110			
	41.0									-.076									
	34.0											-.859							
	30.0			.308				.138				-.601	-0.999		-.463	-.126	-.026		
	15.0		.341		.314		.251			.118		-.136		-1.234	-.810	-.117	-.038	-.038	
	03.0	.426	.395	.377	.361		.322			.136	-0.248	-.373			-.677	-.117	-.065	-.020	.052
	01.0							.281											
	00.0																-.061	-.009	
-4.3	P.L.	0.567	0.447	0.423	0.382	0.342	0.261	0.081		-0.037		-0.142			-0.110	-0.090	-0.039	-0.091	0.022
	57.5						.261								-.110				
	51.0						.302	.121											
	48.0							.135											
	45.0				.382				0.047			-.263				-.090			
	41.0									.041									
	34.0											-.569							
	30.0			.423				.236				-.421	-0.720		-.416	-.119	-.039		
	15.0		.447		.395		.356			.198		-.063		-1.194	-.952	-.137	-.065	-.091	
	03.0	.567	.458	.458	.443		.401			.168	-0.382	-.494			-.636	-.181	-.127	-.062	.022
	01.0							.332											
	00.0																-.112	-.034	
4.3	00.0																-0.099	-0.022	
	01.0							0.088											
	03.0	0.224	0.269	0.270	0.247		0.214			0.031	-0.239	-0.385			-0.667	-0.153	-.088	-.027	0.030
	15.0		.221		.216		.173			.042		-.193		-1.208	-.805	-.146	-.031	-.010	
	30.0			.196				.051				-.652	-1.168		-.492	-.124	-.012		
	34.0											-1.011							
	41.0									-.165									
	45.0				.161				-0.173			-.477				-.115			
	48.0							-.088											
	51.0						.095	-.095											
	57.5						.047								-.215				
	P.L.	.224	.221	.196	.161	0.128	.047	-.114		-.205		-.300			-.215	-.115	-.012	-.010	.030
-8.6	P.L.	0.596	0.535	0.506	0.457	0.419	0.354	0.176		0.053		-0.060			-0.049	-0.071	-0.044	-0.145	-0.002
	57.5						.354								-.049				
	51.0						.385	.215											
	48.0							.233											
	45.0				.457				0.149			-.158				-.071			
	41.0									.138									
	34.0											-.404							
	30.0			.506				.314				-.299	-0.511		-.331	-.107	-.044		
	15.0		.535		.472		.420			.258		-.010		-1.173	-1.026	-.165	-.104	-.145	
	03.0	.596	.458	.461			.408			.122	-0.567	-.631			-.528	-.292	-.229	-.108	-.002
	01.0							.299											
	00.0																-.206	-.069	
8.6	00.0																-0.203	-0.061	
	01.0							-0.301											
	03.0	-0.131	-0.163	-0.397	-0.186		-0.321			-0.260	-0.357	-0.465			-0.653	-0.252	-.152	-.065	-0.001
	15.0		.045		.089		.072			-.038		-.245		-1.247	-.856	-.193	-.063	-.074	
	30.0			.041				-.049				-.739	-1.356		-.670	-.127	-.010		
	34.0											-1.230							
	41.0									-.278									
	45.0				.018				-0.297			-.613				-.127			
	48.0							-.211											
	51.0						-.032	-.215											
	57.5						-.082								-.257				
	P.L.	-.131	.045	.041	.018	-0.012	-.082	-.227		-.301		-.380			-.257	-.127	-.010	-.074	-.001

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(b) $M = 0.80$; $\alpha = 5.1^{\circ}$

β, deg	ϕ, deg	Pressure coefficients for x/l of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0.5	P.L.	0.331	0.347	0.267	0.249	0.217	0.157	-0.001		-0.116		-0.238			-0.218	-0.173	-0.065	-0.054	0.046
	57.5						.157								-.218				
	51.0						.195	.027											
	48.0							.036											
	45.0				.249				-0.051	-.108		-.380				-.173			
	41.0									-.072									
	34.0											-.671							
	30.0			.267				.100				-.519	-0.878		-.541	-.171	-.065		
	15.0		.347		.256		.204			.058		-.185		-1.238	-.845	-.139	-.062	-.054	
	03.0	.331	.345	.306	.272		.230			.051	-0.366	-.483			-.780	-.123	-.065	-.027	.046
	01.0							.193									-.072	-.016	
-3.8	P.L.	0.462	0.448	0.372	0.340	0.311	0.255	0.097		-0.027		-0.153			-0.149	-0.164	-0.089	-0.113	0.018
	57.5						.255								-.149				
	51.0						.285	.126											
	48.0							.136											
	45.0				.340				0.055	-.002		-.264				-.164			
	41.0									.030									
	34.0											-.476							
	30.0			.372				.188				-.383	-0.611		-.453	-.172	-.089		
	15.0		.448		.347		.287			.132		-.118		-1.220	-1.029	-.167	-.105	-.113	
	03.0	.462	.414	.375	.356		.304			.068	-0.523	-.622			-.756	-.196	-.116	-.053	.018
	01.0							.231											
	00.0																-.101	-.042	
4.8	00.0																-.107	-0.041	
	01.0							-0.072											
	03.0	0.143	0.235	0.172	0.123		0.120			-0.115	-0.387	-0.513			-0.768	-0.175	-.088	-.047	0.017
	15.0		.192		.173		.125			-.014		-.235		-1.184	-.798	-.145	-.042	-.037	
	30.0			.161				.026				-.630	-0.996		-.508	-.165	-.044		
	34.0											-.847							
	41.0									-.153									
	45.0				.155				-0.135	-.181		-.452				-.174			
	48.0							-.057											
	51.0						.110	-.061											
	57.5						.076								-.253				
	P.L.	.143	.192	.161	.155	0.131	.076	-.074		-.181		-.301			-.253	-.174	-.044	-.037	.017
-8.1	P.L.	0.532	0.521	0.451	0.412	0.384	0.342	0.179		0.050		-0.086			-0.099	-0.152	-0.096	-0.155	0.007
	57.5						.342								-.099				
	51.0						.360	.203											
	48.0							.213											
	45.0				.412				0.132	.067		-.185				-.152			
	41.0									.104									
	34.0											-.359							
	30.0			.451				.252				-.285	-0.492		-.378	-.169	-.096		
	15.0		.521		.399		.345			.184		-.073		-1.203	-1.110	-.210	-.147	-.155	
	03.0	.532	.415	.378	.353		.306			.033	-0.653	-.710			-.701	-.270	-.170	-.067	.007
	01.0							.202											
	00.0																-.138	-.057	
9.1	00.0																-0.156	-0.062	
	01.0							-0.343											
	03.0	-0.254	-0.376	-0.487	-0.294		-0.350			-0.323	-0.480	-0.571			-0.701	-0.238	-.135	-.076	-0.007
	15.0		-.011		.057		.014			-.068		-.258		-1.212	-.790	-.167	-.057	-.098	
	30.0			.002				-.078				-.727	-1.252		-.561	-.153	-.036		
	34.0											-1.087							
	41.0									-.262									
	45.0				.018				-0.243	-.272		-.552				-.174			
	48.0							-.173											
	51.0						-.014	-.178											
	57.5						-.042								-.303				
	P.L.	-.254	-.011	.002	.018	0.001	-.042	-.178		-.264		-.381			-.303	-.174	-.036	-.098	-.007

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(c) M = 0.80; α = 10.2°

β, deg	ø, deg	Pressure coefficients for x/l of –																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0.4	P.L.	0.292	0.243	0.250	0.242		0.189	0.035		-0.070		-0.237			-0.245	-0.241	-0.110	-0.062	0.054
	57.5						.189								-.245				
	51.0						.206	.050											
	48.0							.050								-.241			
	45.0				.242				-0.017			-.334							
	41.0									-.054									
	34.0											-.560							
	30.0			.250				.084				-.475	-0.729		-.552	-.227	-.110		
	15.0		.243		.229		.163			.012		-.230		-1.196	-.815	-.168	-.082	-.062	
	03.0	.292	.250	.237	.212		.164			-.026	-0.473	-.577			-.791	-.129	-.067	-.032	.054
	01.0							-.069									-.061	-.021	
	00.0																		
-3.8	P.L.	0.386	0.336	0.329	0.304		0.258	0.115		0.005		-0.171			-0.191	-0.248	-0.143	-0.114	0.032
	57.5						.258								-.191				
	51.0						.267	.120											
	48.0							.124								-.248			
	45.0				.304				0.060			-.245							
	41.0									.017									
	34.0											-.417							
	30.0			.329				.149				-.361	-0.541		-.466	-.243	-.143		
	15.0		.336		.300		.229			.071		-.174		-1.221	-.981	-.222	-.145	-.114	
	03.0	.386	.309	.301	.283		.215			-.028	-0.645	-.728			-.755	-.191	-.109	-.057	.032
	01.0							-.038									-.089	-.044	
	00.0																		
4.7	00.0																-0.098	-0.043	
	01.0							-0.040											
	03.0	0.070	0.113	0.110	0.074		0.028			-0.148	-0.477	-0.589			-0.764	-0.156	-.085	-.057	0.022
	15.0		.129		.152		.087			-.045		-.280		-1.145	-.789	-.167	-.054	-.054	
	30.0			.138				.005				-.595	-0.864		-.574	-.206	-.073		
	34.0											-.705							
	41.0									-.139									
	45.0				.156				-0.096			-.410				-.227			
	48.0							-.032											
	51.0						.117	-.038											
	57.5						.098								-.285				
	P.L.	.070	.129	.138	.156		.098	-.044		-.135		-.301			-.285	-.227	-.073	-.054	.022
-8.2	P.L.	0.450	0.417	0.405	0.379		0.339	0.202		0.094		-0.094			-0.126	-0.238	-0.156	-0.148	0.022
	57.5						.339								-.126				
	51.0						.346	.199											
	48.0							.199								-.238			
	45.0				.379				0.136			-.160							
	41.0									.090									
	34.0											-.293							
	30.0			.405				.203				-.256	-0.408		-.393	-.249	-.156		
	15.0		.417		.345		.276			.115		-.129		-1.191	-1.130	-.288	-.203	-.148	
	03.0	.450	.305	.290	.268		.209			-.074	-0.785	-.838			-.743	-.242	-.134	-.062	.022
	01.0							-.058									-.124	-.058	
	00.0																		
9.0	00.0																-0.134	-0.064	
	01.0							-0.062											
	03.0	-0.290	-0.381	-0.509	-0.316		-0.344			-0.367	-0.569	-0.635			-0.711	-0.189	-.130	-.079	0.003
	15.0		-.043		.049		-.026			-.086		-.298		-1.176	-.768	-.146	-.067	-.095	
	30.0			-.008				-.081				-.713	-1.056		-.579	-.191	-.064		
	34.0											-.881							
	41.0									-.220									
	45.0				.046				-0.190			-.491				-.224			
	48.0							-.130											
	51.0						.023	-.129							-.336				
	57.5						-.005								-.336				
	P.L.	-.290	-.043	-.008	.046		-.005	-.134		-.210		-.374				-.224	-.064	-.095	.003

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(d) $M = 0.90$; $\alpha = 0^\circ$

β, deg	∅, deg	Pressure coefficients for x/l of –																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0	P.L.	0.463	0.374	0.345	0.307	0.265	0.192	0.010		-0.096		-0.250			-0.256	-0.234	-0.007	-0.043	0.041
	57.5						.192								-.256				
	51.0						.235	.042											
	48.0							.056											
	45.0				.307				-0.025			-.452				-.234			
	41.0									-.014									
	34.0											-.804							
	30.0			.345				.185				-.446	-0.969		-.632	-.180	-.007		
	15.0		.374		.357		.305			.178		-.039		-0.962	-1.066	-.223	-.017	-.043	
	03.0	.463	.432	.412	.400		.364			.196	-0.169	-.285			-.604	-.310	-.041	-.024	.041
	01.0							.340											
	00.0																-.039	-.014	
-4.3	P.L.	0.600	0.472	0.450	0.416	0.375	0.296	0.111		-0.012		-0.150			-0.159	-0.188	-0.033	-0.089	0.018
	57.5						.296								-.159				
	51.0						.341	.159											
	48.0							.172											
	45.0				.416				0.086			-.266				-.188			
	41.0									.088									
	34.0											-.601							
	30.0			.450				.273				-.364	-0.733		-.502	-.141	-.033		
	15.0		.472		.429		.394			.249		.020		-0.928	-1.068	-.146	-.061	-.089	
	03.0	.600	.494	.491	.481		.438			.230	-0.285	-.394			-.624	-.208	-.112	-.055	.018
	01.0							.386											
	00.0																-.099	-.036	
4.3	00.0																-0.090	-0.030	
	01.0							0.133											
	03.0	0.258	0.302	0.305	0.283		0.254			0.090	-0.154	-0.288			-0.623	-0.289	-.070	-.036	0.017
	15.0		.247		.254		.215			.101		-.097		-0.977	-.908	-.464	-.010	-.023	
	30.0			.225				.095				-.502	-1.036		-.741	-.389	.028		
	34.0											-.903							
	41.0									-.101									
	45.0				.196				-0.123			-.575				-.270			
	48.0							-.049											
	51.0						.136	-.057											
	57.5						.090								-.332				
	P.L.	.258	.247	.225	.196	0.162	.090	-.081		-.162		-.336			-.332	-.270	.028	-.023	.017
-8.7	P.L.	0.626	0.567	0.543	0.495	0.458	0.395	0.213		0.081		-0.057			-0.075	-0.142	-0.051	-0.147	-0.014
	57.5						.395								-.075				
	51.0						.428	.257											
	48.0							.273											
	45.0				.495				0.189			-.154				-.142			
	41.0									.182									
	34.0											-.380							
	30.0			.543				.354				-.225	-0.558		-.366	-.121	-.051		
	15.0		.567		.512		.461			.309		.073		-0.909	-1.056	-.148	-.112	-.147	
	03.0	.626	.497	.498	.488		.448			.185	-0.489	-.548			-.676	-.285	-.234	-.097	-.014
	01.0							.351											
	00.0																.210	.075	
8.7	00.0																-0.202	-0.070	
	01.0							-0.256											
	03.0	-0.073	-0.155	-0.342	-0.139		-0.160			-0.187	-0.280	-0.369			-0.678	-0.289	-.145	-.077	-0.019
	15.0		.081		.127		.113			.013		-.141		-1.007	-.878	-.494	-.052	-.092	
	30.0			.076				-.003				-.558	-1.119		-.814	-.479	.036		
	34.0											-1.020							
	41.0									-.207									
	45.0				.053				-0.243			-.692				-.308			
	48.0							-.171											
	51.0						.015	-.170											
	57.5						-.037								-.417				
	P.L.	-.073	.081	.076	.053	0.026	-.037	-.191		-.235		-.416			-.417	-.308	.036	-.092	-.019

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(e) M = 0.90; α = 5.1°

β, deg	ϕ, deg	Pressure coefficients for x/l of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0.5	P.L.	0.363	0.381	0.300	0.286	0.256	0.198	0.038		-0.078		-0.226			-0.237	-0.467	-0.037	-0.058	0.036
	57.5						.198								-.237				
	51.0						.238	.071											
	48.0							.079											
	45.0				.286				-0.000	-.054		-.377				-.467			
	41.0									-.013									
	34.0											-.681							
	30.0			.300				.143				-.454	-0.840		-.581	-.449	-.037		
	15.0		.381		.295		.248			.118		-.092		-0.989	-1.124	-.315	-.040	-.058	
	03.0	.363	.381	.341	.308		.270			.115	-0.276	-.385			-.684	-.286	-.035	-.032	.036
	01.0							.243											
	00.0																-.043	-.023	
-3.8	P.L.	0.487	0.475	0.400	0.371	0.343	0.290	0.131		0.005		-0.142			-0.157	-0.397	-0.079	-0.114	0.011
	57.5						.290								-.157				
	51.0						.320	.164											
	48.0							.174											
	45.0				.371				0.096	.039		-.251				-.397			
	41.0									.078									
	34.0											-.470							
	30.0			.400				.228				-.343	-0.590		-.451	-.482	-.079		
	15.0		.475		.381		.325			.184		-.033		-0.952	-1.105	-.311	-.099	-0.114	
	03.0	.487	.449	.409	.391		.343			.132	-0.429	-.519			-.714	-.279	-.099	-.056	.011
	01.0							.280											
	00.0																-.080	-.049	
4.9	00.0																-.090	-.050	
	01.0							-.054											
	03.0	0.140	0.245	0.173	0.116		0.126			-0.071	-0.287	-0.395			-0.709	-0.300	-.070	-.063	0.004
	15.0		.256		.189		.155			.036		-.147		-1.009	-.828	-.530	-.006	-.035	
	30.0			.174				.059				-.527	-1.032		-.666	-.421	.001		
	34.0											-.863							
	41.0									-.105									
	45.0				.173				-0.105	-.139		-.530				-.366			
	48.0							-.036											
	51.0						.133	-.042											
	57.5						.099								-.330				
	P.L.	.140	.256	.174	.173	0.144	.099	-.057		-.153		-.320			-.330	-.366	.001	-.035	.004
-8.2	P.L.	0.571	0.565	0.494	0.453	0.430	0.387	0.226		0.094		-0.056			-0.082	-0.323	-0.103	-0.166	-0.012
	57.5						.387								-.082				
	51.0						.409	.255											
	48.0							.264											
	45.0				.453				0.188	.125		-.149				-.323			
	41.0									.161									
	34.0											-.286							
	30.0			.494				.300				-.197	-0.447		-.343	-.425	-.103		
	15.0		.565		.446		.389			.243		.020		-0.928	-1.083	-.337	-.161	-.166	
	03.0	.571	.454	.416	.394		.352			.093	-0.602	-.648			-.746	-.308	-.174	-.079	-.012
	01.0							.247											
	00.0																-.131	-.074	
9.3	00.0																-0.138	-0.078	
	01.0							-0.290											
	03.0	-0.197	-0.327	-0.446	-0.252		-0.300			-0.256	-0.391	-0.466			-0.748	-0.311	-.129	-.092	-0.019
	15.0		.085		.093		.052			-.007		-.152		-1.010	-.873	-.552	-.036	-.102	
	30.0			.034				-.036				-.578	-1.097		-.769	-.469	.019		
	34.0											-.960							
	41.0									-.189									
	45.0				.048				-0.189	-.195		-.613				-.386			
	48.0							-.135											
	51.0						.026	-.138											
	57.5						-.001								-.397				
	P.L.	-.197	.085	.034	.048	0.034	-.001	-.142		-.214		-.393			-.397	-.386	.019	-.102	-.019

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(f) M = 0.90; $\alpha = 10.2^{\circ}$

β, deg	ϕ, deg	Pressure coefficients for x/l of –																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0.4	P.L.	0.325	0.277	0.283	0.278		0.229	0.074		-0.029		-0.214			-0.228	-0.490	-0.089	-0.073	0.036
	57.5						.229								-.228				
	51.0						.248	.094											
	48.0							.093								-.490			
	45.0				.278				0.033			-.308							
	41.0									.001									
	34.0											-.534							
	30.0			.283				.127				-.425	-0.661		-.519	-.630	-.089		
	15.0		.277		.267		.203			.072		-.137		-0.985	-1.160	-.420	-.061	-.073	
	03.0	.325	.282	.271	.252		.204			.042	-0.388	-.464			-.750	-.353	-.033	-.049	.036
	01.0							.064									-.023	-.035	
	00.0																		
-3.9	P.L.	0.416	0.367	0.361	0.339		0.293	0.153		0.044		-0.142			-0.168	-0.428	-0.130	-0.111	0.013
	57.5						.293								-.168				
	51.0						.305	.164											
	48.0							.167								-.428			
	45.0				.339				0.110			-.211							
	41.0									.069									
	34.0											-.365							
	30.0			.361				.191				-.290	-0.509		-.406	-.553	-.130		
	15.0		.367		.340		.270			.128		-.083		-0.953	-1.125	-.558	-.134	-.111	
	03.0	.416	.344	.335	.322		.260			.041	-0.548	-.610			-.782	-.392	-.086	-.066	.013
	01.0							.082									-.079	-.065	
	00.0																		
4.7	00.0																-0.088	-0.063	
	01.0							0.072											
	03.0	0.104	0.149	0.143	0.104		0.065			-0.085	-0.393	-0.474			-0.772	-0.401	-.074	-.081	0.011
	15.0		.157		.186		.126			.017		-.188		-1.002	-.925	-.535	-.021	-.059	
	30.0			.166				.047				-.524	-0.837		-.614	-.491	-.044		
	34.0											-.689							
	41.0									-.078									
	45.0								-0.043			-.412				-.490			
	48.0				.189			.007											
	51.0						.156	-.001											
	57.5						.135								-.302				
	P.L.	.104	.157	.166	.189		.135	-.009		-.090		-.288			-.302	-.490	-.044	-.059	.011
-8.3	P.L.	0.482	0.450	0.439	0.415		0.376	0.239		0.130		-0.061			-0.099	-0.370	-0.137	-0.143	0.005
	57.5						.376								-.099				
	51.0						.383	.241											
	48.0							.242								-.370			
	45.0				.415				0.184			-.128							
	41.0									.141									
	34.0											-.246							
	30.0			.439				.249				-.190	-0.366		-.335	-.502	-.137		
	15.0		.450		.385		.317			.174		-.037		-0.935	-1.096	-.632	-.187	-.143	
	03.0	.482	.345	.330	.312		.254			-.003	-0.657	-.699			-.809	-.418	-.114	-.072	.005
	01.0							.072									-.114	-.072	
	00.0																		
9.1	00.0																-0.125	-0.075	
	01.0							0.051											
	03.0	-0.219	-0.328	-0.409	-0.248		-0.273			-0.288	-0.465	-0.520			-0.790	-0.426	-.129	-.091	0.001
	15.0		-.003		.096		.020			-.019		-.198		-1.004	-.886	-.603	-.019	-.097	
	30.0			.029				-.035				-.589	-0.981		-.683	-.504	-.022		
	34.0											-.818							
	41.0									-.146									
	45.0				.086				-0.130			-.501				-.489			
	48.0							-.087											
	51.0						.071	-.086							-.380				
	57.5						.039												
	P.L.	-.219	-.003	.029	.086		.039	-.094		-.161		-.359			-.380	-.489	-.022	-.097	.001

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(g) M = 0.95; $\alpha = 0^\circ$

β, deg	ø, deg	Pressure coefficients for x/l of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0	P.L.	0.491	0.402	0.374	0.339	0.296	0.227	0.049		-0.049		-0.223			-0.230	-0.428	-0.017	-0.022	0.036
	57.5						.227								-.230				
	51.0						.268	.080											
	48.0							.092											
	45.0				.339				0.023			-.433				-.428			
	41.0									.034									
	34.0											-.718							
	30.0			.374				.224				-.357	-0.870		-.623	-.497	-.017		
	15.0		.402		.389		.343			.225		.026		-0.831	-.957	-.501	.000	-.022	
	03.0	.491	.460	.441	.432		.398			.244	-0.106	-.215			-.514	-.579	.001	-.009	.036
	01.0							.375									.004	.002	
	00.0																		
-4.4	P.L.	0.627	0.497	0.478	0.445	0.407	0.330	0.149		0.028		-0.118			-0.127	-0.345	-0.118	-0.072	0.018
	57.5						.330								-.127				
	51.0						.376	.195											
	48.0							.209											
	45.0				.445				0.129			-.273				-.345			
	41.0									.133									
	34.0											-.545							
	30.0			.478				.309				-.285	-0.681		-.444	-.449	-.118		
	15.0		.497		.458		.427			.290		.081		-0.801	-.960	-.398	-.103	-.072	
	03.0	.627	.521	.518	.512		.471			.277	-0.226	-.325			-.540	-.510	-.073	-.036	.018
	01.0							.422									-.057	-.026	
	00.0																		
4.4	00.0																-0.045	-0.019	
	01.0							0.180											
	03.0	0.288	0.329	0.336	0.316		0.282			0.140	-0.093	-0.221			-0.538	-0.610	-.037	-.024	0.015
	15.0		.275		.287		.251			.151		-.026		-0.853	-.962	-.715	-.010	-.006	
	30.0			.254				.135				-.408	-0.928		-.785	-.563	-.006		
	34.0											-.803							
	41.0									.046									
	45.0				.229				-0.077			-.527				-.499			
	48.0							-.010											
	51.0						.175	-.013											
	57.5						.127								-.305				
	P.L.	.288	.275	.254	.229	0.197	.127	-.038		-.104		-.291			-.305	-.499	-.006	-.006	.015
-8.8	P.L.	0.652	0.595	0.571	0.526	0.486	0.426	0.246		0.116		-0.028			-0.044	-0.272	-0.123	-0.135	-0.006
	57.5						.426								-.044				
	51.0						.460	.293											
	48.0							.307											
	45.0				.526				0.228			-.124				-.272			
	41.0									.224									
	34.0											-.350							
	30.0			.571				.388				-.177	-0.484		-.315	-.386	-.123		
	15.0		.595		.541		.494			.350		.132		-0.784	-.948	-.335	-.240	-.135	
	03.0	.652	.529	.526	.518		.480			.234	-0.429	-.477			-.595	-.467	-.309	-.077	-.006
	01.0							.386									-.216	-.062	
	00.0																		
8.8	00.0																-0.181	-0.061	
	01.0							-0.214											
	03.0	-0.037	-0.147	-0.301	-0.106		-0.128			-0.141	-0.226	-0.305			-0.596	-0.627	-.168	-.064	-0.009
	15.0		.107		.158		.149			.055		-.074		-0.884	-.959	-.847	-.059	-.076	
	30.0			.104				.036				-.470	-0.999		-.926	-.619	.007		
	34.0											-.915							
	41.0									-.151									
	45.0				.084				-0.221			-.639				-.579			
	48.0							-.134											
	51.0						.055	-.132											
	57.5						.000								-.389				
	P.L.	-.037	.107	.104	.084	0.058	.000	-.149		-.182		-.368			-.389	-.579	.007	-.076	-.009

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(h) $M = 0.95$; $\alpha = 5.1^\circ$

β, deg	ø, deg	Pressure coefficients for x/l of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0.5	P.L.	0.393	0.410	0.332	0.319	0.290	0.236	0.079		-0.032		-0.193			-0.197	-0.428	-0.116	-0.031	0.043
	57.5						.236								-.197				
	51.0						.276	.112											
	48.0							.121											
	45.0				.319				0.047	-.002		-.369				-.428			
	41.0									.039									
	34.0											-.611							
	30.0			.332				.184				-.371	-0.766		-.518	-.568	-.116		
	15.0		.410		.328		.283			.165		-.024		-0.856	-.995	-.531	-.072	-.031	
	03.0	.393	.411	.371	.342		.309			.168	-0.218	-.317			-.592	-.646	-.050	-.013	.043
	01.0							.284											
	00.0																-.047	-.002	
-3.8	P.L.	0.510	0.501	0.426	0.401	0.372	0.322	0.165		0.043		-0.106			-0.115	-0.363	-0.244	-0.084	0.021
	57.5						.322								-.115				
	51.0						.352	.199											
	48.0							.209											
	45.0				.401				0.137	.081		-.213				-.363			
	41.0									.121									
	34.0											-.439							
	30.0			.426				.264				-.292	-0.556		-.409	-.490	-.244		
	15.0		.501		.412		.359			.228		.027		-0.823	-.975	-.462	-.210	-.084	
	03.0	.510	.477	.438	.422		.378			.181	-0.355	-.426			-.616	-.538	-.109	-.036	.021
	01.0							.319											
	00.0																-.107	-.032	
4.9	00.0																-0.106	-0.033	
	01.0							0.018											
	03.0	0.199	0.299	0.231	0.175		0.186			-0.004	-0.222	-0.323			-0.609	-0.661	-.101	-.061	-0.001
	15.0		.298		230		.197			.088		-.074		-0.875	-.992	-.604	-.053	-.018	
	30.0			.213				.10_				-.429	-0.869		-.653	-.607	-.069		
	34.0											-.731							
	41.0									-.042									
	45.0				.215				-0.047	-.075		-.471				-.494			
	48.0							.014											
	51.0						.182	.010											
	57.5						.147								-.280				
	P.L.	.199	.298	.213	.215	0.190	.147	-.008		-.096		-.269			-.280	-.494	-.069	-.018	-.001
-8.3	P.L.	0.563	0.558	0.491	0.457	0.428	0.388	0.229		0.104		-0.051			-0.077	-0.328	-0.199	-0.117	0.006
	57.5						.388								-.077				
	51.0						.412	.260											
	48.0							.271											
	45.0				.457				0.193	.128		-.165				-.328			
	41.0									.176									
	34.0											-.326							
	30.0			.491				.315				-.187	-0.502		-.339	-.466	-.199		
	15.0		.558		.451		.404			.265		.059		-0.825	-.980	-.480	-.291	-.117	
	03.0	.563	.476	.433	.413		.373			.147	-0.439	-.485			-.633	-.570	-.185	-.051	.006
	01.0							.288											
	00.0																-.182	-.046	
9.3	00.0																-0.231	-0.063	
	01.0							-0.241											
	03.0	-0.150	-0.257	-0.418	-0.213		-0.262			-0.199	-0.323	-0.393			-0.654	-0.639	-.251	-.073	-0.007
	15.0		.120		.125		.090			.042		-.090		-0.879	-.995	-.801	-.082	-.079	
	30.0			.067				.003				-.485	-0.984		-.846	-.658	-.063		
	34.0											-.859							
	41.0									-.134									
	45.0				.080				-0.150	-.139		-.570				-.554			
	48.0							-.096											
	51.0						.065	-.097											
	57.5						.040								-.360				
	P.L.	-.150	.120	.067	.080	0.067	.040	-.105		-.162		-.345			-.360	-.554	-.063	-.079	-.007

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(1) $M = 0.95$; $\alpha = 10.3^\circ$

β, deg	∅, deg	Pressure coefficients for x/l of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0.4	P.L.	0.350	0.302	0.311	0.307		0.261	0.109		0.014		-0.174			-0.192	-0.431	-0.283	-0.037	0.091
	57.5						.261								-.192				
	51.0						.283	.131											
	48.0							.131											
	45.0				.307				0.077			-.275				-.431			
	41.0									.049									
	34.0											-.493							
	30.0			.311				.162				-.373	-0.627		-.475	-.570	-.283		
	15.0		.302		.297		.237			.116		-.079		-0.865	-1.037	-.551	-.169	-.037	
	03.0	.350	.310	.298	.283		.236			.090	-0.333	-.399			-.660	-.624	-.128	-.010	.091
	01.0							.114											
	00.0																-.115	.012	
-3.9	P.L.	0.442	0.395	0.391	0.371		0.328	0.189		0.084		-0.101			-0.116	-0.372	-0.370	-0.055	0.033
	57.5						.328								-.116				
	51.0						.340	.201											
	48.0							.205											
	45.0				.371				0.150			-.169				-.372			
	41.0									.115									
	34.0											-.316							
	30.0			.391				.229				-.238	-0.437		-.351	-.492	-.370		
	15.0		.395		.369		.306			.174		-.020		-0.831	-1.006	-.577	-.343	-.055	
	03.0	.442	.372	.365	.353		.293			.089	-0.481	-.540			-.690	-.594	-.202	-.038	.033
	01.0							.129											
	00.0																-.197	-.060	
4.8	00.0																-0.186	-0.064	
	01.0							0.121											
	03.0	0.143	0.180	0.175	0.142		0.105			-0.029	-0.330	-0.410			-0.675	-0.685	-.163	-.081	0.006
	15.0		.191		.223		.166			.069		-.123		-0.877	-1.041	-.597	-.138	-.038	
	30.0			.199				.088				-.441	-0.746		-.555	-.610	-.184		
	34.0											-.609							
	41.0									-.023									
	45.0				.224				0.006			-.372				-.476			
	48.0							.049											
	51.0						.198	.042											
	57.5						.173								-.256				
	P.L.	.143	.191	.199	.224		.173	.030		-.040		-.241			-.256	-.476	-.184	-.038	.006
-7.2	P.L.	0.516	0.451	0.444	0.419		0.379	0.240		0.135		-0.053			-0.084	-0.340	-0.354	-0.070	0.025
	57.5						.379								-.084				
	51.0						.389	.247											
	48.0							.251											
	45.0				.419				0.198			-.119				-.340			
	41.0									.155									
	34.0											-.245							
	30.0			.444				.263				-.171	-0.383		-.301	-.469	-.354		
	15.0		.451		.398		.336			.201		.003		-0.825	-1.000	-.605	-.435	-.070	
	03.0	.516	.372	.360	.344		.288			.062	-0.538	-.579			-.701	-.604	-.246	-.042	.025
	01.0							.119											
	00.0																-.256	-.043	
8.0	00.0																-0.254	-0.059	
	01.0							0.102											
	03.0	-0.081	-0.154	-0.269	-0.140		-0.160			-0.182	-0.373	-0.433			-0.695	-0.671	-.223	-.095	0.013
	15.0		.073		.149		.089			.038		-.138		-0.886	-1.045	-.629	-.130	-.064	
	30.0			.095				.023				-.491	-0.861		-.629	-.653	-.151		
	34.0											-.707							
	41.0									-.078									
	45.0				.140				-0.061			-.441				-.525			
	48.0							-.026											
	51.0						.129	-.024											
	57.5						.099								-.315				
	P.L.	-.081	.073	.095	.140		.099	-.038		-.098		-.294			-.315	-.525	-.151	-.064	.013

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(j) M = 0.99; $\alpha = 0^\circ$

β, deg	ø, deg	Pressure coefficients for x/l of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0	P.L.	0.524	0.436	0.410	0.376	0.336	0.269	0.097		0.007		-0.174			-0.186	-0.376	-0.131	-0.095	-0.017
	57.5						.269								-.186				
	51.0						.311	.129											
	48.0							.138											
	45.0				.376				0.072			-.384				-.376			
	41.0									.086									
	34.0											-.644							
	30.0			.410				.268				-.286	-0.788		-.566	-.474	-.131		
	15.0		.436		.426		.379			.271		.087		-0.739	-.875	-.477	-.117	-.095	
	03.0	.524	.494	.474	.468		.434			.290	-0.050	-.155			-.441	-.523	-.119	-.078	-.017
	01.0							.415									-.123	-.067	
	00.0																		
-4.4	P.L.	0.657	0.527	0.509	0.478	0.442	0.369	0.191		0.079		-0.075			-0.083	-0.294	-0.142	-0.151	-0.040
	57.5						.369								-.083				
	51.0						.414	.239											
	48.0							.251											
	45.0				.478				0.174			-.245				-.294			
	41.0									.179									
	34.0											-.483							
	30.0			.509				.349				-.220	-0.615		-.385	-.403	-.142		
	15.0		.527		.490		.462			.334		.136		-0.712	-.879	-.355	-.217	-.151	
	03.0	.657	.554	.552	.544		.505			.321	-0.169	-.262			-.467	-.465	-.248	-.110	-.040
	01.0							.458									-.212	-.101	
	00.0																		
4.4	00.0																-0.200	-0.094	
	01.0							0.227											
	03.0	0.316	0.361	0.366	0.347		0.318			0.184	-0.039	-0.160			-0.464	-0.548	-.168	-.099	-0.049
	15.0		.306		.321		.288			.193		.029		-0.765	-.882	-.678	-.099	-.080	
	30.0			.286				.175				-.341	-0.851		-.730	-.523	-.088		
	34.0											-.733							
	41.0									.001									
	45.0				.264				-0.032			-.483				-.448			
	48.0							.031											
	51.0						.213	.028							-.260				
	57.5						.168								-.260	-.448	-.088	-.080	-.049
	P.L.	.316	.306	.286	.264	0.230	.168	.004		-.052		-.241							
-8.9	P.L.	0.682	0.626	0.603	0.559	0.524	0.465	0.291		0.165		0.022			0.006	-0.217	-0.106	-0.232	-0.072
	57.5						.465								.006				
	51.0						.498	.336											
	48.0							.350											
	45.0				.559				0.275			-.080				-.217			
	41.0									.268									
	34.0											-.299							
	30.0			.603				.426				-.130	-0.402		-.264	-.334	-.106		
	15.0		.626		.577		.528			.391		.185		-0.691	-.865	-.290	-.215	-.232	
	03.0	.682	.562	.558	.551		.514			.277	-0.387	-.431			-.532	-.409	-.602	-.166	-.072
	01.0							.423									-.563	-.157	
	00.0																		
8.9	00.0																-0.502	-0.148	
	01.0							-0.164											
	03.0	0.007	-0.111	-0.254	-0.062		-0.085			-0.090	-0.172	-0.243			-0.519	-0.570	-.327	-.146	-0.072
	15.0		.145		.197		.191			.101		-.013		-0.787	-.869	-.769	-.147	-.131	
	30.0			.141				.084				-.392	-0.905		-.843	-.566	-.083		
	34.0											-.827							
	41.0									-.124									
	45.0				.125				-0.182			-.581				-.519			
	48.0							-.091											
	51.0						.101	-.085							-.330				
	57.5						.048								-.330				
	P.L.	.007	.145	.141	.125	0.099	.048	-.103		-.136		-.310				-.519	-.083	-.131	-.072

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(k) $M = 0.99$; $\alpha = 5.2^{\circ}$

β, deg	ø, deg	Pressure coefficients for x/l of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0.5	P.L.	0.426	0.441	0.365	0.356	0.326	0.275	0.121		0.015		-0.145			-0.153	-0.367	-0.197	-0.118	-0.025
	57.5						.275								-.153				
	51.0						.314	.155											
	48.0							.162											
	45.0				.356				0.096	.045		-.326				-.367			
	41.0									.088									
	34.0											-.544							
	30.0			.365				.225				-.303	-0.688		-.459	-.504	-.197		
	15.0		.441		.366		.322			.210		.032		-0.760	-.901	-.478	-.170	-.118	
	03.0	.426	.446	.405	.379		.346			.214	-0.162	-.249			-.517	-.580	-.161	-.097	-.025
	01.0							.323											
	00.0																-.170	-.085	
-3.9	P.L.	0.539	0.529	0.460	0.434	0.406	0.358	0.207		0.087		-0.060			-0.070	-0.302	-0.221	-0.184	-0.048
	57.5						.358								-.070				
	51.0						.390	.241											
	48.0							.251											
	45.0				.434				0.182	.125		-.173				-.302			
	41.0									.167									
	34.0											-.383							
	30.0			.460				.303				-.230	-0.498		-.349	-.429	-.221		
	15.0		.529		.446		.395			.269		.080		-0.730	-.881	-.415	-.288	-.184	
	03.0	.539	.508	.469	.454		.413			.227	-0.298	-.363			-.544	-.484	-.236	-.126	-.048
	01.0							.357											
	00.0																-.213	-.125	
4.9	00.0																-0.218	-0.122	
	01.0							0.067											
	03.0	0.245	0.342	0.265	0.218		0.226			0.052	-0.170	-0.264			-0.533	-0.587	-0.205	-0.148	-0.072
	15.0		.336		.275		.239			.138		-.012		-0.775	-.898	-.551	-.140	-.112	
	30.0			.254				.148				-.354	-0.765		-.577	-.537	-.143		
	34.0											-.641							
	41.0									.014									
	45.0				.255				0.009	-.018		-.406				-.424			
	48.0							.063											
	51.0						.227	.062											
	57.5						.194								-.224				
	P.L.	.245	.336	.254	.255	0.236	.194	.043		-.039		-.211			-.224	-.424	-.143	-.112	-.072
-8.4	P.L.	0.613	0.617	0.548	0.512	0.487	0.449	0.298		0.171		0.025			0.003	-0.241	-0.192	-0.230	-0.070
	57.5						.449								.003				
	51.0						.470	.328											
	48.0							.337											
	45.0				.512				0.267	.203		-.069				-.241			
	41.0									.244									
	34.0											-.197							
	30.0			.548				.374				-.088	-0.351		-.228	-.365	-.192		
	15.0		.617		.510		.459			.325		.133		-0.712	-.868	-.421	-.307	-.230	
	03.0	.613	.517	.477	.460		.420			.190	-0.448	-.485			-.573	-.486	-.390	-.154	-.070
	01.0							.327											
	00.0																-.318	-.157	
9.4	00.0																-0.352	-0.175	
	01.0							-0.201											
	03.0	-0.119	-0.254	-0.376	-0.182		-0.224			-0.159	-0.273	-0.339			-0.580	-0.580	-.345	-.191	-0.083
	15.0		.151		.161		.129			.086		-.029		-0.781	-.901	-.751	-.159	-.184	
	30.0			.099				.045				-.412	-0.899		-.783	-.600	-.125		
	34.0											-.779							
	41.0									-.091									
	45.0				.115				-0.114	-.095		-.510				-.491			
	48.0							-.057											
	51.0						.104	-.057											
	57.5						.082								-.306				
	P.L.	-.119	.151	.099	.115	0.101	.082	-.061		-.112		-.288			-.306	-.491	-.125	-.184	-.083

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(l) M = 0.99; α = 10.3°

β, deg	∅, deg	Pressure coefficients for x/l of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0.4	P.L.	0.384	0.337	0.345	0.342		0.300	0.151		0.061		-0.123			-0.141	-0.366	-0.298	-0.145	0.014
	57.5						.300								-.141				
	51.0						.321	.171											
	48.0							.175											
	45.0				.342				0.124			-.226				-.366			
	41.0									.097									
	34.0											-.433							
	30.0			.345				.205				-.308	-0.562		-.414	-.498	-.298		
	15.0		.337		.335		.277			.164		-.021		-0.769	-.943	-.495	-.217	-.145	
	03.0	.384	.345	.333	.313		.276			.140	-0.275	-.334			-.583	-.574	-.187	-.112	.014
	01.0							.160									-.180	-.088	
	00.0																		
-3.9	P.L.	0.476	0.430	0.426	0.407		0.366	0.233		0.130		-0.048			-0.063	-0.307	-0.333	-0.178	-0.050
	57.5						.366								-.063				
	51.0						.380	.246											
	48.0							.250											
	45.0				.407				0.199			-.114				-.307			
	41.0									.163									
	34.0											-.255							
	30.0			.426				.270				-.181	-0.370		-.288	-.421	-.333		
	15.0		.430		.407		.343			.218		.035		-0.737	-.914	-.523	-.368	-.178	
	03.0	.476	.405	.396	.380		.330			.135	-0.421	-.479			-.613	-.530	-.250	-.148	-.050
	01.0							.173									-.246	-.163	
	00.0																		
4.8	00.0																-0.240	-0.164	
	01.0							0.162											
	03.0	0.172	0.214	0.204	0.170		0.151			0.016	-0.265	-0.345			-0.599	-0.632	-.216	-.187	-0.077
	15.0		.222		.257		.202			.115		-.068		-0.786	-.950	-.543	-.179	-.155	
	30.0			.231				.127				-.372	-0.682		-.500	-.548	-.209		
	34.0											-.546							
	41.0									.025									
	45.0				.256				0.052			-.325				-.420			
	48.0							.089											
	51.0						.234	.083							-.208				
	57.5						.210												
	P.L.	.172	.222	.231	.256		.210	.070		.006		-.189			-.208	-.420	-.209	-.155	-.077
-7.2	P.L.	0.555	0.494	0.483	0.459		0.423	0.291		0.187		0.005			-0.023	-0.267	-0.327	-0.193	-0.056
	57.5						.423								-.023				
	51.0						.434	.299											
	48.0							.300											
	45.0				.459				0.249			-.054				-.267			
	41.0									.209									
	34.0											-.166							
	30.0			.483				.308				-.103	-0.299		-.228	-.390	-.327		
	15.0		.494		.441		.378			.250		.066		-0.727	-.901	-.563	-.421	-.193	
	03.0	.555	.409	.397	.375		.329			.110	-0.495	-.536			-.629	-.538	-.294	-.157	-.056
	01.0							.166									-.300	-.164	
	00.0																		
8.1	00.0																-0.300	-0.174	
	01.0							0.145											
	03.0	-0.038	-0.120	-0.219	-0.094		-0.127			-0.129	-0.310	-0.367			-0.617	-0.610	-.263	-.210	-0.079
	15.0		.110		.188		.127			.086		-.080		-0.789	-.948	-.572	-.167	-.188	
	30.0			.132				.067				-.418	-0.777		-.565	-.582	-.179		
	34.0											-.631							
	41.0									-.026									
	45.0				.179				-0.010			-.382				-.458			
	48.0							.018											
	51.0						.172	.022							-.259				
	57.5						.141												
	P.L.	-.038	.110	.132	.179		.141	.005		-.049		-.237			-.259	-.458	-.179	-.188	-.079

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(m) M = 1.02; $\alpha = 0^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0	P.L.	0.556	0.466	0.441	0.407	0.370	0.310	0.137		0.051		-0.128			-0.145	-0.331	-0.110	-0.082	-0.005
	57.5						.310								-.145				
	51.0						.347	.170											
	48.0							.181											
	45.0				.407				0.114			-.350				-.331			
	41.0									.129									
	34.0											-.587							
	30.0			.441				.300				-.232	-0.728		-.518	-.435	-.110		
	15.0		.466		.457		.413			.307		.131		-0.675	-.825	-.438	-.100	-.082	
	03.0	.556	.523	.504	.497		.467			.325	-0.006	-.107			-.386	-.473	-.105	-.066	-.005
	01.0							.450											
	00.0																-.112	-.056	
-4.4	P.L.	0.686	0.558	0.540	0.509	0.474	0.403	0.230		0.118		-0.035			-0.040	-0.245	-0.105	-0.137	-0.029
	57.5						.403								-.040				
	51.0						.448	.278											
	48.0							.289											
	45.0				.509				0.216			-.215				-.245			
	41.0									.217									
	34.0											-.425							
	30.0			.540				.383				-.164	-0.550		-.341	-.357	-.105		
	15.0		.558		.522		.496			.371		.180		-0.645	-.818	-.308	-.184	-.137	
	03.0	.686	.583	.582	.576		.537			.356	-0.124	-.217			-.412	-.420	-.241	-.098	-.029
	01.0							.492											
	00.0																-.207	-.087	
4.4	00.0																-0.187	-0.079	
	01.0							0.276											
	03.0	0.355	0.396	0.402	0.382		0.354			0.223	0.004	-0.114			-0.407	-0.491	-.150	-.083	-0.031
	15.0		.340		.360		.325			.234		.081		-0.692	-.820	-.618	-.077	-.064	
	30.0			.323				.216				-.276	-0.771		-.661	-.473	-.064		
	34.0											-.659							
	41.0									.046									
	45.0				.300				0.015			-.442				-.393			
	48.0							.075											
	51.0						.253	.075											
	57.5						.210								-.212				
	P.L.	.355	.340	.323	.300	0.269	.210	.050		-.007		-.195			-.212	-.393	-.064	-.064	-.031
-8.9	P.L.	0.706	0.654	0.632	0.588	0.555	0.498	0.328		0.201		0.064			0.049	-0.172	-0.069	-0.219	-0.060
	57.5						.498								.049				
	51.0						.531	.374											
	48.0							.385											
	45.0				.588				0.312			-.052				-.172			
	41.0									.305									
	34.0											-.256							
	30.0			.632				.459				-.085	-0.350		-.220	-.290	-.069		
	15.0		.654		.607		.559			.425		.230		-0.624	-.805	-.243	-.176	-.219	
	03.0	.706	.594	.589	.582		.548			.314	-0.335	-.378			-.475	-.355	-.555	-.156	-.060
	01.0							.457											
	00.0																-.574	-.147	
8.9	00.0																-0.529	-0.137	
	01.0							-0.114											
	03.0	0.051	-0.077	-0.203	-0.016		-0.043			-0.045	-0.128	-0.197			-0.461	-0.521	-.317	-.135	-0.059
	15.0		.183		.232		.230			.139		.035		-0.718	-.812	-.711	-.123	-.115	
	30.0			.177				.124				-.330	-0.834		-.786	-.525	-.059		
	34.0											-.758							
	41.0									-.087									
	45.0				.162				-0.140			-.544				-.466			
	48.0							-.046											
	51.0						.142	-.041											
	57.5						.092								-.287				
	P.L.	.051	.183	.177	.162	0.139	.092	-.058		-.097		-.261			-.287	-.466	-.059	-.115	-.059

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(n) M = 1.02; α = 5.2°

β, deg	∅, deg	Pressure coefficients for x/ℓ of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0.5	P.L.	0.447	0.463	0.393	0.384	0.353	0.306	0.154		0.053		-0.107			-0.119	-0.324	-0.165	-0.105	-0.012
	57.5						.306								-.119				
	51.0						.344	.188											
	48.0							.193											
	45.0				.384				0.132	.077		-.308				-.324			
	41.0									.123									
	34.0											-.509							
	30.0			.393				.260				-.255	-0.654		-.438	-.461	-.165		
	15.0		.463		.389		.354			.248		.077		-0.694	-.838	-.450	-.143	-.105	
	05.0	.447	.470	.425	.398		.368			.249	-0.118	-.204			-.465	-.534	-.145	-.087	-.012
	01.0							.348									-.155	-.075	
	00.0																		
-3.9	P.L.	0.572	0.561	0.493	0.467	0.442	0.397	0.247		0.130		-0.015			-0.027	-0.251	-0.181	-0.172	-0.034
	57.5						.397								-.027				
	51.0						.427	.281											
	48.0							.288											
	45.0				.467				0.225	.164		-.162				-.251			
	41.0									.209									
	34.0											-.328							
	30.0			.493				.338				-.178	-0.443		-.296	-.374	-.181		
	15.0		.561		.478		.430			.308		.127		-0.663	-.825	-.367	-.258	-.172	
	05.0	.572	.543	.501	.488		.446			.266	-0.252	-.320			-.489	-.444	-.218	-.112	-.034
	01.0							.394									-.192	-.111	
	00.0																		
4.9	00.0																-0.197	-0.108	
	01.0							0.113											
	03.0	0.285	0.379	0.300	0.259		0.268			0.095	-0.123	-0.217			-0.475	-0.536	-.183	-.134	-0.058
	15.0		.368		.310		.277			.181		.036		-0.705	-.839	-.508	-.115	-.097	
	30.0			.291				.187				-.295	-0.694		-.521	-.482	-.115		
	34.0											-.577							
	41.0									.059									
	45.0				.292				0.056	.023		-.387				-.369			
	48.0							.106											
	51.0						.267	.105							-.179				
	57.5						.234												
	P.L.	.285	.368	.291	.292	0.273	.234	.085		.005		-.165			-.179	-.369	-.115	-.097	-.058
-8.3	P.L.	0.638	0.640	0.579	0.542	0.516	0.481	0.332		0.207		0.064			0.040	-0.195	-0.154	-0.213	-0.054
	57.5						.481								.040				
	51.0						.502	.362											
	48.0							.371											
	45.0				.542				0.305	.236		-.057				-.195			
	41.0									.281									
	34.0											-.157							
	30.0			.579				.407				-.048	-0.315		-.189	-.319	-.154		
	15.0		.640		.535		.489			.360		.177		-0.648	-.813	-.378	-.261	-.213	
	05.0	.638	.550	.507	.490		.452			.229	-0.384	-.421			-.513	-.440	-.373	-.137	-.054
	01.0							.362									-.293	-.141	
	00.0																		
9.4	00.0																-0.326	-0.162	
	01.0							-0.142											
	03.0	-0.053	-0.162	-0.309	-0.119		-0.162			-0.102	-0.216	-0.280			-0.518	-0.534	-.311	-.177	-0.070
	15.0		.195		.201		.171			.122		.015		-0.713	-.839	-.685	-.132	-.161	
	30.0			.143				.088				-.351	-0.822		-.708	-.542	-.097		
	34.0											-.708							
	41.0									-.051									
	45.0				.157				-0.069	-.062		-.471				-.431			
	48.0							-.009											
	51.0						.151	-.007											
	57.5						.127								-.259				
	P.L.	-.053	.195	.143	.157	0.145	.127	-.015		-.071		-.238			-.259	-.431	-.097	-.161	-.070

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(o) M = 1.02; α = 10.3°

β, deg	∅, deg	Pressure coefficients for x/l of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0.4	P.L.	0.416	0.369	0.379	0.376		0.332	0.185		0.096		-0.085			-0.101	-0.321	-0.264	-0.129	0.028
	51.0						0.355	0.210											
	48.0							.211											
	45.0				.376				0.163			-.186				-.321			
	41.0									.138									
	34.0											-0.382							
	30.0			.379				.241				-.257	-0.510		-0.364	-0.443	-.264		
	15.0		.369		.365		.312			.201		.022		-0.703	-.887	-.445	-.187	-.129	
	03.0	.416	.379	.365	.346		.311			.180	-0.230	-.285			-.525	-.537	-.157	-.096	.028
	01.0							.181									-.152	-.074	
	00.0																		
-3.9	P.L.	0.497	0.455	0.453	0.433		0.396	0.263		0.162		-0.011			-0.026	-0.265	-0.295	-0.164	-0.035
	57.5						.396								-.026				
	51.0						.409	.277											
	48.0							.279											
	45.0				.433				0.232			-.078				-.265			
	41.0									.195									
	34.0											-.224							
	30.0			.453				.303				-.145	-0.331		-.247	-.381	-.295		
	15.0		.455		.434		.374			.252		.075		-0.677	-.860	-.472	-.335	-.164	
	03.0	.497	.435	.428	.409		.362			.174	-0.362	-.419			-.557	-.485	-.219	-.135	-.035
	01.0							.195									-.215	-.149	
	00.0																		
4.8	00.0																-0.213	-0.147	
	01.0							0.190											
	03.0	0.221	0.253	0.246	0.205		0.195			0.067	-0.220	-0.298			-0.539	-0.580	-.187	-.168	-0.061
	15.0		.261		.295		.242			.157		-.017		-0.714	-.886	-.493	-.154	-.140	
	30.0			.271				.168				-.314	-0.604		-.443	-.488	-.185		
	34.0											-.480							
	41.0									.071									
	45.0				.296				0.097			-.270				-.363			
	48.0							.132											
	51.0						.273	.129							-.158				
	57.5						.249								-.158	-.363	-.185	-.140	-.061
	P.L.	.221	.261	.271	.296		.249	.112		.049		-.140							
-7.2	P.L.	0.574	0.515	0.507	0.483		0.450	0.318		0.217		0.039			0.011	-0.226	-0.287	-0.178	-0.040
	57.5						.450								.011				
	51.0						.460	.326											
	48.0							.328								-.226			
	45.0				.483				0.278			-.023							
	41.0									.240									
	34.0											-.144							
	30.0			.507				.337				-.072	-0.272		-.196	-.350	-.287		
	15.0		.515		.463		.405			.280		.104		-0.670	-.850	-.508	-.367	-.178	
	03.0	.574	.438	.424	.400		.358			.150	-0.421	-.462			-.568	-.494	-.257	-.142	-.040
	01.0							.186									-.263	-.148	
	00.0																		
8.1	00.0																-0.281	-0.161	
	01.0							0.171											
	03.0	-0.006	-0.091	-0.193	-0.071		-0.097			-0.093	-0.264	-0.323			-0.563	-0.565	-.240	-.200	-0.067
	15.0		.140		.220		.162			.122		-.036		-0.725	-.889	-.531	-.141	-.176	
	30.0			.163				.101				-.366	-0.724		-.521	-.533	-.151		
	34.0											-.585							
	41.0									.008									
	45.0				.209				0.026			-.349				-.418			
	48.0							.054											
	51.0						.206	.058											
	P.L.	-.006	.140	.163	.209		.171	.031		-.019		-.196			-.226	-.418	-.151	-.176	-.067

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(p) M = 1.08; $\alpha = 0°$

β, deg	ø, deg	Pressure coefficients for x/l of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0	P.L.	0.587	0.497	0.475	0.448	0.417	0.361	0.197		0.121		-0.056			-0.077	-0.258	-0.074	-0.038	0.043
	57.5						.361								-.077				
	51.0						.400	.230											
	48.0							.234											
	45.0				.448				0.177			-.305				-.258			
	41.0									.195									
	34.0											-.489							
	30.0			.475				.352				-.143	-0.621		-.443	-.371	-.074		
	15.0		.497		.500		.462			.364		.206		-0.560	-.723	-.379	-.080	-.038	
	03.0	.587	.554	.539	.539		.511			.381	0.061	-.040			-.295	-.383	-.086	-.021	.043
	01.0							.500											
	00.0																-.095	-.015	
-4.4	P.L.	0.717	0.586	0.572	0.550	0.516	0.453	0.284		0.182		0.024			0.013	-0.180	-0.053	-0.096	0.020
	57.5						.453								.013				
	51.0						.491	.330											
	48.0							.343											
	45.0				.550				0.276			-.188				-.180			
	41.0									.278									
	34.0											-.346							
	30.0			.572				.431				-.080	-0.468		-.281	-.299	-.053		
	15.0		.586		.563		.540			.426		.253		-0.532	-.711	-.254	-.127	-.096	
	03.0	.717	.615	.616	.615		.580			.412	-0.058	-.141			-.321	-.352	-.231	-.054	.020
	01.0							.540											
	00.0																-.193	-.045	
4.4	00.0																-0.173	-0.036	
	01.0							0.336											
	03.0	0.383	0.427	0.436	0.425		0.398			0.278	0.068	-0.047			-0.320	-0.403	-.128	-.040	0.014
	15.0		.370		.399		.370			.287		.148		-0.583	-.715	-.547	-.049	-.018	
	30.0			.356				.266				-.194	-0.669		-.586	-.413	-.039		
	34.0											-.570							
	41.0									.098									
	45.0				.340				0.080			-.387				-.323			
	48.0							.130											
	51.0						.304	.132											
	57.5						.260								-.147				
	P.L.	.383	.370	.356	.340	0.312	.260	.106		.055		-.126			-.147	-.323	-.039	-.018	.014
-8.8	P.L.	0.722	0.683	0.662	0.624	0.593	0.536	0.376		0.259		0.123			0.103	-0.103	-0.012	-0.176	0.013
	57.5						.536								.103				
	51.0						.573	.423											
	48.0							.436											
	45.0				.624				0.368			-.022				-.103			
	41.0									.359									
	34.0											-.199							
	30.0			.662				.505				-.017	-0.295		-.162	-.227	-.012		
	15.0		.683		.646		.603			.479		.296		-0.514	-.697	-.185	-.112	-.176	
	03.0	.722	.630	.626	.623		.590			.373	-0.252	-.292			-.381	-.282	-.460	-.102	.013
	01.0							.509											
	00.0																-.532	-.097	
8.8	00.0																-0.455	-0.085	
	01.0							-0.006											
	03.0	0.133	0.030	-0.070	0.082		0.067			0.050	-0.040	-0.109			-0.358	-0.427	-.273	-.082	0.011
	15.0		.237		.295		.290			.207		.110		-0.594	-.706	-.597	-.082	-.052	
	30.0			.232				.191				-.232	-0.703		-.666	-.444	-.027		
	34.0											-.633							
	41.0									-.018									
	45.0				.220				-0.059			-.450				-.374			
	48.0							.025											
	51.0						.209	.036											
	57.5						.162								-.205				
	P.L.	.133	.237	.232	.220	0.202	.162	.017		-.026		-.180			-.205	-.374	-.027	-.052	.011

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(q) M = 1.08; $\alpha = 5.2^{\circ}$

β, deg	ø, deg	Pressure coefficients for x/l of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0.3	P.L.	0.486	0.489	0.431	0.428	0.403	0.359	0.212		0.118		-0.038			-0.054	-0.243	-0.130	-0.067	0.038
	57.5						.359								-.054				
	51.0						.398	.248											
	48.0							.254											
	45.0				.428				0.199	.143		-.192				-.243			
	41.0									.191									
	34.0											-.401							
	30.0			.431				.312				-.168	-0.532		-.347	-.376	-.130		
	15.0		.489		.437		.402			.306		.151		-0.578	-.739	-.366	-.114	-.067	
	03.0	.486	.509	.472	.452		.426			.314	-0.048	-.126			-.368	-.458	-.104	-.046	.038
	01.0							.409											
	00.0																-.114	-.035	
-4.1	P.L.	0.593	0.579	0.523	0.503	0.481	0.438	0.295		0.183		0.036			0.032	-0.175	-0.125	-0.136	0.013
	57.5						.438								.032				
	51.0						.468	.330											
	48.0							.338											
	45.0				.503				0.279	.217		-.079				-.175			
	41.0									.266									
	34.0											-.259							
	30.0			.523				.385				-.102	-0.366		-.227	-.298	-.125		
	15.0		.579		.514		.469			.358		.196		-0.551	-.719	-.302	-.205	-.136	
	03.0	.593	.573	.532	.525		.490			.321	-0.182	-.247			-.399	-.381	-.203	-.076	.013
	01.0							.442											
	00.0																-.167	-.076	
4.7	00.0																-0.172	-0.070	
	01.0							0.162											
	03.0	0.312	0.414	0.332	0.301		0.310			0.156	-0.056	-0.145			-0.385	-0.458	-.153	-.094	-0.010
	15.0		.388		.349		.321			.236		.105		-0.591	-.735	-.454	-.084	-.054	
	30.0			.322				.235				-.212	-0.599		-.446	-.411	-.085		
	34.0											-.488							
	41.0									.117									
	45.0				.330				0.107	.078		-.277				-.296			
	48.0							.157											
	51.0						.314	.157											
	57.5						.280								-.121				
	P.L.	.312	.388	.322	.330	0.314	.280	.136		.061		-.100			-.121	-.296	-.085	-.054	-.010
-8.5	P.L.	0.658	0.663	0.609	0.576	0.557	0.522	0.380		0.258		0.121			0.099	-0.120	-0.104	-0.180	0.018
	57.5						.522								.099				
	51.0						.544	.410											
	48.0							.418											
	45.0				.576				0.355	.289		.052				-.120			
	41.0									.337									
	34.0											-.103							
	30.0			.609				.451				.000	-0.206		-.116	-.237	-.104		
	15.0		.663		.575		.531			.408		.244		-0.533	-.707	-.316	-.204	-.180	
	03.0	.658	.579	.541	.529		.498			.284	-0.327	-.360			-.431	-.367	-.428	-.098	.018
	01.0							.412											
	00.0																-.286	-.109	
9.2	00.0																-0.303	-0.109	
	01.0							-0.084											
	03.0	-0.005	-0.082	-0.272	-0.068		-0.106			-0.041	-0.145	-0.206			-0.427	-0.468	-.272	-.129	0.003
	15.0		.231		.241		.220			.171		.082		-0.597	-.734	-.602	-.092	-.086	
	30.0			.178				.143				-.263	-0.717		-.621	-.471	-.056		
	34.0											-.611							
	41.0									.002									
	45.0				.197				-0.019	-.017		-.370				-.354			
	48.0							.046											
	51.0						.204	.051											
	57.5						.178								-.194				
	P.L.	-.005	.231	.178	.197	0.189	.178	.042		-.015		-.171			-.194	-.354	-.056	-.086	.003

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(r) $M = 1.08$; $\alpha = 10.3^\circ$

β, deg	ø, deg	Pressure coefficients for x/l of –																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0.4	P.L.	0.434	0.393	0.405	0.412		0.372	0.237		0.155		-0.013			-0.033	-0.237	-0.221	-0.092	0.082
	57.5						.372								-.033				
	51.0						.395	.256											
	48.0							.259											
	45.0				.412				0.219			-.116				-.237			
	41.0									.202									
	34.0											-.303							
	30.0			.405				.289				-.178	-0.426		-.289	-.362	-.221		
	15.0		.393		.404		.357			.262		.091		-0.589	-.773	-.377	-.153	-.092	
	03.0	.434	.409	.395	.384		.356			.243	-0.164	-.213			-.433	-.479	-.121	-.058	.081
	01.0							.211									-.118	-.039	
	00.0																		
-3.9	P.L.	0.519	0.485	0.484	0.468		0.433	0.309		0.214		0.048			0.031	-0.186	-0.239	-0.118	0.031
	57.5						.433								.031				
	51.0						.449	.326											
	48.0							.328											
	45.0				.468				0.287			-.016				-.186			
	41.0									.255									
	34.0											-.168							
	30.0			.484				.350				-.085	-0.258		-.178	-.294	-.239		
	15.0		.485		.472		.416			.308		.141		-0.564	-.746	-.400	-.293	-.118	
	03.0	.519	.465	.459	.446		.405			.233	-0.290	-.340			-.466	-.407	-.183	-.091	.031
	01.0							.226									-.180	-.109	
	00.0																		
4.8	00.0																-0.177	-0.110	
	01.0							0.220											
	03.0	0.248	0.286	0.279	0.245		0.242			0.127	-0.149	-0.225			-0.446	-0.506	-.149	-.125	0.003
	15.0		.288		.332		.286			.215		.050		-0.604	-.775	-.423	-.116	-.095	
	30.0			.300				.215				-.233	-0.515		-.371	-.404	-.151		
	34.0											-.400							
	41.0									.128									
	45.0				.332				0.153			-.204				-.286			
	48.0							.179											
	51.0						.319	.175							-.095				
	57.5						.290								-.095	-.286	-.151	-.095	.003
	P.L.	.248	.288	.300	.332		.290	.156		.096		-.078							
-7.2	P.L.	0.596	0.546	0.540	0.518		0.488	0.363		0.263		0.096			0.078	-0.150	-0.239	-0.107	0.024
	57.5						.488								.078				
	51.0						.498	.374											
	48.0							.376											
	45.0				.518				0.330			.041				-.150			
	41.0									.296									
	34.0											-.079							
	30.0			.540				.383				-.007	-0.187		-.121	-.267	-.239		
	15.0		.546		.503		.450			.336		.173		-0.558	-.739	-.441	-.305	-.107	
	03.0	.596	.472	.460	.442		.404			.209	-0.350	-.386			-.482	-.410	-.222	-.086	.024
	01.0							.218									-.227	-.095	
	00.0																		
8.0	00.0																-0.236	-0.104	
	01.0							0.207											
	03.0	0.034	-0.059	-0.151	-0.028		-0.049			-0.035	-0.189	-0.244			-0.467	-0.492	-.192	-.148	0.012
	15.0		.173		.264		.217			.175		.035		-0.611	-.779	-.470	-.090	-.105	
	30.0			.197				.154				-.278	-0.633		-.452	-.448	-.102		
	34.0											-.497							
	41.0									.065									
	45.0				.248				0.065			-.268				-.327			
	48.0							.106											
	51.0						.257	.111							-.154				
	57.5						.226								-.154	-.327	-.102	-.105	.012
	P.L.	.034	.173	.197	.248		.226	.092		.037		-.130							

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(s) M = 1.13; $\alpha = 0^{\circ}$

β, deg	∅, deg	Pressure coefficients for x/l of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0	P.L.	0.573	0.486	0.473	0.458	0.427	0.379	0.218		0.162		-0.018			-0.043	-0.216	-0.055	-0.040	0.052
	57.5						.379								-.043				
	51.0						.416	.251											
	48.0							.255											
	45.0				.458				0.206			-.240				-.216			
	41.0									.228									
	34.0											-.426							
	30.0			.473				.375				-.086	-0.551		-.408	-.333	-.055		
	15.0		.486		.511		.478			.394		.253		-0.482	-.640	-.360	-.084	-.040	
	03.0	.573	.546	.542	.547		.527			.413	0.098	.003			-.237	-.320	-.095	-.023	.052
	01.0							.521									-.107	-.017	
	00.0																		
-4.4	P.L.	0.702	0.575	0.574	0.558	0.529	0.472	0.310		0.223		0.065			0.049	-0.136	-0.033	-0.132	0.016
	57.5						.472								.049				
	51.0						.516	.360											
	48.0							.367											
	45.0				.558				0.310			-.109				-.136			
	41.0									.315									
	34.0											-.273							
	30.0			.574				.453				-.024	-0.388		-.233	-.255	-.033		
	15.0		.575		.572		.556			.455		.298		-0.450	-.627	-.227	-.109	-.132	
	03.0	.702	.603	.612	.621		.594			.438	-0.051	-.118			-.278	-.299	-.305	-.073	.016
	01.0							.559									-.272	-.065	
	00.0																		
4.4	00.0																-0.202	-0.055	
	01.0							0.362											
	03.0	0.371	0.415	0.433	0.436		0.415			0.305	0.096	-0.005			-0.262	-0.343	-.157	-.059	0.010
	15.0		.347		.409		.385			.316		.200		-0.495	-.636	-.471	-.057	-.035	
	30.0			.347				.291				-.134	-0.573		-.510	-.366	-.048		
	34.0											-.487							
	41.0									.135						-.269			
	45.0				.347				0.085			-.304							
	48.0							.153											
	51.0						.326	.160							-.100				
	57.5						.284												
	P.L.	.371	.347	.347	.347	0.324	.284	.133		.093		-.076			-.100	-.269	-.048	-.035	.010
-8.9	P.L.	0.712	0.677	0.661	0.631	0.602	0.550	0.394		0.287		0.144			0.132	-0.068	-0.003	-0.226	-0.016
	57.5						.550								.132				
	51.0						.588	.444											
	48.0							.455											
	45.0				.631				0.394			.007				-.068			
	41.0									.387									
	34.0											-.159							
	30.0			.661				.525				.029	-0.268		-.117	-.194	-.003		
	15.0		.677		.655		.616			.506		.339		-0.438	-.618	-.177	-.095	-.226	
	03.0	.712	.626	.626	.630		.601			.395	-0.221	-.257			-.331	-.259	-.420	-.123	-.016
	01.0							.525									-.494	-.121	
	00.0																		
8.9	00.0																-0.480	-0.122	
	01.0							-0.005											
	03.0	0.114	-0.003	-0.135	0.041		0.034			0.060	-0.022	-0.075			-0.308	-0.376	-.378	-.117	-0.019
	15.0		.216		.284		.305			.231		.145		-0.511	-.634	-.542	-.100	-.068	
	30.0			.204				.212				-.176	-0.627		-.613	-.412	-.046		
	34.0											-.570							
	41.0									-.002						-.332			
	45.0				.212				-0.048			-.396							
	48.0							.041											
	51.0						.231	.053							-.170				
	57.5						.187												
	P.L.	.114	.216	.204	.212	0.200	.187	.039		.002		-.140			-.170	-.332	-.046	-.068	-.019

TABLE III.- Continued

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(t) M = 1.13; $\alpha = 5.2^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0	P.L.	0.469	0.458	0.433	0.440	0.411	0.369	0.223		0.147		-0.013			-0.034	-0.202	-0.109	-0.067	0.037
	57.5						.369								-.034				
	51.0						.404	.252											
	48.0							.263											
	45.0				.440				0.222	.172		-.151				-.202			
	41.0									.219									
	34.0											-.345							
	30.0			.433				.334				-.126	-0.461		-.300	-.331	-.109		
	15.0		.458		.445		.418			.344		.183		-0.499	-.614	-.319	-.133	-.067	
	03.0	.469	.504	.466	.463		.445			.334	-0.019	-.087			-.310	-.392	-.124	-.047	.037
	01.0							.411											
	00.0																-.127	-.035	
-4.4	P.L.	0.627	0.569	0.533	0.521	0.504	0.467	0.323		0.226		0.067			0.057	-0.130	-0.100	-0.152	0.011
	57.5						.467								.057				
	51.0						.496	.357											
	48.0							.365											
	45.0				.521				0.311	.249		-.039				-.130			
	41.0									.303									
	34.0											-.199							
	30.0			.533				.409				-.057	-0.305		-.183	-.251	-.100		
	15.0		.569		.530		.491			.394		.241		-0.470	-.635	-.281	-.185	-.152	
	03.0	.627	.567	.528	.533		.507			.347	-0.168	-.228			-.351	-.360	-.273	-.086	.011
	01.0							.463											
	00.0																-.210	-.088	
4.4	00.0																-0.183	-0.084	
	01.0							0.196											
	03.0	0.306	0.426	0.353	0.350		0.327			0.198	-0.018	-0.102			-0.328	-0.423	-.160	-.101	-0.014
	15.0		.347		.359		.340			.273		.144		-0.514	-.660	-.424	-.091	-.064	
	30.0			.316				.257				-.168	-0.536		-.406	-.372	-.090		
	34.0											-.423							
	41.0									.143									
	45.0				.338				0.123	.098		-.220				-.250			
	48.0							.178											
	51.0						.337	.179											
	57.5						.305								-.086				
	P.L.	.306	.347	.316	.338	0.327	.305	.160		.102		-.058			-.086	-.250	-.090	-.064	-.014
-8.9	P.L.	0.641	0.650	0.613	0.587	0.568	0.538	0.400		0.294		0.144			0.133	-0.076	-0.089	-0.205	-0.011
	57.5						.538								.133				
	51.0						.559	.428											
	48.0							.439											
	45.0				.587				0.381	.313		.084				-.076			
	41.0									.365									
	34.0											-.090							
	30.0			.613				.472				.018	-0.169		-.090	-.199	-.089		
	15.0		.650		.585		.546			.441		.276		-0.458	-.619	-.295	-.181	-.205	
	03.0	.641	.574	.537	.534		.509			.303	-0.301	-.332			-.389	-.348	-.463	-.118	-.011
	01.0							.424											
	00.0																-.340	-.133	
8.9	00.0																-0.335	-0.149	
	01.0							-0.043											
	03.0	0.020	-0.031	-0.283	-0.109		-0.071			-0.007	-0.103	-0.161			-0.370	-0.441	-.273	-.177	-0.032
	15.0		.229		.244		.242			.198		.118		-0.517	-.658	-.553	-.098	-.114	
	30.0			.168				.168				-.216	-0.643		-.566	-.428	-.066		
	34.0											-.549							
	41.0									.025									
	45.0				.210				-0.002	-.004		-.303				-.309			
	48.0							.073											
	51.0						.234	.079											
	57.5						.205								-.159				
	P.L.	.020	.229	.168	.210	0.200	.205	.071		.015		-.133			-.159	-.309	-.066	-.114	-.032

TABLE III.- Concluded

PRESSURE COEFFICIENTS FOR LARGE VEE-WINDSHIELD CANOPY 2

(u) $M = 1.13$; $\alpha = 10.3^{\circ}$

β, deg	ϕ, deg	Pressure coefficients for x/l of —																	
		0.008	0.044	0.076	0.124	0.140	0.164	0.212	0.244	0.260	0.295	0.311	0.324	0.345	0.356	0.440	0.600	0.828	0.988
0.4	P.L.	0.369	0.372	0.393	0.415		0.365	0.225		0.156		-0.009			-0.031	-0.212	-0.195	-0.094	0.065
	57.5						.365								-.031				
	51.0						.391	.246											
	48.0							.251											
	45.0				.415				0.228			-.107				-.212			
	41.0									.214									
	34.0											-.280							
	30.0			.393				.291				-.146	-0.390		-.272	-.326	-.195		
	15.0		.372		.398		.358			.280		.122		-0.526	-.662	-.348	-.162	-.094	
	03.0	.369	.386	.384	.383		.363			.262	-0.104	-.168			-.379	-.406	-.123	-.059	.065
	01.0							.323									-.118	-.038	
	00.0																		
-3.9	P.L.	0.500	0.471	0.481	0.473		0.295	0.163		0.102		-0.059			-0.085	-0.249	-0.223	-0.125	0.009
	57.5						.295								-.085				
	51.0						.456	.334											
	48.0							.336											
	45.0				.473				0.302			-.180				-.249			
	41.0									.279									
	34.0											-.151							
	30.0			.481				.358				-.059	-0.243		-.157	-.255	-.223		
	15.0		.471		.473		.425			.328		.175		-0.495	-.665	-.386	-.269	-.125	
	03.0	.500	.447	.453	.449		.416			.256	-0.254	-.303			-.406	-.364	-.185	-.098	.009
	01.0							.365									-.178	-.118	
	00.0																		
4.8	00.0																-0.174	-0.117	
	01.0							0.132											
	03.0	0.217	0.256	0.259	0.231		0.248			0.131	-0.103	-0.182			-0.389	-0.458	-0.150	-0.129	-0.019
	15.0		.251		.329		.293			.235		.090		-0.530	-.694	-.396	-.115	-.097	
	30.0			.281				.224				-.188	-0.481		-.346	-.366	-.152		
	34.0											-.364							
	41.0									.149									
	45.0				.331				0.148			-.178				-.244			
	48.0							.189											
	51.0						.328	.186											
	57.5						.297								-.080				
	P.L.	.217	.251	.281	.331		.297	.167		.106		-.055			-.080	-.244	-.152	-.097	-.019
-7.2	P.L.	0.561	0.528	0.531	0.515		0.488	0.368		0.276		0.110			0.087	-0.117	-0.238	-0.134	-0.004
	57.5						.488								.087				
	51.0						.502	.379											
	48.0							.384											
	45.0				.515				0.347			.054				-.117			
	41.0									.313									
	34.0											-.071							
	30.0			.531				.393				.006	-0.163		-.101	-.230	-.238		
	15.0		.528		.506		.455			.356		.205		-0.487	-.663	-.411	-.277	-.134	
	03.0	.561	.461	.451	.442		.411			.232	-0.301	-.339			-.424	-.377	-.229	-.115	-.004
	01.0							.239									-.226	-.127	
	00.0																		
8.1	00.0																-0.239	-0.140	
	01.0							-0.014											
	03.0	0.044	-0.093	-0.138	-0.009		-0.016			-0.004	-0.143	-0.196			-0.411	-0.452	-.190	-.182	-0.022
	15.0		.156		.266		.237			.186		.081		-0.535	-.696	-.447	-.102	-.131	
	30.0			.182				.179				-.222	-0.561		-.418	-.403	-.116		
	34.0											-.439							
	41.0									.085									
	45.0				.251				0.077			-.230				-.284			
	48.0							.127											
	51.0						.275	.132											
	57.5						.241								-.127				
	P.L.	.044	.156	.182	.251		.241	.115		.053		-.100			-.127	-.284	-.116	-.131	-.022

TABLE IV

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(a) $M = 0.80$; $\alpha = 0^\circ$

β, deg	ø, deg	Pressure coefficients for x/l of —														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0	P.L.	0.150			0.106	0.045		-0.066	-0.135	-0.092	-0.106	-0.045	-0.012	-0.023	-0.057	-0.029
	80.0	.150			.111	.062		-.066	-.214	-.103		-.045				
	60.0	-.233			.178	.118		-.012	-.245	-.128	-.092		-.012			
	40.0	.327			.143	.116		.042	-.213	-.155		-.021		-.023		
	32.0				.212											
	23.0					.255										
	20.0		0.431		.267		0.100	.016	-.225	-.193	-.112		-.001		-.057	
	11.0							.042								
	00.0			0.460		.240		.065	-.208	-.204	-.089	-.019		-.029		-.029
-4.2	P.L.	0.243			0.187	0.125		0.008	-0.077	-0.079	-0.111	-0.074	-0.032	-0.027	-0.071	-0.044
	80.0	.243			.204	.158		.037	-.140	-.090		-.074				
	60.0	-.089			.272	.209		.081	-.156	-.120	-.124		-.032			
	40.0	.262			.258	.197		.115	-.149	-.158		-.057		-.027		
	32.0				.268											
	23.0					.290										
	20.0		0.409		.277		0.125	.078	-.206	-.212	-.147		-.036		-.071	
	11.0							.069								
	00.0			0.407		.220		.048	-.239	-.236	-.122	-.048		-.055		-.044
4.2	00.0			0.448		0.232		0.045	-0.225	-0.227	-0.113	-0.044		-0.049		-0.040
	11.0							-.027								
	20.0		0.432		0.223		0.034	-.107	-.287	-.223	-.131		-0.015		-0.072	
	23.0					.170										
	32.0				.105											
	40.0	0.339			-.075	.000		-.067	-.314	-.191		-.024		-.033		
	60.0	-.428			.053	-.010		-.133	-.356	-.156	-.084		-.012			
	80.0	.014			.012	-.046		-.178	-.284	-.121		-.037				
	P.L.	.014			.014	-.040		-.148	-.196	-.120	-.131	-.037	-.012	-.033	-.072	-.040
-8.5	P.L.	0.348			0.267	0.207		0.088	-0.015	-0.061	-0.127	-0.115	-0.091	-0.096	-0.138	-0.085
	80.0	.348			.286	.247		.131	-.064	-.078		-.115				
	60.0	.027			.343	.280		.161	-.086	-.131	-.183		-.091			
	40.0	.126			.302	.247		.151	-.120	-.204		-.139		-.096		
	32.0				.265											
	23.0					.277										
	20.0		0.358		.251		0.104	.074	-.226	-.282	-.237		-.116		-.138	
	11.0							.046								
	00.0			0.354		.170		-.004	-.314	-.324	-.208	-.131		-.110		-.085
8.5	00.0			0.405		0.199		-0.002	-0.275	-0.302	-0.186	-0.121		-0.102		-0.078
	11.0							-.143								
	20.0		0.403		0.155		-0.073	-.303	-.386	-.297	-.194		-0.057		-0.110	
	23.0					.047										
	32.0				-.046											
	40.0	0.324			-.382	-.151		-.211	-.458	-.255		-.048		-.063		
	60.0	-.660			-.094	-.145		-.270	-.486	-.188	-.094		-.045			
	80.0	-.239			-.102	-.160		-.299	-.338	-.151		-.092				
	P.L.	-.239			-.087	-.135		-.239	-.274	-.156	-.197	-.092	-.045	-.063	-.110	-.078

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(b) M = 0.80; $\alpha = 5.1^\circ$

β, deg	∅, deg	Pressure coefficients for x/l of −														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0	P.L.	0.128				0.036		-0.079	-0.160	-0.139	-0.147	-0.084	-0.041	-0.040	-0.064	-0.031
	80.0	.128			0.106	.066		-.056	-.219	-.146		-.084				
	60.0	-.255			.153	.098		-.019	-.253	-.166	-.138		-.041			
	40.0	.230			.116	.076		.001	-.251	-.191		-.047		-.040		
	32.0				.147											
	23.0					.179										
	20.0		0.343		.188		0.021	-.051	-.294	-.226	-.126		-.025		-.064	
	11.0							-.037								
	00.0			0.371		.157		-.008	-.285	-.236	-.106	-.035		-.048		-.031
-4.2	P.L.	0.221				0.105		-0.013	-0.113	-0.138	-0.173	-0.131	-0.080	-0.060	-0.083	-0.055
	80.0	.221			0.178	.140		.023	-.163	-.146		-.131				
	60.0	-.141			.226	.169		.054	-.195	-.180	-.187		-.080			
	40.0	.119			.197	.139		.053	-.213	-.217		-.096		-.060		
	32.0				.188											
	23.0					.208										
	20.0		0.339		.194		0.043	-.002	-.283	-.254	-.169		-.056		-.083	
	11.0							-.016								
	00.0			0.341		.142		-.021	-.310	-.263	-.131	-.057		-.069		-.055
4.2	00.0			0.361		0.153		-0.016	-0.295	-0.255	-0.126	-0.055		-0.064		-0.048
	11.0							-.102								
	20.0		0.360		0.154		-0.040	-.158	-.339	-.237	-.126		-0.029		-0.079	
	23.0					.111										
	32.0				.058											
	40.0	0.275			-.065	-.024		-.088	-.328	-.196		-.032		-.042		
	60.0	-.419			.053	.000		-.115	-.340	-.167	-.102		-.021			
	80.0	.020			.019	-.029		-.150	-.275	-.145		-.057				
	P.L.	.020				-.040		-.147	-.210	-.137	-.124	-.057	-.021	-.042	-.079	-.048
-8.5	P.L.	0.302				0.183		0.063	-0.051	-0.118	-0.198	-0.191	-0.138	-0.116	-0.114	-0.077
	80.0	.302			0.245	.217		.104	-.102	-.149		-.191				
	60.0	-.031			.279	.225		.114	-.152	-.226	-.280		-.138			
	40.0	-.042			.210	.165		.067	-.209	-.296		-.199		-.116		
	32.0				.170											
	23.0					.179										
	20.0		0.280		.165		0.014	-.023	-.320	-.344	-.274		-.120		-.114	
	11.0							-.039								
	00.0			0.285		.090		-.079	-.389	-.352	-.210	-.126		-.110		-.077
8.5	00.0			0.316		0.108		-0.075	-0.360	-0.345	-0.211	-0.136		-0.102		-0.070
	11.0							-.232								
	20.0		0.323		0.077		-0.158	-.382	-.445	-.307	-.177		-0.085		-0.106	
	23.0					-.019										
	32.0				-.100											
	40.0	0.252			-.367	-.176		-.234	-.460	-.243		-.064		-.093		
	60.0	-.635			-.091	-.133		-.250	-.450	-.188	-.111		-.075			
	80.0	-.203			-.093	-.138		-.260	-.330	-.167		-.132				
	P.L.	-.203				-.132		-.234	-.270	-.152	-.153	-.132	-.075	-.093	-.106	-.070

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(c) M = 0.80; α = 10.2°

β, deg	ϕ, deg	Pressure coefficients for x/l of −														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0.4	P.L.	0.121			0.070	0.025		-0.089	-0.181	-0.189	-0.199	-0.131	-0.067	-0.055	-0.063	-0.007
	80.0	.121			.088	.071		-.054	-.235	-.193		-.131				
	60.0	-.189			.121	.097		-.045	-.266	-.216	-.186		-.067			
	40.0	.105			.101	.069		-.044	-.292	-.229		-.068		-.055		
	32.0				.097											
	23.0					.114										
	20.0		0.264		.118		-0.048	-.106	-.344	-.246	-.132		-.039		-.063	
	11.0							-.104								
	00.0			0.267		.080		-.081	-.347	-.246	-.110	-.034		-.056		-.007
-3.8	P.L.	0.198			0.124	0.082		-0.036	-0.139	-0.185	-0.233	-0.188	-0.099	-0.065	-0.083	-0.032
	80.0	.198			.139	.127		.005	-.196	-.209		-.188				
	60.0	-.155			.174	.146		.002	-.234	-.252	-.254		-.099			
	40.0	-.035			.144	.104		-.011	-.279	-.276		-.120		-.065		
	32.0				.119											
	23.0					.128										
	20.0		0.253		.119		-0.036	-.078	-.346	-.286	-.175		-.079		-.083	
	11.0							-.088								
	00.0			0.251		.068		-.093	-.370	-.271	-.126	-.050		-.099		-.032
4.7	00.0			0.272		0.071		-0.095	-0.361	-0.270	-0.127	-0.056		-0.098		-0.034
	11.0							-.166								
	20.0		0.283		.088		-0.106	-.196	-.376	-.240	-.118		-0.050		-0.093	
	23.0					.052										
	32.0				.023											
	40.0	0.204			-.029	-.006		-.109	-.341	-.206		-.045		-.044		
	60.0	-.373			.045	.018		-.123	-.321	-.188	-.129		-.043			
	80.0	.036			.021	-.006		-.130	-.276	-.179		-.078				
	P.L.	.036			.008	-.040		-.150	-.223	-.175	-.154	-.078	-.043	-.044	-.093	-.034
-8.1	P.L.	0.244			0.189	0.150		0.039	-0.078	-0.169	-0.263	-0.249	-0.151	-0.101	-0.098	-0.039
	80.0	.244			.194	.191		.072	-.151	-.223		-.249				
	60.0	-.065			.206	.187		.044	-.216	-.317	-.368		-.151			
	40.0	-.190			.131	.099		-.015	-.294	-.375		-.231		-.101		
	32.0				.087											
	23.0					.089										
	20.0		0.199		.088		-0.066	-.107	-.391	-.383	-.276		-.108		-.098	
	11.0							-.114								
	00.0			0.227		.024		-.143	-.443	-.346	-.186	-.105		-.111		-.039
8.9	00.0			0.225		0.028		-0.149	-0.426	-0.351	-0.195	-0.113		-0.096		-0.041
	11.0							-.285								
	20.0		0.250		0.022		-0.215	-.385	-.457	-.285	-.146		-0.123		-0.080	
	23.0					-.062										
	32.0				-.110											
	40.0	0.184			-.280	-.130		-.225	-.431	-.219		-.080		-.147		
	60.0	-.552			-.068	-.091		-.230	-.395	-.191	-.124		-.072			
	80.0	-.118			-.064	-.088		-.220	-.317	-.184		-.085				
	P.L.	-.118			-.069	-.120		-.221	-.261	-.161	-.135	-.085	-.072	-.147	-.080	-.041

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(d) $M = 0.90$; $\alpha = 0^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of –														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0	P.L.	0.163			0.126	0.066		-0.065	-0.179	-0.118	-0.115	-0.049	-0.012	-0.032	-0.073	-0.039
	80.0	.163			.133	.077		-.069	-.288	-.119		-.049				
	60.0	-.227			.203	.140		.001	-.321	-.131	-.095		-.012			
	40.0	.356			.162	.137		.058	-.252	-.141		-.018		-.032		
	32.0				.232											
	23.0					.278										
	20.0		0.467		.290		0.118	.029	-.237	-.162	-.113		-.004		-.073	
	11.0							.063								
	00.0			0.497		.265		.086	-.216	-.171	-.092	-.017		-.041		-.039
-4.3	P.L.	0.260			0.205	0.142		0.012	-0.105	-0.119	-0.129	-0.072	-0.032	-0.033	-0.087	-0.053
	80.0	.260			.219	.171		.039	-.179	-.127		-.072				
	60.0	-.092			.293	.229		.090	-.185	-.157	-.131		-.032			
	40.0	.276			.277	.215		.130	-.154	-.196		-.054		-.033		
	32.0				.287											
	23.0					.311										
	20.0		0.445		.300		0.141	.092	-.200	-.256	-.146		-.036		-.087	
	11.0							.087								
	00.0			0.442		.246		.073	-.226	-.261	-.118	-.043		-.065		-.053
4.3	00.0			0.477		0.257		0.066	-0.243	-0.332	-0.120	-0.045		-0.064		-0.049
	11.0							-.014								
	20.0		0.464		0.246		0.048	-.120	-.312	-.227	-.132		-0.021		-0.092	
	23.0					.194										
	32.0				.125											
	40.0	0.378			-.075	.012		-.064	-.397	-.164		-.020		-.046		
	60.0	-.442			.073	.005		-.131	-.489	-.147	-.085		-.015			
	80.0	-.021			.021	-.042		-.191	-.411	-.131		-.056				
	P.L.	-.021			.032	-.026		-.156	-.271	-.133	-.135	-.056	-.015	-.046	-.092	-.049
-8.6	P.L.	0.367			0.285	0.225		0.096	-0.026	-0.098	-0.160	-0.115	-0.089	-0.096	-0.143	-0.087
	80.0	.367			.307	.263		.139	-.082	-.117		-.115				
	60.0	.028			.366	.303		.177	-.094	-.175	-.188		-.089			
	40.0	.138			.325	.268		.173	-.109	-.258		-.132		-.096		
	32.0				.289											
	23.0					.302										
	20.0		0.399		.282		0.125	.097	-.202	-.380	-.219		-.107		-.143	
	11.0							.074								
	00.0			0.392		.202		.030	-.283	-.494	-.182	-.112		-.112		-.087
8.6	00.0			0.438		0.222		0.018	-0.300	-0.566	-0.196	-0.124		-0.116		-0.088
	11.0							-.126								
	20.0		0.436		0.177		-0.053	-.345	-.405	-.572	-.178		-0.068		-0.133	
	23.0					.082										
	32.0				-.021											
	40.0	0.376			-.394	-.143		-.259	-.567	-.297		-.051		-.070		
	60.0	-.680			-.077	-.131		-.297	-.648	-.238	-.133		-.044			
	80.0	-.363			-.099	-.154		-.356	-.500	-.186		-.213				
	P.L.	-.363			-.074	-.127		-.261	-.379	-.169	-.181	-.213	-.044	-.070	-.133	-.088

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(e) $M = 0.90$; $\alpha = 5.1^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of −														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0	P.L.	0.134				0.051		-0.076	-0.196	-0.188	-0.150	-0.075	-0.041	-0.050	-0.078	-0.035
	80.0	.134			0.118	.075		-.056	-.278	-.183		-.075				
	60.0	-.260			.174	.112		-.008	-.317	-.192	-.131		-.041			
	40.0	.243			.129	.092		.016	-.298	-.204		-.043		-.050		
	32.0				.167											
	23.0					.204										
	20.0		0.378		.209		0.036	-.041	-.317	-.227	-.120		-.027		-.078	
	11.0							-.018								
	00.0			0.405		.181		.019	-.307	-.250	-.104	-.034		-.060		-.035
-4.3	P.L.	0.242				0.125		-0.004	-0.127	-0.195	-0.189	-0.129	-0.083	-0.068	-0.098	-0.061
	80.0	.242			0.199	.160		.034	-.187	-.210		-.129				
	60.0	-.140			.249	.191		.075	-.213	-.259	-.191		-.083			
	40.0	.121			.217	.161		.075	-.222	-.311		-.092		-.068		
	32.0				.208											
	23.0					.232										
	20.0		0.372		.219		0.059	.017	-.279	-.359	-.162		-.057		-.098	
	11.0							.011								
	00.0			0.374		.167		.006	-.313	-.339	-.123	-.052		-.081		-.061
4.3	00.0			0.387		0.176		0.005	-0.327	-0.407	-0.132	-0.061		-0.083		-0.060
	11.0							-.090								
	20.0		0.388		0.174		-0.030	-.174	-.378	-.269	-.123		-0.041		-0.099	
	23.0					.131										
	32.0				.075							-.037		-.058		
	40.0	0.309			-.065	-.016		-.082	-.407	-.202			-.030			
	60.0	-.425			.068	.015		-.111	-.444	-.178	-.102					
	80.0	.004			.028	-.021		-.159	-.371	-.168		-.061				
	P.L.	.004				-.027		-.154	-.267	-.169	-.122	-.061	-.030	-.058	-.099	-.060
-8.6	P.L.	0.325				0.203		0.078	-0.053	-0.158	-0.271	-0.191	-0.136	-0.120	-0.127	-0.080
	80.0	.325			0.272	.238		.117	-.108	-.191		-.191				
	60.0	-.026			.305	.250		.137	-.144	-.281	-.294		-.136			
	40.0	-.044			.235	.189		.095	-.193	-.385		-.192		-.120		
	32.0				.192											
	23.0					.201										
	20.0		0.314		.191		0.031	.004	-.283	-.501	-.238		-.109		-.127	
	11.0							-.011								
	00.0			0.321		.120		-.041	-.362	-.588	-.179	-.106		-.119		-.080
8.6	00.0			0.349		0.137		-0.046	-0.396	-0.637	-0.193	-0.122		-0.116		-0.077
	11.0							-.202								
	20.0		0.356		0.106		-0.128	-.392	-.470	-.489	-.150		-0.091		-0.121	
	23.0					.023										
	32.0				-.062							-.076		-.097		
	40.0	0.299			-.345	-.151		-.249	-.537	-.289			-.131			
	60.0	-.600			-.064	-.109		-.248	-.567	-.235	-.127					
	80.0	-.281			-.072	-.112		-.275	-.450	-.200		-.118				
	P.L.	-.281				-.110		-.239	-.341	-.178	-.129	-.118	-.131	-.097	-.121	-.077

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(f) $M = 0.90$; $\alpha = 10.2^\circ$

β, deg	∅, deg	Pressure coefficients for x/l of −														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0.4	P.L.	0.127			0.084	0.038		-0.088	-0.205	-0.281	-0.201	-0.121	-0.068	-0.065	-0.069	-0.004
	80.0	.127			.099	.081		-.052	-.276	-.286		-.121				
	60.0	-.187			.136	.114		-.038	-.305	-.299	-.172		-.068			
	40.0	.135			.118	.083		-.029	-.326	-.285		-.062		-.065		
	32.0				.116											
	23.0					.134							-.041		-.069	
	20.0		0.295		.139		-0.035	-.091	-.365	-.282	-.117					
	11.0							-.084								
	00.0			0.298		.104		-.052	-.373	-.286	-.103	-.035		-.063		-.004
-3.8	P.L.	0.217			0.148	0.105		-0.017	-0.141	-0.258	-0.261	-0.189	-0.103	-0.081	-0.098	-0.034
	80.0	.217			.165	.154		.025	-.207	-.296		-.189				
	60.0	-.150			.200	.170		.026	-.236	-.374	-.263		-.103			
	40.0	-.045			.169	.128		.012	-.287	-.431		-.118		-.081		
	32.0				.140											
	23.0					.150							-.088		-.098	
	20.0		0.283		.141		-0.018	-.055	-.344	-.438	-.167					
	11.0							-.059								
	00.0			0.281		.091		-.067	-.383	-.362	-.121	-.056		-.118		-.034
4.7	00.0			0.301		0.095		-0.068	-0.398	-0.380	-0.123	-0.061		-0.116		-0.038
	11.0							-.140								
	20.0		0.312		0.110		-0.090	-.182	-.406	-.280	-.113		-.060		-.110	
	23.0					.078										
	32.0				.044							-.044		-.052		
	40.0	0.232			-.009	.014		-.091	-.394	-.239			-.048			
	60.0	-.360			.066	.037		-.112	-.381	-.231	-.125					
	80.0	.052			.042	.011		-.126	-.337	-.236		-.078				
	P.L.	.052			.026	-.021		-.149	-.258	-.247	-.155	-.078	-.048	-.052	-.110	-.038
-8.1	P.L.	0.268			0.208	0.166		0.055	-0.075	-0.211	-0.377	-0.240	-0.152	-0.117	-0.106	-0.048
	80.0	.268			.218	.211		.088	-.152	-.270		-.240				
	60.0	-.057			.231	.210		.069	-.201	-.393	-.471		-.152			
	40.0	-.190			.154	.126		.015	-.280	-.512		-.206		-.117		
	32.0				.106											
	23.0					.110							-.116		-.106	
	20.0		0.230		.110		-0.049	-.081	-.358	-.596	-.226					
	11.0							-.083								
	00.0			0.257		.049		-.106	-.432	-.586	-.164	-.118		-.115		-.048
9.0	00.0			0.255		0.050		-0.127	-0.469	-0.642	-0.178	-0.130		-0.120		-0.054
	11.0							-.273								
	20.0		0.281		0.043		-0.200	-.402	-.484	-.374	-.154		-.161		-.101	
	23.0					-.034										
	32.0				-.090							-.120		-.139		
	40.0	0.225			-.273	-.117		-.214	-.498	-.280			-.053			
	60.0	-.527			-.053	-.076		-.223	-.487	-.240	-.131					
	80.0	-.146			-.049	-.074		-.225	-.405	-.236		-.078				
	P.L.	-.146			-.050	-.106		-.229	-.316	-.216	-.130	-.078	-.053	-.139	-.101	-.054

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(g) M = 0.95; $\alpha = 0^\circ$

β, deg	∅, deg	Pressure coefficients for x/l of −														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0	P.L.	0.193			0.159	0.099		-0.037	-0.162	-0.219	-0.203	-0.031	-0.010	-0.040	-0.112	-0.048
	80.0	.193			.170	.117		-.033	-.271	-.233		-.031				
	60.0	-.177			.234	.173		.041	-.286	-.278	-.162		-.010			
	40.0	.365			.198	.170		.093	-.219	-.331		.002		-.040		
	32.0				.261											
	23.0					.304										
	20.0		0.494		.312		0.144	.067	-.205	-.436	-.114		-.007		-.112	
	11.0							.095								
	00.0			0.490		.284		.110	-.199	-.509	-.091	.007		-.054		-.048
-4.3	P.L.	0.286			0.235	0.173		0.038	-0.088	-0.160	-0.272	-0.043	-0.026	-0.037	-0.116	-0.059
	80.0	.286			.250	.204		.068	-.174	-.177		-.043				
	60.0	-.059			.321	.257		.123	-.176	-.229	-.317		-.026			
	40.0	.284			.304	.244		.163	-.145	-.286		-.021		-.037		
	32.0				.314											
	23.0					.340										
	20.0		0.467		.324		0.170	.124	-.174	-.400	-.251		-.030		-.116	
	11.0							.121								
	00.0			0.463		.271		.102	-.204	-.506	-.156	-.012		-.071		-.059
4.3	00.0			0.491		0.281		0.097	-0.213	-0.513	-0.129	-0.007		-0.071		-0.054
	11.0							.026								
	20.0		0.474		0.273		0.082	-.067	-.266	-.543	-.103		-0.013		-0.123	
	23.0					.227										
	32.0				.161											
	40.0	0.405			-.021	.057		-.014	-.340	-.418		.005		-.053		
	60.0	-.364			.107	.045		-.083	-.427	-.346	-.090		-.010			
	80.0	.003			.065	.004		-.162	-.388	-.291		-.029				
	P.L.	.003			.067	.011		-.124	-.248	-.294	-.156	-.029	-.010	-.053	-.123	-.054
-8.7	P.L.	0.397			0.320	0.260		0.127	-0.000	-0.095	-0.251	-0.154	-0.080	-0.100	-0.173	-0.097
	80.0	.397			.337	.301		.172	-.055	-.108		-.154				
	60.0	.054			.392	.331		.208	-.064	-.179	-.365		-.080			
	40.0	.143			.351	.297		.202	-.075	-.268		-.091		-.100		
	32.0				.319											
	23.0					.335										
	20.0		0.421		.304		0.156	.126	-.156	-.402	-.562		-.092		-.173	
	11.0							.111								
	00.0			0.417		.230		.061	-.244	-.525	-.469	-.064		-.117		-.097
8.7	00.0			0.464		0.251		0.055	-0.270	-0.553	-0.380	-0.061		-0.122		-0.091
	11.0							-.088								
	20.0		0.462		0.208		-0.014	-.291	-.360	-.640	-.193		-0.061		-0.158	
	23.0					.116										
	32.0				.011											
	40.0	0.393			-.330	-.096		-.195	-.498	-.639		-.020		-.084		
	60.0	-.593			-.039	-.086		-.254	-.588	-.421	-.158		-.050			
	80.0	-.355			-.057	-.110		-.345	-.483	-.356		-.174				
	P.L.	-.355			-.043	-.090		-.248	-.359	-.366	-.229	-.174	-.050	-.084	-.158	-.091

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(h) $M = 0.95$; $\alpha = 5.1^\circ$

β, deg	∅, deg	Pressure coefficients for x/l of –														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0	P.L.	0.162				0.083		-0.050	-0.165	-0.258	-0.330	-0.045	-0.037	-0.059	-0.106	-0.038
	80.0	.162			0.152	.112		-.023	-.247	-.274		-.045				
	60.0	-.215			.200	.144		.030	-.278	-.322	-.297		-.037			
	40.0	.245			.161	.125		.055	-.259	-.371		-.010		-.059		
	32.0				.194											
	23.0					.230										
	20.0		0.400		.232		0.066	.001	-.270	-.463	-.203		-.023		-.106	
	11.0							.020								
	00.0			0.430		.204		.050	-.269	-.525	-.178	.000		-.069		-.038
-4.3	P.L.	0.268				0.155		0.024	-0.101	-0.211	-0.350	-0.116	-0.077	-0.078	-0.130	-0.067
	80.0	.268			0.228	.192		.063	-.168	-.231		-.116				
	60.0	-.112			.273	.216		.107	-.189	-.294	-.441		-.077			
	40.0	.119			.241	.186		.106	-.197	-.365		-.055		-.078		
	32.0				.234											
	23.0					.256										
	20.0		0.390		.238		0.085	.049	-.246	-.465	-.373		-.050		-.130	
	11.0							.045								
	00.0			0.393		.190		.036	-.283	-.541	-.249	-.026		-.098		-.067
4.3	00.0			0.413		0.198		0.037	-0.290	-0.555	-0.222	-0.019		-0.094		-0.063
	11.0							-.046								
	20.0		0.413		0.198		0.006	-.119	-.322	-.527	-.179		-0.036		-0.123	
	23.0					.162										
	32.0				.108											
	40.0	0.329			-.017	.028		-.031	-.351	-.415		-.009		-.068		
	60.0	-.362			.100	.050		-.061	-.389	-.360	-.180		-.017			
	80.0	.031			.065	.017		-.132	-.333	-.320		-.032				
	P.L.	.031				.007		-.128	-.230	-.306	-.246	-.032	-.017	-.068	-.123	-.063
-8.7	P.L.	0.349				0.234		0.105	-0.028	-0.145	-0.319	-0.407	-0.104	-0.126	-0.146	-0.073
	80.0	.349			0.295	.269		.146	-.088	-.178		-.407				
	60.0	-.009			.328	.273		.169	-.129	-.273	-.494		-.104			
	40.0	-.039			.259	.213		.125	-.150	-.382		-.164		-.126		
	32.0				.223											
	23.0					.232										
	20.0		0.340		.213		0.063	.033	-.240	-.498	-.653		-.076		-.146	
	11.0							.027								
	00.0			0.346		.147		-.008	-.323	-.598	-.359	-.109		-.141		-.073
8.7	00.0			0.373		0.162		-0.009	-0.365	-0.629	-0.350	-0.091		-0.142		-0.074
	11.0							-.173								
	20.0		0.382		0.132		-0.098	-.369	-.422	-.685	-.226		-0.080		-0.139	
	23.0					.050										
	32.0				-.040											
	40.0	0.329			-.309	-.116		-.222	-.505	-.522		-.075		-.097		
	60.0	-.563			-.038	-.076		-.236	-.540	-.410	-.205		-.138			
	80.0	-.291			-.044	-.085		-.293	-.433	-.368		-.105				
	P.L.	-.291				-.085		-.237	-.327	-.357	-.240	-.105	-.138	-.097	-.139	-.074

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(i) M = 0.95; α = 10.2°

β, deg	ϕ, deg	Pressure coefficients for x/l of –														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0.4	P.L.	0.160			0.116	0.072		-0.056	-0.167	-0.295	-0.416	-0.129	-0.060	-0.077	-0.093	-0.011
	80.0	.160			.132	.118		-.015	-.233	-.320		-.129				
	60.0	-.165			.166	.146		.001	-.256	-.375	-.437		-.060			
	40.0	.128			.146	.115		.012	-.279	-.415		-.056		-.077		
	32.0				.142											
	23.0					.161										
	20.0		0.317		.160		-0.004	-.048	-.311	-.481	-.287		-.035		-.093	
	11.0							-.039								
	00.0			0.319		.127		-.017	-.327	-.522	-.249	-.033		-.080		-.011
-3.8	P.L.	0.240			0.173	0.133		0.012	-0.110	-0.248	-0.409	-0.267	-0.075	-0.093	-0.119	-0.036
	80.0	.240			.191	.182		.053	-.181	-.289		-.267				
	60.0	-.130			.223	.196		.057	-.210	-.369	-.554		-.075			
	40.0	-.038			.191	.154		.048	-.250	-.443		-.117		-.093		
	32.0				.163											
	23.0					.176										
	20.0		0.308		.162		0.012	-.019	-.299	-.513	-.396		-.086		-.119	
	11.0							-.018								
	00.0			0.305		.117		-.025	-.340	-.543	-.285	-.068		-.137		-.036
4.7	00.0			0.326		0.121		-0.028	-0.351	-0.570	-0.263	-0.055		-0.150		-0.036
	11.0							-.095								
	20.0		0.336		0.135		-0.059	-.136	-.353	-.496	-.240		-0.043		-0.116	
	23.0					.109										
	32.0				.074											
	40.0	0.252			.018	.045		-.047	-.348	-.413		-.035		-.049		
	60.0	-.328			.091	.068		-.071	-.340	-.370	-.293		-.029			
	80.0	.072			.068	.042		-.093	-.300	-.336		-.062				
	P.L.	.072			.054	.008		-.119	-.230	-.315	-.357	-.062	-.029	-.049	-.116	-.036
-8.2	P.L.	0.290			0.231	0.193		0.080	-0.043	-0.206	-0.368	-0.570	-0.106	-0.121	-0.131	-0.048
	80.0	.290			.240	.239		.116	-.125	-.258		-.570				
	60.0	-.042			.253	.234		.097	-.194	-.371	-.616		-.106			
	40.0	-.179			.177	.151		.047	-.288	-.485		-.231		-.121		
	32.0				.131											
	23.0					.135										
	20.0		0.255		.132		-0.020	-.051	-.328	-.577	-.615		-.121		-.131	
	11.0							-.044								
	00.0			0.284		.077		-.064	-.392	-.630	-.353	-.186		-.109		-.048
9.1	00.0			0.282		0.079		-0.086	-0.446	-0.682	-0.354	-0.186		-0.113		-0.053
	11.0							-.239								
	20.0		0.308		0.069		-0.168	-.395	-.458	-.647	-.281		-0.246		-0.113	
	23.0					-.001										
	32.0				-.064											
	40.0	0.258			-.245	-.086		-.209	-.480	-.464		-.130		-.107		
	60.0	-.498			-.026	-.042		-.225	-.461	-.404	-.268		-.001			
	80.0	-.160			-.024	-.044		-.227	-.379	-.383		-.069				
	P.L.	-.160			-.027	-.076		-.219	-.298	-.360	-.295	-.069	-.001	-.107	-.113	-.053

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(j) $M = 0.99$; $\alpha = 0^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of –														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0	P.L.	0.193			0.174	0.117		-0.016	-0.142	-0.207	-0.272	-0.107	-0.019	-0.052	-0.129	-0.130
	80.0	.193			.178	.127		-.021	-.269	-.222		-.107				
	60.0	-.194			.251	.193		.060	-.283	-.274	-.257		-.019			
	40.0	.406			.203	.181		.113	-.209	-.324		-.074		-.052		
	32.0				.281											
	23.0					.330										
	20.0		0.526		.338		0.170	.081	-.173	-.434	-.289		-.017		-.129	
	11.0							.123								
	00.0			0.523		.319		.150	-.152	-.479	-.263	-.072		-.063		-.130
-4.3	P.L.	0.308			0.257	0.198		0.065	-0.060	-0.140	-0.253	-0.193	-0.040	-0.046	-0.135	-0.148
	80.0	.308			.273	.228		.093	-.148	-.157		-.193				
	60.0	-.037			.346	.285		.154	-.153	-.208	-.304		-.040			
	40.0	.311			.328	.269		.192	-.118	-.261		-.138		-.046		
	32.0				.337											
	23.0					.367										
	20.0		0.498		.351		0.199	.155	-.134	-.371	-.379		-.043		-.135	
	11.0							.153								
	00.0			0.493		.304		.141	-.158	-.469	-.323	-.099		-.081		-.148
4.3	00.0			0.519		0.313		0.132	-0.170	-0.477	-0.318	-0.105		-0.083		-0.141
	11.0							.056								
	20.0		0.499		0.298		0.109	-.057	-.235	-.535	-.305		-0.034		-0.152	
	23.0					.257										
	32.0				.182											
	40.0	0.437			-.014	.078		-.009	-.325	-.438		-.073		-.064		
	60.0	-.373			.130	.073		-.073	-.416	-.347	-.229		-.028			
	80.0	-.018			.080	.025		-.177	-.371	-.279		-.108				
	P.L.	-.018			.090	.039		-.111	-.220	-.280	-.290	-.108	-.028	-.064	-.152	-.141
-8.7	P.L.	0.411			0.334	0.275		0.145	0.017	-0.081	-0.226	-0.286	-0.085	-0.102	-0.188	-0.192
	80.0	.411			.353	.313		.187	-.047	-.098		-.286				
	60.0	.062			.416	.355		.230	-.050	-.160	-.324		-.085			
	40.0	.180			.373	.320		.232	-.055	-.239		-.350		-.102		
	32.0				.340											
	23.0					.361										
	20.0		0.455		.335		0.186	.161	-.123	-.365	-.486		-.093		-.188	
	11.0							.143								
	00.0			0.452		.267		.105	-.201	-.479	-.516	-.177		-.122		-.192
8.7	00.0			0.493		0.285		0.096	-0.235	-0.517	-0.531	-0.204		-0.131		-0.191
	11.0							-.049								
	20.0		0.491		0.239		0.029	-.284	-.323	-.607	-.405		-0.090		-0.198	
	23.0					.156										
	32.0				.047											
	40.0	0.433			-.320	-.062		-.173	-.481	-.652		-.130		-.102		
	60.0	-.639			-.008	-.053		-.235	-.564	-.430	-.261		-.072			
	80.0	-.384			-.033	-.074		-.324	-.447	-.344		-.284				
	P.L.	-.384			-.009	-.045		-.211	-.318	-.355	-.354	-.284	-.072	-.102	-.198	-.191

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(k) M = 0.99; $\alpha = 5.1^{\circ}$

β, deg	ϕ, deg	Pressure coefficients for x/l of –														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0	P.L.	0.172				0.109		-0.020	-0.130	-0.230	-0.314	-0.166	-0.060	-0.076	-0.144	-0.129
	80.0	.172			0.171	.135		.004	-.219	-.246		-.166				
	60.0	-.208			.227	.172		.077	-.252	-.295	-.312		-.060			
	40.0	.278			.182	.149		.089	-.228	-.342		-.126		-.076		
	32.0				.220											
	23.0					.259										
	20.0		0.435		.262		0.095	.030	-.228	-.438	-.291		-.048		-.144	
	11.0							.057								
	00.0			0.464		.239		.092	-.221	-.491	-.271	-.115		-.084		-.129
-4.3	P.L.	0.292				0.184		0.055	-0.065	-0.179	-0.312	-0.287	-0.096	-0.086	-0.161	-0.154
	80.0	.292			0.254	.218		.091	-.130	-.198		-.287				
	60.0	-.095			.302	.249		.144	-.150	-.257	-.390		-.096			
	40.0	.154			.270	.218		.144	-.158	-.320		-.201		-.086		
	32.0				.265											
	23.0					.291										
	20.0		0.425		.271		0.121	.088	-.196	-.420	-.385		-.072		-.161	
	11.0							.087								
	00.0			0.428		.227		.084	-.226	-.498	-.307	-.136		-.107		-.154
4.3	00.0			0.439		0.234		0.079	-0.243	-0.521	-0.328	-0.141		-0.109		-0.153
	11.0							-.010								
	20.0		0.441		0.228		0.036	-.107	-.289	-.534	-.288		-0.066		-0.168	
	23.0					.195										
	32.0				.134											
	40.0	0.365			-.004	.053		-.020	-.330	-.397		-.111		-.083		
	60.0	-.358			.127	.079		-.019	-.373	-.335	-.258		-.047			
	80.0	.025			.088	.045		-.122	-.316	-.285		-.133				
	P.L.	.025				.038		-.102	-.207	-.271	-.290	-.133	-.047	-.083	-.168	-.153
-8.7	P.L.	0.374				0.259		0.134	0.004	-0.114	-0.284	-0.403	-0.134	-0.123	-0.184	-0.170
	80.0	.374			0.323	.292		.170	-.063	-.144		-.403				
	60.0	.012			.358	.305		.203	-.103	-.228	-.437		-.134			
	40.0	-.006			.290	.247		.163	-.146	-.332		-.427		-.123		
	32.0				.248											
	23.0					.263										
	20.0		0.375		.247		0.095	.072	-.204	-.444	-.574		-.115		-.184	
	11.0							.064								
	00.0			0.381		.188		.037	-.278	-.535	-.472	-.203		-.141		-.170
8.7	00.0			0.407		0.199		0.038	-0.326	-0.583	-0.528	-0.209		-0.148		-0.172
	11.0							-.122								
	20.0		0.414		0.168		-0.057	-.337	-.381	-.645	-.334		-0.108		-0.184	
	23.0					.092										
	32.0				.002											
	40.0	0.368			-.272	-.071		-.179	-.468	-.528		-.169		-.114		
	60.0	-.547			.007	-.032		-.168	-.504	-.395	-.276		-.190			
	80.0	-.293			-.007	-.035		-.245	-.400	-.338		-.197				
	P.L.	-.293				-.035		-.192	-.292	-.323	-.294	-.197	-.190	-.114	-.184	-.172

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(l) $M = 0.99$; $\alpha = 10.3^{\circ}$

β, deg	ϕ, deg	Pressure coefficients for x/l of −														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0.4	P.L.	0.177			0.140	0.100		-0.025	-0.135	-0.255	-0.375	-0.257	-0.106	-0.100	-0.141	-0.092
	80.0	.177			.155	.144		.015	-.208	-.275		-.257				
	60.0	-.137			.192	.174		.037	-.230	-.326	-.399		-.106			
	40.0	.172			.173	.144		.054	-.245	-.366		-.170		-.100		
	32.0				.170											
	23.0					.192										
	20.0		0.348		.190		0.028	-.002	-.270	-.436	-.301		-.077		-.141	
	11.0							.007								
	00.0			0.350		.162		.031	-.279	-.481	-.271	-.136		-.095		-.092
-3.9	P.L.	0.268			0.204	0.168		0.047	-0.068	-0.210	-0.363	-0.418	-0.129	-0.117	-0.167	-0.123
	80.0	.268			.220	.215		.088	-.141	-.247		-.418				
	60.0	-.106			.252	.229		.094	-.177	-.322	-.505		-.129			
	40.0	-.012			.224	.188		.088	-.210	-.393		-.254		-.117		
	32.0				.196											
	23.0					.209										
	20.0		0.342		.194		0.049	.026	-.253	-.467	-.408		-.136		-.167	
	11.0							.027								
	00.0			0.338		.151		.021	-.289	-.502	-.308	-.160		-.165		-.123
4.8	00.0			0.355		0.156		0.009	-0.307	-0.532	-0.302	-0.162		-0.171		-0.125
	11.0							-.061								
	20.0		0.366		0.167		-0.025	-.105	-.310	-.467	-.283		-0.094		-0.183	
	23.0					.143										
	32.0				.104											
	40.0	0.283			.049	.080		-.023	-.307	-.377		-.144		-.079		
	60.0	-.296			.122	.102		-.053	-.302	-.338	-.314		-.082			
	80.0	.095			.099	.075		-.078	-.263	-.305		-.179				
	P.L.	.095			.085	.042		-.096	-.188	-.286	-.344	-.179	-.082	-.079	-.183	-.125
-8.3	P.L.	0.321			0.262	0.227		0.117	0.001	-0.173	-0.325	-0.523	-0.174	-0.160	-0.174	-0.143
	80.0	.321			.270	.271		.151	-.082	-.228		-.523				
	60.0	-.015			.284	.268		.134	-.149	-.329	-.553		-.174			
	40.0	-.152			.208	.183		.083	-.250	-.438		-.393		-.160		
	32.0				.163											
	23.0					.169										
	20.0		0.289		.164		0.015	-.024	-.285	-.530	-.634		-.176		-.174	
	11.0							-.013								
	00.0			0.318		.115		-.029	-.342	-.585	-.391	-.251		-.143		-.143
9.1	00.0			0.315		0.117		-0.037	-0.397	-0.627	-0.400	-0.252		-0.152		-0.143
	11.0							-.179								
	20.0		0.342		0.108		-0.125	-.334	-.402	-.609	-.318		-0.288		-0.169	
	23.0					.044										
	32.0				-.020											
	40.0	0.294			-.193	-.034		-.162	-.427	-.429		-.208		-.151		
	60.0	-.447			.014	.009		-.181	-.416	-.365	-.292		-.071			
	80.0	-.134			.017	.005		-.186	-.343	-.341		-.171				
	P.L.	-.134			.014	-.029		-.179	-.264	-.314	-.309	-.171	-.071	-.151	-.169	-.143

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(m) $M = 1.02$; $\alpha = 0^{\circ}$

β, deg	∅, deg	Pressure coefficients for x/l of −														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0	P.L.	0.242			0.220	0.166		0.033	-0.091	-0.161	-0.231	-0.107	-0.007	-0.036	-0.116	-0.129
	80.0	.242			.226	.180		.035	-.207	-.171		-.107				
	60.0	-.121			.291	.233		.114	-.213	-.220	-.239		-.007			
	40.0	.429			.253	.234		.166	-.144	-.268		-.070		-.036		
	32.0				.320											
	23.0					.367										
	20.0		0.541		.372		0.212	.136	-.117	-.373	-.277		-.004		-.116	
	11.0							.169								
	00.0			0.572		.351		.186	-.108	-.433	-.245	-.061		-.046		-.129
-4.3	P.L.	0.347			0.302	0.245		0.110	-0.010	-0.095	-0.204	-0.202	-0.040	-0.038	-0.129	-0.150
	80.0	.347			.318	.277		.141	-.091	-.106		-.202				
	60.0	.014			.380	.323		.201	-.096	-.156	-.272		-.040			
	40.0	.327			.365	.313		.235	-.064	-.215		-.161		-.038		
	32.0				.372											
	23.0					.400										
	20.0		0.520		.381		0.235	.196	-.089	-.323	-.377		-.041		-.129	
	11.0							.191								
	00.0			0.520		.333		.174	-.122	-.425	-.351	-.104		-.072		-.150
4.3	00.0			0.558		0.347		0.174	-0.121	-0.430	-0.274	-0.089		-0.066		-0.134
	11.0							.105								
	20.0		0.545		0.334		0.153	.008	-.173	-.464	-.278		-0.013		-0.131	
	23.0					.295										
	32.0				.225											
	40.0	0.465			.046	.129		.041	-.252	-.370		-.061		-.045		
	60.0	-.288			.173	.129		-.020	-.339	-.292	-.209		-.011			
	80.0	.037			.130	.078		-.123	-.312	-.233		-.088				
	P.L.	.037			.135	.085		-.062	-.170	-.237	-.257	-.088	-.011	-.045	-.131	-.134
-8.7	P.L.	0.452			0.380	0.323		0.192	0.067	-0.031	-0.173	-0.261	-0.091	-0.096	-0.184	-0.196
	80.0	.452			.397	.363		.236	.009	-.044		-.261				
	60.0	.113			.451	.393		.275	.001	-.109	-.282		-.091			
	40.0	.193			.411	.358		.274	-.005	-.195		-.373		-.096		
	32.0				.380											
	23.0					.395										
	20.0		0.484		.367		0.226	.199	-.080	-.321	-.466		-.094		-.184	
	11.0							.185								
	00.0			0.487		.298		.139	-.163	-.434	-.541	-.184		-.113		-.196
8.7	00.0			0.523		0.316		0.135	-0.190	-0.468	-0.457	-0.185		-0.113		-0.182
	11.0							-.005								
	20.0		0.520		0.274		0.065	-.219	-.267	-.547	-.377		-0.068		-0.179	
	23.0					.185										
	32.0				.083											
	40.0	0.462			-.256	-.008		-.121	-.414	-.575		-.112		-.085		
	60.0	-.555			.032	-.003		-.184	-.494	-.382	-.235		-.055			
	80.0	-.313			.014	-.032		-.280	-.401	-.307		-.251				
	P.L.	-.313			.029	-.007		-.172	-.277	-.320	-.326	-.251	-.055	-.085	-.179	-.182

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(n) M = 1.02; $\alpha = 5.1^\circ$

β, deg	ø, deg	Pressure coefficients for x/l of −														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0	P.L.	0.222				0.157		0.028	-0.084	-0.180	-0.272	-0.171	-0.052	-0.061	-0.127	-0.124
	80.0	.222			0.220	.185		.056	-.164	-.193		-.171				
	60.0	-.140			.268	.214		.128	-.189	-.241	-.299		-.052			
	40.0	.295			.229	.194		.142	-.168	-.290		-.116		-.061		
	32.0				.261											
	23.0					.298										
	20.0		0.466		.297		0.137	.086	-.176	-.381	-.277		-.035		-.127	
	11.0							.106								
	00.0			0.490		.269		.131	-.177	-.446	-.243	-.096		-.070		-.124
-4.3	P.L.	0.326				0.224		0.094	-0.025	-0.133	-0.263	-0.293	-0.093	-0.076	-0.152	-0.154
	80.0	.326			0.291	.258		.131	-.090	-.149		-.293				
	60.0	-.049			.335	.281		.191	-.108	-.208	-.361		-.093			
	40.0	.169			.304	.252		.181	-.114	-.277		-.205		-.076		
	32.0				.298											
	23.0					.321										
	20.0		0.450		.301		0.156	.128	-.154	-.376	-.385		-.066		-.152	
	11.0							.128								
	00.0			0.453		.258		.118	-.188	-.460	-.307	-.123		-.099		-.154
4.3	00.0			0.470		0.268		0.120	-0.196	-0.470	-0.274	-0.118		-0.093		-0.148
	11.0							.040								
	20.0		0.472		0.264		0.080	-.036	-.228	-.473	-.258		-0.049		-0.148	
	23.0					.232										
	32.0				.174											
	40.0	0.394			.051	.102		.029	-.266	-.348		-.093		-.066		
	60.0	-.283			.167	.123		.015	-.307	-.285	-.236		-.030			
	80.0	.076			.134	.092		-.083	-.269	-.240		-.114				
	P.L.	.076				.082		-.061	-.169	-.227	-.258	-.114	-.030	-.066	-.148	-.148
-8.7	P.L.	0.407				0.298		0.174	0.046	-0.077	-0.233	-0.374	-0.128	-0.113	-0.175	-0.170
	80.0	.407			0.357	.332		.212	-.018	-.105		-.374				
	60.0	.053			.388	.336		.244	-.066	-.191	-.397		-.128			
	40.0	.016			.321	.278		.198	-.115	-.294		-.469		-.113		
	32.0				.286											
	23.0					.297										
	20.0		0.403		.277		0.134	.107	-.167	-.403	-.556		-.109		-.175	
	11.0							.104								
	00.0			0.409		.218		.072	-.241	-.496	-.507	-.191		-.131		-.170
8.7	00.0			0.439		0.234		0.079	-0.279	-0.529	-0.485	-0.191		-0.130		-0.165
	11.0							-.078								
	20.0		0.448		0.203		-0.014	-.274	-.325	-.582	-.310		-0.094		-0.165	
	23.0					.125										
	32.0				.041											
	40.0	0.401			-.219	-.019		-.133	-.410	-.485		-.148		-.100		
	60.0	-.492			.046	.013		-.129	-.444	-.353	-.247		-.174			
	80.0	-.242			.035	.006		-.208	-.356	-.302		-.174				
	P.L.	-.242				.003		-.154	-.254	-.290	-.270	-.174	-.174	-.100	-.165	-.165

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(o) M = 1.02; $\alpha = 10.3^{\circ}$

β, deg	ø, deg	Pressure coefficients for x/l of –														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0.4	P.L.	0.210			0.176	0.139		0.014	-0.092	-0.208	-0.324	-0.217	-0.086	-0.083	-0.122	-0.088
	80.0	.210			.185	.181		.051	-.164	-.229		-.217				
	60.0	-.100			.223	.209		.076	-.191	-.282	-.343		-.086			
	40.0	.212			.207	.175		.096	-.206	-.323		-.142		-.083		
	32.0				.210											
	23.0					.232										
	20.0		0.381		.226		0.071	.041	-.226	-.392	-.259		-.053		-.122	
	11.0							.056								
	00.0			0.384		.198		.077	-.235	-.435	-.233	-.111		-.076		-.088
-3.9	P.L.	0.298			0.237	0.203		0.084	-0.025	-0.168	-0.315	-0.405	-0.119	-0.106	-0.153	-0.122
	80.0	.298			.254	.249		.124	-.097	-.207		-.405				
	60.0	-.066			.283	.261		.131	-.137	-.279	-.466		-.119			
	40.0	.009			.254	.218		.123	-.177	-.355		-.248		-.106		
	32.0				.226											
	23.0					.238										
	20.0		0.367		.224		0.078	.058	-.216	-.427	-.398		-.123		-.153	
	11.0							.060								
	00.0			0.366		.182		.056	-.251	-.464	-.285	-.147		-.148		-.122
4.8	00.0			0.385		0.188		0.041	-0.266	-0.499	-0.277	-0.146		-0.165		-0.129
	11.0							-.033								
	20.0		0.397		0.197		0.007	-.086	-.275	-.435	-.252		-0.081		-0.178	
	23.0					.175										
	32.0				.135											
	40.0	0.320			.074	.107		-.001	-.279	-.339		-.121		-.064		
	60.0	-.281			.151	.133		-.030	-.275	-.297	-.270		-.063			
	80.0	.121			.127	.104		-.055	-.238	-.262		-.154				
	P.L.	.121			.115	.075		-.067	-.156	-.245	-.299	-.154	-.063	-.064	-.178	-.129
-8.2	P.L.	0.345			0.286	0.250		0.143	0.032	-0.139	-0.291	-0.452	-0.146	-0.139	-0.159	-0.136
	80.0	.345			.293	.296		.177	-.051	-.195		-.452				
	60.0	.011			.311	.295		.163	-.112	-.285	-.491		-.146			
	40.0	-.103			.240	.212		.121	-.205	-.388		-.362		-.139		
	32.0				.197											
	23.0					.205										
	20.0		0.325		.200		0.052	.016	-.240	-.468	-.557		-.151		-.159	
	11.0							.024								
	00.0			0.352		.152		.010	-.294	-.526	-.346	-.218		-.129		-.136
9.1	00.0			0.346		0.150		-0.001	-0.353	-0.582	-0.380	-0.234		-0.141		-0.143
	11.0							-.140								
	20.0		0.372		0.141		-0.087	-.298	-.359	-.571	-.292		-0.274		-0.157	
	23.0					.079										
	32.0				.016											
	40.0	0.327			-.155	.007		-.127	-.388	-.398		-.191		-.142		
	60.0	-.414			.049	.049		-.145	-.378	-.331	-.264		-.057			
	80.0	-.110			.051	.044		-.149	-.309	-.304		-.151				
	P.L.	-.110			.049	.012		-.141	-.228	-.280	-.276	-.151	-.057	-.142	-.157	-.143

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(p) $M = 1.08$; $\alpha = 0^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of –														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0	P.L.	0.240			0.247	0.208		0.075	-0.041	-0.117	-0.184	-0.083	0.033	0.011	-0.061	-0.073
	80.0	.240			.253	.219		.065	-.159	-.128		-.083				
	60.0	-.116			.322	.276		.159	-.162	-.179	-.193		.033			
	40.0	.462			.280	.271		.215	-.091	-.225		-.047		.011		
	32.0				.350											
	23.0					.407										
	20.0		0.572		.402		0.256	.183	-.057	-.327	-.237		.038		-.061	
	11.0							.221								
	00.0			0.598		.393		.242	-.041	-.366	-.209	-.039		.002		-.073
-4.4	P.L.	0.349			0.322	0.277		0.148	0.030	-0.057	-0.155	-0.156	0.003	0.016	-0.066	-0.087
	80.0	.349			.335	.304		.174	-.063	-.071		-.156				
	60.0	.003			.407	.358		.242	-.063	-.119	-.204		.003			
	40.0	.343			.389	.344		.279	-.021	-.169		-.111		.016		
	32.0				.400											
	23.0					.439										
	20.0		0.557		.413		0.277	.244	-.028	-.271	-.301		.003		-.066	
	11.0							.246								
	00.0			0.565		.380		.234	-.052	-.356	-.265	-.070		-.020		-.087
4.4	00.0			0.577		0.387		0.227	-0.066	-0.366	-0.273	-0.087		-0.019		-0.084
	11.0							.156								
	20.0		0.571		0.361		0.197	.040	-.127	-.423	-.271		0.028		-0.084	
	23.0					.334										
	32.0				.250											
	40.0	0.497			.047	.158		.072	-.223	-.368		-.045		.002		
	60.0	-.341			.194	.168		.012	-.309	-.266	-.184		.030			
	80.0	-.040			.148	.117		-.097	-.263	-.193		-.078				
	P.L.	-.040			.161	.130		-.020	-.122	-.200	-.232	-.078	.030	.002	-.084	-.084
-8.7	P.L.	0.470			0.402	0.354		0.229	0.104	0.006	-0.122	-0.205	-0.069	-0.047	-0.119	-0.118
	80.0	.470			.421	.393		.269	.034	-.006		-.205				
	60.0	.114			.478	.428		.318	.026	-.065	-.218		-.069			
	40.0	.210			.438	.394		.320	.037	-.142		-.295		-.047		
	32.0				.405											
	23.0					.429										
	20.0		0.518		.397		0.266	.249	-.022	-.260	-.383		-.063		-.119	
	11.0							.235								
	00.0			0.518		.341		.196	-.096	-.367	-.437	-.163		-.063		-.118
8.7	00.0			0.546		0.355		0.192	-0.131	-0.402	-0.422	-0.178		-0.064		-0.122
	11.0							.062								
	20.0		0.546		0.305		0.119	-.183	-.208	-.486	-.390		-0.033		-0.128	
	23.0					.231										
	32.0				.123											
	40.0	0.511			-.238	.009		-.075	-.366	-.552		-.091		-.040		
	60.0	-.592			.056	.037		-.138	-.443	-.348	-.211		-.028			
	80.0	-.365			.047	.016		-.225	-.336	-.254		-.229				
	P.L.	-.365			.082	.041		-.112	-.219	-.269	-.291	-.229	-.028	-.040	-.128	-.122

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(q) M = 1.08; $\alpha = 5.1^{\circ}$

β, deg	ϕ, deg	Pressure coefficients for x/l of –														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0	P.L.	0.216				0.192		0.057	-0.051	-0.136	-0.215	-0.125	-0.016	-0.022	-0.074	-0.069
	80.0	.216			0.239	.216		.059	-.139	-.149		-.125				
	60.0	-.146			.289	.251		.146	-.161	-.195	-.232		-.016			
	40.0	.317			.248	.228		.181	-.124	-.243		-.075		-.022		
	32.0				.284											
	23.0					.332										
	20.0		0.504		.322		0.177	.132	-.118	-.339	-.223		-.000		-.074	
	11.0							.155								
	00.0			0.510		.310		.185	-.112	-.391	-.199	-.062		-.029		-.069
-4.3	P.L.	0.335				0.254		0.129	0.019	-0.091	-0.203	-0.236	-0.063	-0.033	-0.093	-0.095
	80.0	.335			0.308	.286		.162	-.056	-.107		-.236				
	60.0	-.063			.356	.314		.222	-.083	-.159	-.275		-.063			
	40.0	.181			.324	.283		.229	-.068	-.219		-.156		-.033		
	32.0				.321											
	23.0					.356										
	20.0		0.477		.325		0.193	.176	-.096	-.311	-.309		-.033		-.093	
	11.0							.179								
	00.0			0.474		.299		.177	-.120	-.388	-.244	-.086		-.055		-.095
4.3	00.0			0.490		0.309		0.175	-0.136	-0.406	-0.264	-0.095		-0.051		-0.093
	11.0							.094								
	20.0		0.493		0.294		0.129	.010	-.174	-.434	-.228		-0.014		-0.094	
	23.0					.274										
	32.0				.204											
	40.0	0.414			.071	.142		.057	-.221	-.317		-.062		-.024		
	60.0	-.301			.196	.172		.036	-.272	-.249	-.194		.003			
	80.0	.018			.159	.135		-.060	-.226	-.202		-.084				
	P.L.	.018				.128		-.018	-.125	-.186	-.211	-.084	.003	-.024	-.094	-.093
-8.7	P.L.	0.425				0.331		0.212	0.097	-0.038	-0.173	-0.298	-0.100	-0.061	-0.106	-0.070
	80.0	.425			0.383	.364		.249	.032	-.059		-.298				
	60.0	.054			.418	.374		.286	-.015	-.133	-.314		-.100			
	40.0	.032			.350	.318		.252	-.062	-.226		-.391		-.061		
	32.0				.315											
	23.0					.338										
	20.0		0.434		.311		0.184	.161	-.102	-.330	-.444		-.073		-.106	
	11.0							.159								
	00.0			0.442		.268		.136	-.167	-.416	-.444	-.154		-.083		-.070
8.7	00.0			0.466		0.269		0.138	-0.214	-0.461	-0.473	-0.168		-0.083		-0.076
	11.0							-.010								
	20.0		0.473		0.238		0.038	-.222	-.262	-.516	-.289		-0.057		-0.106	
	23.0					.152										
	32.0				.079											
	40.0	0.439			-.182	-.005		-.077	-.352	-.459		-.116		-.067		
	60.0	-.562			.083	.043		-.102	-.393	-.311	-.215		-.142			
	80.0	-.290			.076	.036		-.163	-.299	-.256		-.140				
	P.L.	-.290				.041		-.098	-.198	-.243	-.232	-.140	-.142	-.067	-.106	-.076

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(r) $M = 1.08$; $\alpha = 10.3^{\circ}$

β, deg	ϕ, deg	Pressure coefficients for x/l of —														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0.4	P.L.	0.222			0.200	0.180		0.047	-0.038	-0.153	-0.256	-0.188	-0.061	-0.041	-0.064	-0.029
	80.0	.222			.212	.223		.079	-.112	-.169		-.188				
	60.0	-.093			.251	.256		.106	-.139	-.221	-.285		-.061			
	40.0	.218			.239	.219		.128	-.147	-.261		-.107		-.041		
	32.0				.239											
	23.0					.272										
	20.0		0.403		.252		0.109	.077	-.160	-.327	-.208		-.025		-.064	
	11.0							.093								
	00.0			0.405		.240		.119	-.170	-.376	-.186	-.076		-.034		-.029
-3.9	P.L.	0.299			0.258	0.239		0.122	0.028	-0.110	-0.248	-0.372	-0.088	-0.065	-0.093	-0.057
	80.0	.299			.276	.286		.162	-.041	-.144		-.372				
	60.0	-.067			.307	.300		.175	-.080	-.211	-.395		-.088			
	40.0	.010			.283	.260		.175	-.117	-.283		-.220		-.065		
	32.0				.256											
	23.0					.280										
	20.0		0.390		.253		0.120	.108	-.148	-.358	-.341		-.092		-.093	
	11.0							.110								
	00.0			0.388		.228		.107	-.179	-.406	-.238	-.110		-.105		-.057
4.8	00.0			0.409		0.234		0.100	-0.194	-0.424	-0.230	-0.107		-0.116		-0.054
	11.0							.033								
	20.0		0.420		0.234		0.069	-.016	-.196	-.380	-.217		-0.048		-0.114	
	23.0					.229										
	32.0				.181											
	40.0	0.310			.128	.172		.060	-.200	-.281		-.096		-.021		
	60.0	-.232			.195	.194		.033	-.199	-.232	-.243		-.031			
	80.0	.127			.175	.171		.004	-.176	-.193		-.146				
	P.L.	.127			.158	.135		-.007	-.096	-.177	-.239	-.146	-.031	-.021	-.114	-.054
-8.2	P.L.	0.369			0.315	0.292		0.190	0.091	-0.076	-0.221	-0.398	-0.116	-0.091	-0.072	-0.050
	80.0	.369			.326	.340		.226	.013	-.138		-.398				
	60.0	.031			.342	.335		.216	-.047	-.218	-.423		-.116			
	40.0	-.110			.276	.259		.178	-.141	-.320		-.391		-.091		
	32.0				.233											
	23.0					.245										
	20.0		0.352		.232		0.100	.070	-.181	-.399	-.510		-.127		-.072	
	11.0							.077								
	00.0			0.381		.195		.063	-.226	-.454	-.327	-.186		-.076		-.050
9.1	00.0			0.379		0.187		0.060	-0.285	-0.504	-0.357	-0.199		-0.067		-0.051
	11.0							-.077								
	20.0		0.402		0.181		-0.023	-.247	-.290	-.510	-.247		-0.243		-0.067	
	23.0					.099										
	32.0				.063											
	40.0	0.366			-.107	.035		-.076	-.323	-.349		-.152		-.068		
	60.0	-.432			.095	.091		-.091	-.315	-.276	-.215		-.010			
	80.0	-.129			.097	.083		-.099	-.253	-.245		-.110				
	P.L.	-.129			.097	.052		-.086	-.174	-.224	-.218	-.110	-.010	-.068	-.067	-.051

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED FLAT-WINDSHIELD CANOPY 3

(s) M = 1.13; $\alpha = 0^{\circ}$

β, deg	ϕ, deg	Pressure coefficients for x/l of –														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0	P.L.	0.185			0.244	0.226		0.090	-0.013	-0.087	-0.159	-0.112	0.013	0.008	-0.057	-0.071
	80.0	.185			.256	.242		.067	-.120	-.095		-.112				
	60.0	-.121			.319	.297		.178	-.111	-.139	-.179		.013			
	40.0	.424			.279	.294		.242	-.047	-.187		-.065		.008		
	32.0				.340											
	23.0					.418										
	20.0		0.572		.392		0.274	.220	-.017	-.289	-.242		.015		-.057	
	11.0							.250								
	00.0			0.577		.401		.270	-.008	-.332	-.222	-.050		-.008		-.071
-4.4	P.L.	0.329			0.317	0.291		0.169	0.054	-0.032	-0.128	-0.182	-0.028	-0.001	-0.067	-0.093
	80.0	.329			.339	.324		.199	-.035	-.044		-.182				
	60.0	-.014			.402	.374		.278	-.020	-.083	-.185		-.028			
	40.0	.283			.384	.362		.313	.018	-.139		-.161		-.001		
	32.0				.384											
	23.0					.445										
	20.0		0.545		.398		0.290	.275	.005	-.238	-.310		-.024		-.067	
	11.0							.271								
	00.0			0.545		.381		.259	-.028	-.328	-.312	-.104		-.029		-.093
4.4	00.0			0.567		0.395		0.258	-0.027	-0.325	-0.241	-0.078		-0.025		-0.079
	11.0							.190								
	20.0		0.563		0.357		0.227	.094	-.074	-.361	-.250		0.019		-0.075	
	23.0					.344										
	32.0				.246											
	40.0	0.488			.067	.191		.112	-.155	-.305		-.045		-.004		
	60.0	-.359			.195	.198		.045	-.238	-.217	-.171		.022			
	80.0	-.111			.164	.145		-.067	-.217	-.159		-.074				
	P.L.	-.111			.171	.152		.007	-.092	-.165	-.206	-.074	.022	-.004	-.075	-.079
-8.8	P.L.	0.449			0.379	0.347		0.229	0.114	0.010	-0.112	-0.205	-0.105	-0.050	-0.123	-0.140
	80.0	.449			.414	.387		.275	.046	-.002		-.205				
	60.0	.059			.467	.435		.335	.045	-.046	-.193		-.105			
	40.0	.150			.426	.400		.338	.035	-.122		-.292		-.050		
	32.0				.379											
	23.0					.421										
	20.0		0.511		.382		0.267	.265	.001	-.234	-.357		-.082		-.123	
	11.0							.240								
	00.0			0.507		.342		.213	-.073	-.337	-.427	-.195		-.064		-.140
8.8	00.0			0.550		0.366		0.225	-0.088	-0.355	-0.356	-0.185		-0.068		-0.134
	11.0							.089								
	20.0		0.552		0.309		0.134	-.139	-.157	-.426	-.384		-0.038		-0.122	
	23.0					.226										
	32.0				.121											
	40.0	0.532			-.215	.009		-.033	-.295	-.462		-.094		-.045		
	60.0	-.508			.040	.022		-.092	-.373	-.297	-.197		-.032			
	80.0	-.322			.036	.011		-.188	-.291	-.224		-.211				
	P.L.	-.322			.066	.037		-.084	-.187	-.240	-.269	-.211	-.032	-.045	-.122	-.134

TABLE IV.- Continued

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(t) $M = 1.13$; $\alpha = 5.1^\circ$

β, deg	∅, deg	Pressure coefficients for x/l of –														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0	P.L.	0.184				0.213		0.077	-0.024	-0.111	-0.190	-0.171	-0.031	-0.017	-0.066	-0.072
	80.0	.184			0.244	.242		.068	-.107	-.120		-.171				
	60.0	-.157			.291	.275		.150	-.122	-.164	-.235		-.031			
	40.0	.268			.251	.252		.191	-.086	-.217		-.109		-.017		
	32.0				.282											
	23.0					.348										
	20.0		0.493		.315		0.195	.143	-.079	-.309	-.250		-.013		-.066	
	11.0							.175								
	00.0			0.485		.322		.206	-.080	-.366	-.220	-.081		-.024		-.072
-4.3	P.L.	0.316				0.272		0.145	0.045	-0.066	-0.176	-0.263	-0.083	-0.028	-0.090	-0.093
	80.0	.316			0.310	.306		.169	-.028	-.081		-.263				
	60.0	-.089			.355	.330		.233	-.057	-.132	-.267		-.083			
	40.0	.120			.321	.300		.263	-.040	-.195		-.204		-.028		
	32.0				.313											
	23.0					.368										
	20.0		0.467		.318		0.211	.200	-.064	-.287	-.343		-.044		-.090	
	11.0							.201								
	00.0			0.462		.306		.195	-.093	-.369	-.287	-.107		-.055		-.093
4.3	00.0			0.477		0.314		0.195	-0.104	-0.370	-0.242	-0.098		-0.051		-0.095
	11.0							.120								
	20.0		0.482		0.286		0.154	.045	-.128	-.381	-.230		-0.019		-0.087	
	23.0					.284										
	32.0				.200											
	40.0	0.384			.083	.165		.085	-.169	-.280		-.073		-.020		
	60.0	-.338			.197	.184		.060	-.219	-.214	-.198		-.001			
	80.0	-.067			.168	.149		-.032	-.189	-.169		-.100				
	P.L.	-.067				.139		.008	-.094	-.159	-.201	-.100	-.001	-.020	-.087	-.095
-8.8	P.L.	0.384				0.328		0.217	0.114	-0.026	-0.156	-0.284	-0.116	-0.059	-0.112	-0.107
	80.0	.384			0.368	.364		.257	.055	-.053		-.284				
	60.0	.070			.404	.377		.286	.005	-.117	-.290		-.116			
	40.0	.020			.337	.318		.275	-.046	-.209		-.388		-.059		
	32.0				.296											
	23.0					.335										
	20.0		0.406		.296		0.186	.165	-.089	-.308	-.420		-.087		-.112	
	11.0							.164								
	00.0			0.418		.269		.143	-.144	-.392	-.451	-.172		-.096		-.107
8.8	00.0			0.464		0.274		0.164	-0.176	-0.418	-0.409	-0.174		-0.090		-0.113
	11.0							.020								
	20.0		0.471		0.233		0.068	-.178	-.214	-.462	-.288		-0.069		-0.113	
	23.0					.145										
	32.0				.071											
	40.0	0.456			-.181	-.004		-.043	-.298	-.422		-.120		-.111		
	60.0	-.498			.058	.046		-.069	-.340	-.279	-.212		-.145			
	80.0	-.271			.066	.044		-.137	-.265	-.231		-.146				
	P.L.	-.271				.044		-.075	-.171	-.222	-.227	-.146	-.145	-.111	-.113	-.113

TABLE IV.- Concluded

PRESSURE COEFFICIENTS FOR FORWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 3

(u) M = 1.13; $\alpha = 10.3^\circ$

β, deg	∅, deg	Pressure coefficients for x/l of −														
		-0.015	0	0.004	0.065	0.164	0.223	0.239	0.309	0.382	0.455	0.527	0.655	0.760	0.869	0.993
0.4	P.L.	0.200			0.202	0.190		0.051	-0.043	-0.148	-0.238	-0.213	-0.050	-0.039	-0.049	-0.041
	80.0	.200			.217	.240		.079	-.117	-.165		-.213				
	60.0	-.128			.253	.304		.106	-.125	-.213	-.284		-.050			
	40.0	.195			.257	.259		.150	-.139	-.257		-.117		-.039		
	32.0				.244											
	23.0					.292										
	20.0		0.401		.255		0.115	.077	-.141	-.326	-.212		-.016		-.049	
	11.0							.092								
	00.0			0.399		.248		.121	-.152	-.378	-.193	-.087		-.028		-.041
-3.9	P.L.	0.271			0.257	0.250		0.120	0.033	-0.101	-0.215	-0.367	-0.088	-0.064	-0.089	-0.068
	80.0	.271			.275	.302		.159	-.032	-.133		-.367				
	60.0	-.110			.305	.319		.175	-.054	-.198	-.365		-.088			
	40.0	-.056			.290	.268		.182	-.112	-.265		-.234		-.064		
	32.0				.259											
	23.0					.296										
	20.0		0.388		.251		0.123	.103	-.132	-.335	-.349		-.092		-.089	
	11.0							.105								
	00.0			0.384		.231		.104	-.162	-.391	-.245	-.118		-.107		-.068
4.8	00.0			0.405		0.225		0.107		-0.405	-0.237	-0.116		-0.119		-0.077
	11.0							.035								
	20.0		0.415		0.233		0.072	-.026	-0.180	-.381	-.208		-0.048		-0.106	
	23.0					.226										
	32.0				.180											
	40.0	0.302			.121	.162		.055	-.193	-.279		-.088		-.016		
	60.0	-.313			.192	.189		.023	-.191	-.228	-.219		-.032			
	80.0	.045			.164	.156		-.007	-.176	-.187		-.127				
	P.L.	.045			.149	.121		-.009	-.095	- 172	-.218	-.127	-.032	-.016	-.106	-.077
-8.3	P.L.	0.356			0.307	0.292		0.185	0.095	-0.056	-0.192	-0.359	-0.124	-0.101	-0.096	-0.088
	80.0	.356			.317	.344		.228	.026	-.119		-.359				
	60.0	.007			.333	.349		.219	.015	-.206	-.382		-.124			
	40.0	-.180			.276	.257		.182	-.117	-.291		-.437		-.101		
	32.0				.229											
	23.0					.248										
	20.0		0.353		.222		0.095	.073	-.172	-.366	-.458		-.135		-.096	
	11.0							.077								
	00.0			0.377		.195		.065	-.203	-.421	-.342	-.197		-.092		-.088
9.2	00.0			0.376		0.183		0.078	-0.258	-0.465	-0.382	-0.211		-0.101		-0.082
	11.0							-.054								
	20.0		0.395		0.176		-0.008	-.228	-.258	-.476	-.247		-0.259		-0.084	
	23.0					.096										
	32.0				.052											
	40.0	0.383			-.119	.020		-.058	-.296	-.337		-.158		-.142		
	60.0	-.457			.075	.082		-.077	-.283	-.264	-.209		-.032			
	80.0	-.162			.084	.076		-.089	-.232	-.233		-.118				
	P.L.	-.162			.086	.047		-.074	-.154	-.212	-.205	-.118	-.032	-.142	-.084	-.082

TABLE V

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(a) M = 0.80; $\alpha = 0^\circ$

β, deg	∅, deg	Pressure coefficients for x/l of −													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0	P.L.	0.277		0.177	0.045	-0.020	-0.115		-0.186	-0.164	-0.182	-0.096	-0.053	-0.037	-0.005
	80.0				.045				-.204		-.182	-.096			
	60.0	.277			.068	-.039	-.119			-.210		-.084	-.053		
	48.0			.210											
	43.0	.367			.099	.017	-.097		-.194		-.227	-.079		-.037	
	40.0			.278											
	32.0				.174										
	29.0						-.065								
	26.0					.087									
	20.0		0.387		.193		.002	-0.095	-.120	-.295	-.207	-.065	-.034		
	00.0			.367	.157	.124		.023	-.112	-.358	-.208	-.047	-.032	-.022	-.005
-4.2	P.L.	0.356		0.279	0.135	0.086	-0.020		-0.115	-0.127	-0.179	-0.133	-0.078	-0.071	-0.023
	80.0				.135				-.113		-.187	-.133			
	60.0	.356			.179	.081	-.006			-.157		-.124	-.078		
	48.0			.292											
	43.0	.393			.216	.125	.010		-.091		-.259	-.129		-.071	
	40.0			.312											
	32.0				.229										
	29.0						.034								
	26.0					.139									
	20.0		0.366		.207		.050	-0.024	-.066	-.275	-.245	-.111	-.060		
	00.0			.348	.145	.112		.004	-.133	-.397	-.248	-.076	-.053	-.042	-.023
4.2	00.0			0.355	0.139	0.106		0.005	-0.134	-0.388	-0.234	-0.070	-0.052	-0.035	-0.017
	20.0		0.373		.146		-0.097	-.229	-.237	-.379	-.233	-.072	-.048		
	26.0					-.018									
	29.0						-.251								
	32.0				.067										
	40.0			.195											
	43.0	0.294			-.110	-.158	-.256		-.350		-.232	-.068		-.048	
	48.0			.052											
	60.0	.158			-.092	-.196	-.263			-.281		-.065	-.052		
	80.0				-.076				-.296		-.180	-.087			
	P.L.	.158		.044	-.076	-.135	-.213		-.258	-.208	-.198	-.087	-.052	-.048	-.017
-8.5	P.L.	0.398		0.354	0.244	0.177	0.065		-0.049	-0.089	-0.179	-0.176	-0.125	-0.132	-0.067
	80.0				.244				-.031		-.203	-.176			
	60.0	.398			.264	.162	.075			-.130		-.199	-.125		
	48.0			.346											
	43.0	.366			.250	.174	.067		-.039		-.341	-.228		-.132	
	40.0			.289											
	32.0				.222										
	29.0						.058								
	26.0					.128									
	20.0		0.313		.184		.038	-0.026	-.073	-.323	-.361	-.223	-.132		
	00.0			.290	.096	.064		-.051	-.202	-.511	-.354	-.151	-.099	-.093	-.067
8.5	00.0			0.309	0.087	0.053		-0.046	-0.209	-0.501	-0.334	-0.149	-0.102	-0.082	-0.049
	20.0		0.322		.062		-0.238	-.464	-.422	-.553	-.321	-.115	-.098		
	26.0					-.179									
	29.0						-.553								
	32.0				-.099										
	40.0			.063											
	43.0	0.168			-.427	-.424	-.474		-.586		-.265	-.102		-.086	
	48.0			-.193											
	60.0	-.025			-.322	-.388	-.434			-.356		-.094	-.100		
	80.0				-.213				-.379		-.203	-.153			
	P.L.	-.025		-.116	-.213	-.258	-.325		-.351	-.287	-.263	-.153	-.100	-.086	-.049

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(b) $M = 0.80$; $\alpha = 5.1^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of –													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0	P.L.	0.242		0.158	0.037	-0.032	-0.123		-0.206	-0.197	-0.219	-0.137	-0.054	-0.038	-0.001
	80.0				.037				-.203		-.220	-.137			
	60.0	.242			.050	-.045	-.125			-.231		-.108	-.054		
	48.0			.181											
	43.0	.306			.076	-.007	-.123		-.209		-.256	-.097		-.038	
	40.0			.224											
	32.0				.118										
	29.0						-.102								
	26.0					.023									
	20.0		0.321		.128		-.063	-0.156	-.171	-.332	-.225	-.067	-.036		
	00.0			.302	.086	.050		-.055	-.180	-.391	-.213	-.054	-.034	-.019	-.001
-4.2	P.L.	0.296		0.232	0.120	0.057	-0.047		-0.151	-0.173	-0.237	-0.185	-0.087	-0.064	-0.019
	80.0				.120				-.134		-.245	-.185			
	60.0	.296			.136	.040	-.045			-.208		-.173	-.087		
	48.0			.248											
	43.0	.319			.153	.072	-.046		-.140		-.314	-.163		-.064	
	40.0			.244											
	32.0				.158										
	29.0						-.034								
	26.0					.059									
	20.0		0.302		.136		-.028	-0.102	-.136	-.335	-.281	-.115	-.066		
	00.0			.284	.070	.035		-.076	-.201	-.432	-.248	-.084	-.069	-.042	-.019
4.2	00.0			0.280	0.069	0.030		-0.069	-0.205	-0.425	-0.247	-0.081	-0.066	-0.037	-0.014
	20.0		0.295		.081		-0.161	-.292	-.277	-.402	-.234	-.070	-.063		
	26.0					-.080									
	29.0						-.275								
	32.0				.017										
	40.0			.148											
	43.0	0.224			-.118	-.162	-.264		-.340		-.231	-.071		-.070	
	48.0			.026											
	60.0	.111			-.100	-.187	-.254			-.280		-.073	-.045		
	80.0				-.083				-.286		-.198	-.098			
	P.L.	.111		.025	-.083	-.138	-.214		-.267	-.224	-.211	-.098	-.045	-.070	-.014
-8.5	P.L.	0.301		0.278	0.195	0.140	0.034		-0.085	-0.136	-0.237	-0.231	-0.129	-0.107	-0.028
	80.0				.195				-.057		-.272	-.231			
	60.0	.301			.205	.114	.027			-.194		-.266	-.129		
	48.0			.264											
	43.0	.260			.172	.103	-.006		-.107		-.425	-.273		-.107	
	40.0			.204											
	32.0				.137										
	29.0						-.027								
	26.0					.036									
	20.0		0.239		.111		-.047	-0.109	-.152	-.395	-.410	-.206	-.095		
	00.0			.224	.024	-.012		-.131	-.272	-.541	-.344	-.138	-.094	-.060	-.028
8.5	00.0			0.232	0.011	-0.027		-0.128	-0.292	-0.548	-0.357	-0.142	-0.100	-0.055	-0.029
	20.0		0.247		-.005		-0.320	-.525	-.459	-.561	-.306	-.123	-.096		
	26.0					-.240									
	29.0						-.566								
	32.0				-.144										
	40.0			.028											
	43.0	0.113			-.418	-.400	-.461		-.539		-.245	-.116		-.083	
	48.0			-.193											
	60.0	-.044			-.297	-.358	-.408			-.339		-.134	-.162		
	80.0				-.211				-.361		-.210	-.110			
	P.L.	-.044		-.121	-.211	-.252	-.317		-.344	-.278	-.239	-.110	-.162	-.083	-.029

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(c) $M = 0.80$; $\alpha = 10.2^{\circ}$

β, deg	∅, deg	Pressure coefficients for x/l of –													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0.2	P.L.	0.161		0.104	0.002	-0.043	-0.131		-0.213	-0.221	-0.246	-0.149	-0.048	-0.040	0.012
	80.0				.002				-.197		-.247	-.149			
	60.0	.161			.027	-.063	-.139			-.248		-.118	-.048		
	48.0			.133											
	43.0	.214			.039	-.037	-.146		-.227		-.266	-.095		-.040	
	40.0			.172											
	32.0				.067										
	29.0						-.146								
	26.0					-.026									
	20.0		0.238		.070		-.118	-0.202	-.214	-.353	-.223	-.063	-.029		
	00.0			.229	.038	-.011		-.117	-.218	-.415	-.209	-.051	-.019	-.003	.012
-4.0	P.L.	0.141		0.173	0.082	0.035	-0.060		-0.167	-0.206	-0.276	-0.204	-0.076	-0.046	-0.011
	80.0				.082				-.134		-.292	-.204			
	60.0	.141			.107	.017	-.069			-.246		-.197	-.076		
	48.0			.193											
	43.0	.226			.108	.028	-.091		-.181		-.360	-.170		-.046	
	40.0			.186											
	32.0				.095										
	29.0						-.093								
	26.0					-.002							-.061		
	20.0		0.224		.075		-.091	-0.162	-.191	-.372	-.299			-.030	-.011
	00.0			.216	.020	-.024		-.140	-.242	-.453	-.240	-.091	-.094		
4.4	00.0			0.219	0.011	-0.034		-0.137	-0.243	-0.464	-0.246	-0.090	-0.080	-0.027	-0.011
	20.0		0.233		.026		-0.202	-.324	-.302	-.407	-.222	-.069	-.051		
	26.0					-.113									
	29.0						-.278								
	32.0				-.015										
	40.0			.117											
	43.0	0.176			-.109	-.154	-.256		-.322		-.230	-.071		-.047	
	48.0			.027						-.274					
	60.0	.089			-.087	-.169	-.237					-.081	-.037		
	80.0				-.086				-.264		-.216	-.111			
	P.L.	.089		.016	-.086	-.129	-.203		-.263	-.234	-.223	-.111	-.037	-.047	-.011
-8.3	P.L.	0.235		0.225	0.153	0.109	0.008		-0.114	-0.177	-0.289	-0.256	-0.121	-0.066	-0.019
	80.0				.153				-.074		-.335	-.256			
	60.0	.235			.158	.069	-.021			-.258		-.298	-.121		
	48.0			.204											
	43.0	.186			.099	.032	-.075		-.176		-.506	-.278		-.066	
	40.0			.136											
	32.0				.062										
	29.0						-.113								
	26.0					-.043									
	20.0		0.185		.050		-.124	-0.185	-.222	-.455	-.438	-.173	-.092		
	00.0			.176	-.034	-.074		-.195	-.325	-.564	-.326	-.160	-.073	-.029	-.019
8.7	00.0			0.177	-0.058	-0.100		-0.200	-0.352	-0.595	-0.352	-0.166	-0.083	-0.031	-0.022
	20.0		0.196		-.060		-0.356	-.550	-.472	-.542	-.275	-.166	-.065		
	26.0					-.271									
	29.0						-.538								
	32.0				-.169										
	40.0			.009											
	43.0	0.092			-.373	-.355	-.425		-.479		-.235	-.156		-.109	
	48.0			-.157						-.320			-.058		
	60.0	-.032			-.251	-.315	-.366					-.117			
	80.0				-.199				-.333		-.219	-.102			
	P.L.	-.032		-.107	-.199	-.233	-.296		-.330	-.272	-.224	-.102	-.058	-.109	-.022

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(d) $M = 0.90$; $\alpha = 0^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of –													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0	P.L.	0.310		0.197	0.055	-0.012	-0.122		-0.220	-0.213	-0.223	-0.101	-0.060	-0.038	-0.005
	80.0				.055				-.250		-.221	-.101			
	60.0	.310			.078	-.038	-.133			-.285		-.090	-.060		
	48.0			.237											
	43.0	.402			.103	.025	-.106		-.236		-.259	-.086		-.038	
	40.0			.306											
	32.0				.190										
	29.0						-.072								
	26.0					.105									
	20.0		0.423		.207		.005	-0.106	-.141	-.397	-.232	-.073	-.043		
	00.0			.399	.175	.143		.023	-.116	-.433	-.225	-.057	-.042	-.023	-.005
-4.3	P.L.	0.388		0.300	0.160	0.096	-0.023		-0.136	-0.165	-0.239	-0.146	-0.088	-0.072	-0.026
	80.0				.160				-.138		-.250	-.146			
	60.0	.388			.201	.089	-.009			-.203		-.136	-.088		
	48.0			.325											
	43.0	.430			.231	.139	.011		-.110		-.324	-.139		-.072	
	40.0			.344											
	32.0				.247										
	29.0						.037								
	26.0					.158									
	20.0		0.399		.224		.057	-0.026	-.073	-.349	-.298	-.121	-.071		
	00.0			.380	.162	.129		.003	-.128	-.474	-.261	-.086	-.065	-.043	-.026
4.3	00.0			0.385	0.155	0.122		0.009	-0.138	-0.474	-0.246	-0.085	-0.066	-0.041	-0.021
	20.0		0.403		.160		-0.092	-.254	-.263	-.526	-.249	-.082	-.062		
	26.0					-.001									
	29.0						-.274								
	32.0				.081										
	40.0			.224											
	43.0	0.326			-.114	-.156	-.274		-.414		-.255	-.079		-.051	
	48.0			.074											
	60.0	.189			-.089	-.195	-.288			-.389		-.077	-.064		
	80.0				-.066				-.371		-.209	-.093			
	P.L.	.189		.066	-.066	-.125	-.225		-.313	-.273	-.227	-.093	-.064	-.051	-.021
-8.6	P.L.	0.427		0.370	0.252	0.187	0.066		-0.063	-0.110	-0.238	-0.183	-0.126	-0.127	-0.059
	80.0				.252				-.051		-.268	-.183			
	60.0	.427			.280	.172	.073			-.151		-.200	-.126		
	48.0			.370											
	43.0	.404			.269	.190	.072		-.055		-.442	-.222		-.127	
	40.0			.321											
	32.0				.244										
	29.0						.066								
	26.0					.150									
	20.0		0.352		.208		.058	-0.015	-.076	-.357	-.551	-.211	-.127		
	00.0			.331	.122	.094		-.027	-.174	-.535	-.503	-.137	-.103	-.082	-.059
8.6	00.0			0.345	0.108	0.075		-0.026	-0.200	-0.546	-0.406	-0.149	-0.111	-0.082	-0.049
	20.0		0.361		.084		-0.209	-.520	-.428	-.705	-.280	-.123	-.107		
	26.0					-.148									
	29.0						-.548								
	32.0				-.076										
	40.0			.102											
	43.0	0.211			-.437	-.430	-.503		-.608		-.246	-.119		-.089	
	48.0			-.164											
	60.0	.016			-.344	-.395	-.488			-.547		-.129	-.108		
	80.0				-.202				-.466		-.228	-.119			
	P.L.	.016		-.084	-.202	-.250	-.352		-.411	-.407	-.264	-.119	-.108	-.089	-.049

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(e) $M = 0.90$; $\alpha = 5.1^{\circ}$

β, deg	ϕ, deg	Pressure coefficients for x/l of –													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0	P.L.	0.235		0.157	0.041	-0.019	-0.126		-0.233	-0.246	-0.267	-0.140	-0.060	-0.038	-0.001
	80.0				.041				-.241		-.266	-.140			
	60.0	.235			.061	-.038	-.132			-.298		-.111	-.060		
	48.0			.192											
	43.0	.300			.081	.004	-.126		-.240		-.286	-.100		-.038	
	40.0			.247											
	32.0				.131										
	29.0						-.107								
	26.0					.039									
	20.0		0.327		.142		-.059	-0.166	-.186	-.420	-.246	-.075	-.043		
	00.0			.315	.107	.068		-.055	-.180	-.464	-.225	-.064	-.039	-.017	-.001
-4.3	P.L.	0.333		0.262	0.144	0.076	-0.037		-0.161	-0.203	-0.304	-0.192	-0.090	-0.062	-0.017
	80.0				.144				-.148		-.316	-.192			
	60.0	.333			.163	.063	-.036			-.248		-.179	-.090		
	48.0			.282											
	43.0	.353			.177	.094	-.035		-.148		-.399	-.167		-.062	
	40.0			.279											
	32.0				.181										
	29.0						-.025								
	26.0					.082									
	20.0		0.335		.155		-.016	-0.103	-.135	-.410	-.342	-.120	-.073		
	00.0			.317	.089	.056		-.076	-.190	-.520	-.264	-.092	-.077	-.042	-.017
4.3	00.0			0.310	0.087	0.049		-0.069	-0.206	-0.512	-0.252	-0.093	-0.076	-0.041	-0.015
	20.0		0.326		.098		-0.154	-.322	-.295	-.540	-.243	-.081	-.075		
	26.0					-.058									
	29.0						-.288								
	32.0				.035										
	40.0			.180											
	43.0	0.255			-.109	-.149	-.272		-.389		-.248	-.082		-.078	
	48.0			.053											
	60.0	.144			-.083	-.176	-.264			-.378		-.084	-.053		
	80.0				-.067				-.347		-.227	-.103			
	P.L.	.144		.051	-.067	-.123	-.220		-.314	-.292	-.240	-.103	-.053	-.078	-.015
-8.6	P.L.	0.334		0.309	0.219	0.164	0.050		-0.086	-0.146	-0.293	-0.230	-0.136	-0.097	-0.031
	80.0				.219				-.062		-.331	-.230			
	60.0	.334			.231	.137	.040			-.203		-.264	-.136		
	48.0			.299											
	43.0	.296			.198	.127	.011		-.120		-.555	-.263		-.097	
	40.0			.241											
	32.0				.164										
	29.0						-.010								
	26.0					.061									
	20.0		0.279		.137		-.024	-0.097	-.171	-.432	-.668	-.183	-.105		
	00.0			.265	.047	.014		-.108	-.271	-.592	-.478	-.151	-.105	-.054	-.031
8.6	00.0			0.271	0.032	-0.005		-0.101	-0.277	-0.607	-0.452	-0.151	-0.113	-0.055	-0.030
	20.0		0.284		.017		-0.299	-.578	-.456	-.742	-.299	-.145	-.107		
	26.0					-.210									
	29.0						-.571								
	32.0				-.126										
	40.0			.066											
	43.0	0.154			-.425	-.408	-.495		-.567		-.253	-.168		-.086	
	48.0			-.163											
	60.0	-.005			-.302	-.360	-.451			-.506		-.186	-.140		
	80.0				-.196				-.418		-.236	-.086			
	P.L.	-.005		-.092	-.196	-.240	-.340		-.390	-.395	-.248	-.086	-.140	-.086	-.030

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(f) $M = 0.90$; $\alpha = 10.2^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of —													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0.2	P.L.	0.188		0.138	0.028	-0.021	-0.117		-0.232	-0.271	-0.318	-0.162	-0.060	-0.048	0.010
	80.0				.028				-.218		-.318	-.162			
	60.0	.188			.051	-.033	-.126			-.315		-.133	-.060		
	48.0			.164											
	43.0	.239			.065	-.014	-.140		-.244		-.336	-.110		-.048	
	40.0			.200											
	32.0				.086										
	29.0						-.135								
	26.0					-.008									
	20.0		0.264		.087		-.109	-0.209	-.224	-.448	-.267	-.077	-.038		
	00.0			.252	.052	.005		-.123	-.237	-.512	-.237	-.065	-.029	-.006	.010
-4.0	P.L.	0.240		0.205	0.109	0.063	-0.040		-0.171	-0.234	-0.360	-0.212	-0.085	-0.042	-0.012
	80.0				.109				-.142		-.385	-.212			
	60.0	.240			.135	.044	-.052			-.285		-.207	-.085		
	48.0			.226											
	43.0	.252			.131	.051	-.076		-.186		-.510	-.174		-.042	
	40.0			.214											
	32.0				.119										
	29.0						-.083								
	26.0					.019									
	20.0		0.256		.095		-.079	-0.163	-.195	-.459	-.396	-.123	-.071		
	00.0			.244	.037	-.006		-.142	-.251	-.559	-.282	-.110	-.101	-.028	-.012
4.5	00.0			0.247	0.027	-0.015		-0.137	-0.263	-0.551	-0.268	-0.111	-0.091	-0.029	-0.016
	20.0		0.261		.045		-0.195	-.353	-.312	-.529	-.245	-.082	-.058		
	26.0					-.095									
	29.0						-.278								
	32.0				.001										
	40.0			.149											
	43.0	0.204			-.091	-.136	-.256		-.356		-.256	-.084		-.051	
	48.0			.056											
	60.0	.118			-.069	-.148	-.234			-.370		-.093	-.044		
	80.0				-.068				-.312		-.255	-.125			
	P.L.	.118		.048	-.068	-.113	-.204		-.303	-.313	-.270	-.125	-.044	-.051	-.016
-8.4	P.L.	0.262		0.254	0.181	0.136	0.029		-0.114	-0.184	-0.344	-0.245	-0.124	-0.070	-0.026
	80.0				.181				-.077		-.395	-.245			
	60.0	.262			.184	.095	-.004			-.264		-.284	-.124		
	48.0			.237											
	43.0	.217			.124	.057	-.057		-.195		-.676	-.251		-.070	
	40.0			.168											
	32.0				.088										
	29.0						-.097								
	26.0					-.019									
	20.0		0.218		.071		-.103	-0.174	-.270	-.502	-.779	-.190	-.090		
	00.0			.210	-.014	-.054		-.175	-.375	-.646	-.457	-.237	-.084	-.034	-.026
8.8	00.0			0.216	-0.036	-0.074		-0.174	-0.351	-0.666	-0.435	-0.208	-0.083	-0.033	-0.027
	20.0		0.235		-.038		-0.342	-.583	-.467	-.711	-.310	-.230	-.091		
	26.0					-.243									
	29.0						-.537								
	32.0				-.149										
	40.0			.051											
	43.0	0.133			-.362	-.346	-.444		-.515		-.271	-.169		-.098	
	48.0			-.121											
	60.0	.008			-.234	-.292	-.382			-.456		-.092	-.065		
	80.0				-.179				-.390		-.254	-.094			
	P.L.			-.073	-.179	-.217	-.308		-.382	-.377	-.255	-.094	-.065	-.098	-.027

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(g) M = 0.95; $\alpha = 0^\circ$

β, deg	∅, deg	Pressure coefficients for x/l of –													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0	P.L.	0.342		0.234	0.085	0.019	-0.092		-0.205	-0.215	-0.313	-0.086	-0.070	-0.035	-0.006
	80.0				.085				-.238		-.319	-.086			
	60.0	.342			.107	.003	-.093			-.293		-.077	-.070		
	48.0			.269											
	43.0	.430			.136	.059	-.075		-.214		-.396	-.069		-.035	
	40.0			.334											
	32.0				.213										
	29.0						-.038								
	26.0					.132									
	20.0		0.444		.229		.032	-0.082	-.110	-.391	-.404	-.056	-.053		
	00.0			.422	.193	.167		.039	-.085	-.430	-.398	-.042	-.051	-.022	-.006
-4.3	P.L.	0.420		0.333	0.191	0.121	0.001		-0.125	-0.148	-0.287	-0.160	-0.095	-0.066	-0.025
	80.0				.191				-.130		-.302	-.160			
	60.0	.420			.226	.116	.013			-.192		-.137	-.095		
	48.0			.356											
	43.0	.463			.255	.162	.033		-.097		-.423	-.127		-.066	
	40.0			.372											
	32.0				.269										
	29.0						.062								
	26.0					.182									
	20.0		0.426		.245		.083	-0.008	-.051	-.327	-.480	-.103	-.075		
	00.0			.406	.185	.158		.025	-.095	-.442	-.513	-.074	-.073	-.042	-.025
4.3	00.0			0.411	0.176	0.149		0.033	-0.102	-0.446	-0.449	-0.077	-0.069	-0.038	-0.019
	20.0		0.431		.188		-0.051	-.224	-.202	-.486	-.422	-.073	-.068		
	26.0					.035									
	29.0						-.212								
	32.0				.111										
	40.0			.258											
	43.0	0.362			-.061	-.106	-.229		-.353		-.400	-.072		-.049	
	48.0			.119											
	60.0	.230			-.046	-.131	-.237			-.422		-.071	-.066		
	80.0				-.023				-.344		-.329	-.084			
	P.L.	.230		.114	-.023	-.081	-.189		-.284	-.311	-.342	-.084	-.066	-.049	-.019
-8.7	P.L.	0.459		0.408	0.287	0.225	0.105		-0.039	-0.087	-0.229	-0.427	-0.139	-0.125	-0.059
	80.0				.287				-.028		-.258	-.427			
	60.0	.459			.312	.211	.110			-.124		-.416	-.139		
	48.0			.405											
	43.0	.434			.299	.222	.107		-.038		-.452	-.322		-.125	
	40.0			.352											
	32.0				.271										
	29.0						.099								
	26.0					.182									
	20.0		0.378		.231		.092	0.022	-.083	-.325	-.586	-.231	-.130		
	00.0			.358	.146	.123		.012	-.242	-.503	-.679	-.174	-.120	-.090	-.059
8.7	00.0			0.376	0.133	0.106		0.011	-0.166	-0.496	-0.628	-0.170	-0.106	-0.069	-0.045
	20.0		0.395		.111		-0.176	-.450	-.376	-.633	-.629	-.150	-.105		
	26.0					-.108									
	29.0						-.490								
	32.0				-.044										
	40.0			.142											
	43.0	0.255			-.384	-.374	-.437		-.557		-.454	-.145		-.079	
	48.0			-.117											
	60.0	.061			-.324	-.346	-.426			-.583		-.151	-.137		
	80.0				-.189				-.453		-.387	-.125			
	P.L.	.061		-.040	-.189	-.213	-.308		-.405	-.437	-.432	-.125	-.137	-.079	-.045

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(h) $M = 0.95$; $\alpha = 5.1^{\circ}$

β, deg	ϕ, deg	Pressure coefficients for x/l of –													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0	P.L.	0.257		0.182	0.063	0.003	-0.103		-0.221	-0.240	-0.359	-0.146	-0.059	-0.035	0.002
	80.0				.063				-.233		-.360	-.146			
	60.0	.257			.081	-.012	-.108			-.298		-.115	-.059		
	48.0			.215											
	43.0	.323			.100	.029	-.100		-.227		-.431	-.100		-.035	
	40.0			.272											
	32.0				.151										
	29.0						-.083								
	26.0					.063									
	20.0		0.351		.162		-.035	-0.158	-.167	-.422	-.419	-.082	-.042		
	00.0			.339	.127	.093		-.041	-.154	-.460	-.398	-.077	-.039	-.013	.002
-4.3	P.L.	0.359		0.288	0.164	0.102	-0.012		-0.154	-0.184	-0.336	-0.266	-0.086	-0.054	-0.016
	80.0				.164				-.149		-.353	-.266			
	60.0	.359			.184	.086	-.011			-.229		-.227	-.086		
	48.0			.308											
	43.0	.383			.197	.117	-.013		-.146		-.489	-.193		-.054	
	40.0			.304											
	32.0				.200										
	29.0						-.001								
	26.0					.105									
	20.0		0.362		.177		.012	-0.082	-.124	-.382	-.528	-.142	-.075		
	00.0			.343	.112	.082		-.053	-.169	-.486	-.496	-.117	-.085	-.037	-.016
4.3	00.0			0.334	0.106	0.075		-0.041	-0.175	-0.489	-0.447	-0.116	-0.080	-0.036	-0.015
	20.0		0.350		.119		-0.126	-.307	-.262	-.535	-.413	-.100	-.082		
	26.0					-.034									
	29.0						-.259								
	32.0				.054										
	40.0			.206											
	43.0	0.281			-.090	-.124	-.253		-.362		-.409	-.093		-.073	
	48.0			.082											
	60.0	.171			-.062	-.144	-.249			-.410		-.093	-.045		
	80.0				-.044				-.338		-.361	-.108			
	P.L.	.171		.079	-.044	-.095	-.197		-.305	-.309	-.371	-.108	-.045	-.073	-.015
-8.7	P.L.	0.370		0.341	0.247	0.194	0.080		-0.067	-0.135	-0.276	-0.525	-0.130	-0.080	-0.035
	80.0				.247				-.045		-.313	-.525			
	60.0	.370			.257	.164	.068			-.193		-.487	-.130		
	48.0			.332											
	43.0	.332			.222	.154	.038		-.103		-.538	-.342		-.080	
	40.0			.270											
	32.0				.190										
	29.0						.018								
	26.0					.091									
	20.0		0.309		.160		.008	-0.062	-.171	-.405	-.678	-.253	-.116		
	00.0			.297	.070	.043		-.069	-.324	-.561	-.723	-.252	-.103	-.044	-.035
8.7	00.0			0.298	0.053	0.021		-0.071	-0.276	-0.560	-0.725	-0.239	-0.123	-0.042	-0.032
	20.0		0.313		.038		-0.274	-.517	-.448	-.696	-.554	-.222	-.104		
	26.0					-.186									
	29.0						-.527								
	32.0				-.103										
	40.0			.098											
	43.0	0.186			-.406	-.383	-.445		-.555		-.446	-.220		-.122	
	48.0			-.130											
	60.0	.029			-.303	-.323	-.409			-.540		-.225	-.050		
	80.0				-.180				-.449		-.398	-.100			
	P.L.	.029		-.061	-.180	-.213	-.300		-.418	-.418	-.419	-.100	-.050	-.122	-.032

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(i) $M = 0.95$; $\alpha \approx 10.2^{\circ}$

β, deg	ϕ, deg	Pressure coefficients for x/l of –													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0.2	P.L.	0.208		0.153	0.043	-0.002	-0.103		-0.235	-0.260	-0.391	-0.218	-0.048	-0.055	0.011
	80.0				.043				-.228		-.398	-.218			
	60.0	.208			.067	-.020	-.114			-.307		-.177	-.048		
	48.0			.183											
	43.0	.260			.075	.005	-.120		-.243		-.464	-.153		-.055	
	40.0			.224											
	32.0				.103										
	29.0						-.116								
	26.0					.016									
	20.0		0.287		.104		-.087	-0.209	-.215	-.445	-.428	-.124	-.026		
	00.0			.276	.073	.031		-.101	-.214	-.492	-.396	-.117	-.011	.002	.011
-4.1	P.L.	0.257		0.224	0.128	0.083	-0.020		-0.165	-0.219	-0.362	-0.335	-0.069	-0.040	-0.013
	80.0				.128				-.145		-.389	-.335			
	60.0	.257			.156	.067	-.030			-.265		-.297	-.069		
	48.0			.249											
	43.0	.273			.152	.075	-.050		-.193		-.552	-.239		-.040	
	40.0			.240											
	32.0				.142										
	29.0						-.054								
	26.0					.046									
	20.0		0.279		.118		-.046	-0.144	-.190	-.430	-.559	-.198	-.060		
	00.0			.269	.062	.021		-.116	-.236	-.520	-.463	-.180	-.106	-.029	-.013
4.5	00.0			0.275	0.053	0.014		-0.105	-0.241	-0.532	-0.439	-0.188	-0.104	-0.031	-0.021
	20.0		0.286		.068		-0.165	-.330	-.298	-.531	-.408	-.149	-.021		
	26.0					-.065									
	29.0						-.255								
	32.0				.025										
	40.0			.178											
	43.0	0.229			-.071	-.108	-.237		-.348		-.419	-.136		-.042	
	48.0			.086											
	60.0	.147			-.045	-.119	-.217			-.369		-.143	-.025		
	80.0				-.044				-.315		-.385	-.169			
	P.L.	.147		.073	-.044	-.085	-.180		-.302	-.306	-.391	-.169	-.025	-.042	-.021
-8.4	P.L.	0.283		0.275	0.198	0.157	0.050		-0.094	-0.175	-0.323	-0.529	-0.089	-0.066	-0.022
	80.0				.198				-.060		-.367	-.529			
	60.0	.283			.206	.118	.020			-.267		-.433	-.089		
	48.0			.265											
	43.0	.246			.152	.085	-.026		-.165		-.613	-.330		-.066	
	40.0			.203											
	32.0				.119										
	29.0						-.062								
	26.0					.014									
	20.0		0.250		.101		-.061	-0.140	-.229	-.473	-.727	-.305	-.064		
	00.0			.243	.017	-.017		-.138	-.364	-.591	-.649	-.369	-.063	-.025	-.022
8.9	00.0			0.247	-0.012	-0.043		-0.137	-0.347	-0.625	-0.689	-0.372	-0.049	-0.026	-0.024
	20.0		0.265		-.015		-0.303	-.536	-.462	-.709	-.481	-.326	-.146		
	26.0					-.206									
	29.0						-.498								
	32.0				-.125										
	40.0			.085											
	43.0	0.167			-.351	-.317	-.402		-.509		-.428	-.265		-.098	
	48.0			-.089											
	60.0	.042			-.221	-.271	-.349			-.476		-.180	-.012		
	80.0				-.151				-.404		-.393	-.155			
	P.L.	.042		-.042	-.151	-.186	-.270		-.387	-.386	-.402	-.155	-.012	-.098	-.024

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(j) M = 0.99; $\alpha = 0^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of –													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0	P.L.	0.375		0.265	0.115	0.055	-0.058		-0.170	-0.189	-0.271	-0.182	-0.151	-0.129	-0.043
	80.0				.115				-.208		-.274	-.182			
	60.0	.375			.138	.035	-.068			-.275		-.174	-.151		
	48.0			.302											
	43.0	.467			.160	.093	-.037		-.178		-.353	-.172		-.129	
	40.0			.367											
	32.0				.244										
	29.0						-.006								
	26.0					.169									
	20.0		0.481		.259		.069	-0.051	-.073	-.353	-.367	-.163	-.132		
	00.0			.455	.227	.205		.076	-.042	-.375	-.372	-.150	-.129	-.116	-.043
-4.3	P.L.	0.456		0.363	0.220	0.154	0.033		-0.095	-0.109	-0.240	-0.251	-0.176	-0.166	-0.065
	80.0				.220				-.102		-.254	-.251			
	60.0	.456			.255	.149	.045			-.161		-.242	-.176		
	48.0			.390											
	43.0	.500			.281	.198	.069		-.068		-.367	-.239		-.166	
	40.0			.404											
	32.0				.299										
	29.0						.096								
	26.0					.219									
	20.0		0.459		.278		.121	0.029	-.019	-.287	-.423	-.218	-.158		
	00.0			.440	.219	.194		.065	-.056	-.385	-.457	-.180	-.155	-.137	-.065
4.3	00.0			0.442	0.208	0.185		0.072	-0.064	-0.396	-0.436	-0.193	-0.158	-0.138	-0.065
	20.0		0.462		.213		-0.018	-.207	-.180	-.472	-.411	-.182	-.157		
	26.0					.068									
	29.0						-.199								
	32.0				.136										
	40.0			.284											
	43.0	0.393			-.063	-.092	-.211		-.329		-.375	-.168		-.149	
	48.0			.140											
	60.0	.256			-.035	-.125	-.233			-.410		-.163	-.157		
	80.0				-.005				-.318		-.303	-.168			
	P.L.	.256		.134	-.005	-.052	-.163		-.253	-.281	-.317	-.168	-.157	-.149	-.065
-8.7	P.L.	0.490		0.435	0.316	0.257	0.137		-0.004	-0.052	-0.194	-0.385	-0.216	-0.232	-0.095
	80.0				.316				.007		-.220	-.385			
	60.0	.490			.342	.243	.144			-.094		-.445	-.216		
	48.0			.435											
	43.0	.464			.328	.258	.143		.000		-.395	-.412		-.232	
	40.0			.383											
	32.0				.303										
	29.0						.137								
	26.0					.218									
	20.0		0.411		.264		.131	0.063	-.037	-.281	-.524	-.332	-.215		
	00.0			.394	.180	.162		.056	-.210	-.443	-.599	-.254	-.204	-.189	-.095
8.7	00.0			0.406	0.162	0.135		0.050	-0.131	-0.452	-0.606	-0.279	-0.210	-0.186	-0.095
	20.0		0.423		.138		-0.144	-.421	-.352	-.608	-.658	-.246	-.211		
	26.0					-.083									
	29.0						-.477								
	32.0				-.020										
	40.0			.170											
	43.0	0.287			-.388	-.378	-.390		-.542		-.435	-.246		-.192	
	48.0			-.095											
	60.0	.091			-.334	-.332	-.401			-.561		-.242	-.241		
	80.0				-.192				-.419		-.362	-.220			
	P.L.	.091		-.012	-.192	-.166	-.274		-.375	-.407	-.410	-.220	-.241	-.192	-.095

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(k) $M = 0.99$; $\alpha = 5.1^{\circ}$

β, deg	ϕ, deg	Pressure coefficients for x/l of –													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0	P.L.	0.289		0.212	0.098	0.044	-0.064		-0.197	-0.204	-0.314	-0.237	-0.160	-0.124	-0.005
	80.0				.098				-.212		-.318	-.237			
	60.0	.289			.117	.026	-.071			-.267		-.210	-.160		
	48.0			.248											
	43.0	.351			.133	.067	-.061		-.195		-.390	-.199		-.124	
	40.0			.305											
	32.0				.183										
	29.0						-.043								
	26.0					.102									
	20.0		0.381		.194		.004	-0.120	-.132	-.390	-.387	-.176	-.143		
	00.0			.368	.161	.130		-.000	-.115	-.416	-.369	-.169	-.140	-.102	-.005
-4.3	P.L.	0.383		0.315	0.195	0.138	0.024		-0.119	-0.149	-0.291	-0.334	-0.188	-0.150	-0.022
	80.0				.195				-.116		-.306	-.334			
	60.0	.383			.217	.122	.027			-.194		-.307	-.188		
	48.0			.338											
	43.0	.407			.230	.153	.030		-.116		-.438	-.286		-.150	
	40.0			.336											
	32.0				.235										
	29.0						.042								
	26.0					.144									
	20.0		0.393		.209		.056	-0.039	-.094	-.341	-.484	-.233	-.176		
	00.0			.375	.144	.119		-.012	-.139	-.433	-.466	-.201	-.183	-.130	-.022
4.3	00.0			0.365	0.137	0.109		0.000	-0.140	-0.443	-0.449	-0.214	-0.186	-0.131	-0.015
	20.0		0.378		.149		-0.092	-.270	-.232	-.503	-.400	-.195	-.190		
	26.0					.004									
	29.0						-.228								
	32.0				.084										
	40.0			.239											
	43.0	0.312			-.068	-.095	-.220		-.329		-.381	-.187		-.171	
	48.0			.112											
	60.0	.203			-.033	-.114	-.216			-.387		-.186	-.157		
	80.0				-.011				-.311		-.330	-.195			
	P.L.	.203		.110	-.011	-.057	-.160		-.275	-.282	-.337	-.195	-.157	-.171	-.015
-8.7	P.L.	0.397		0.372	0.279	0.227	0.117		-0.031	-0.098	-0.242	-0.494	-0.246	-0.183	-0.038
	80.0				.279				-.008		-.278	-.494			
	60.0	.397			.289	.198	.105			-.164		-.603	-.246		
	48.0			.364											
	43.0	.361			.255	.189	.077		-.060		-.491	-.455		-.183	
	40.0			.303											
	32.0				.223										
	29.0						.058								
	26.0					.128									
	20.0		0.341		.190		.049	-0.021	-.123	-.362	-.628	-.326	-.233		
	00.0			.330	.101	.080		-.029	-.304	-.509	-.674	-.313	-.227	-.141	-.038
8.7	00.0			0.332	0.085	0.059		-0.032	-0.243	-0.506	-0.682	-0.312	-0.231	-0.144	-0.045
	20.0		0.345		.070		-0.230	-.476	-.403	-.644	-.544	-.288	-.241		
	26.0					-.143									
	29.0						-.492								
	32.0				-.072										
	40.0			.137											
	43.0	0.220			-.383	-.346	-.401		-.509		-.421	-.293		-.199	
	48.0			-.094											
	60.0	.066			-.289	-.291	-.364			-.506		-.305	-.244		
	80.0				-.159				-.403		-.367	-.183			
	P.L.	.066		-.021	-.159	-.176	-.257		-.373	-.385	-.390	-.183	-.244	-.199	-.045

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(l) M = 0.99; α = 10.3°

β, deg	ϕ, deg	Pressure coefficients for x/l of —													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0.2	P.L.	0.250		0.198	0.089	.045	-.048		-0.190	-0.217	-0.343	-0.289	-0.165	-0.133	-0.003
	80.0				.089				-.186		-.352	-.289			
	60.0	.250			.110	.032	-.059			-.261		-.253	-.165		
	48.0			.228											
	43.0	.301			.121	.054	-.068		-.200		-.432	-.227		-.133	
	40.0			.263											
	32.0				.143										
	29.0						-.065								
	26.0					.058									
	20.0		0.326		.142		-.037	-0.151	-.169	-.393	-.399	-.192	-.145		
	00.0			.315	.109	.073		-.055	-.174	-.446	-.367	-.181	-.132	-.088	-.003
-4.1	P.L.	0.290		0.259	0.163	0.123	0.024		-0.123	-0.181	-0.327	-0.396	-0.198	-0.137	-0.040
	80.0				.163				-.106		-.352	-.396			
	60.0	.290			.191	.104	.013			-.228		-.365	-.198		
	48.0			.283											
	43.0	.304			.186	.112	-.004		-.151		-.516	-.307		-.137	
	40.0			.275											
	32.0				.176										
	29.0						-.008								
	26.0					.084									
	20.0		0.309		.150		.003	-0.098	-.156	-.387	-.535	-.257	-.188		
	00.0			.301	.094	.059		-.068	-.202	-.477	-.454	-.234	-.234	-.119	-.040
4.5	00.0			0.307	0.087	0.053		-0.060	-0.198	-0.478	-0.411	-0.237	-0.232	-0.115	-0.038
	20.0		0.317		.102		-0.117	-.274	-.249	-.479	-.377	-.202	-.160		
	26.0					-.025									
	29.0						-.203								
	32.0				.060										
	40.0			.213											
	43.0	0.262			-.033	-.066	-.184		-.298		-.385	-.199		-.136	
	48.0			.122											
	60.0	.181			-.009	-.073	-.164			-.336		-.207	-.154		
	80.0				-.004				-.275		-.353	-.237			
	P.L.	.181		.114	-.004	-.042	-.129		-.262	-.268	-.353	-.237	-.154	-.136	-.038
-8.5	P.L.	0.314		0.315	0.240	0.200	0.098		-0.047	-0.129	-0.273	-0.549	-0.253	-0.170	-0.044
	80.0				.240				-.016		-.318	-.549			
	60.0	.314			.246	.161	.069			-.227		-.642	-.253		
	48.0			.302											
	43.0	.274			.185	.124	.016		-.114		-.573	-.417		-.170	
	40.0			.235											
	32.0				.152										
	29.0						-.024								
	26.0					.052									
	20.0		0.280		.132		-.021	-0.098	-.188	-.433	-.711	-.368	-.209		
	00.0			.274	.046	.018		-.097	-.356	-.559	-.676	-.437	-.201	-.127	-.044
8.9	00.0			0.280	0.023	-0.005		-0.096	-0.307	-0.563	-0.650	-0.398	-0.201	-0.127	-0.043
	20.0		0.297		.019		-0.257	-.476	-.411	-.634	-.460	-.349	-.322		
	26.0					-.172									
	29.0						-.442								
	32.0				-.093										
	40.0			.124											
	43.0	0.200			-.312	-.280	-.348		-.454		-.398	-.303		-.197	
	48.0			-.048											
	60.0	.081			-.197	-.224	-.295			-.432		-.226	-.166		
	80.0				-.123				-.353		-.363	-.205			
	P.L.	.081		-.002	-.123	-.146	-.221		-.339	-.349	-.369	-.205	-.166	-.197	-.043

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(m) M = 1.02; $\alpha = 0^{\circ}$

β, deg	∅, deg	Pressure coefficients for x/l of −													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0	P.L.	0.409		0.305	0.155	0.098	-0.012		-0.127	-0.149	-0.225	-0.174	-0.138	-0.127	-0.064
	80.0				.155				-.161		-.233	-.174			
	60.0	.409			.176	.083	-.019			-.224		-.163	-.138		
	48.0			.337											
	43.0	.496			.201	.134	.006		-.130		-.311	-.159		-.127	
	40.0			.396											
	32.0				.276										
	29.0						.041								
	26.0					.205									
	20.0		0.503		.292		.108	-0.009	-.031	-.297	-.335	-.146	-.120		
	00.0			.480	.258	.237		.110	-.005	-.330	-.352	-.135	-.117	-.113	-.064
-4.3	P.L.	0.491		0.401	0.258	0.194	0.079		-0.056	-0.068	-0.195	-0.246	-0.164	-0.161	-0.085
	80.0				.258				-.064		-.208	-.246			
	60.0	.491			.289	.192	.094			-.114		-.235	-.164		
	48.0			.425											
	43.0	.529			.316	.235	.112		-.030		-.323	-.230		-.161	
	40.0			.434											
	32.0				.332										
	29.0						.136								
	26.0					.255									
	20.0		0.486		.307		.160	0.073	.014	-.244	-.388	-.201	-.144		
	00.0			.466	.251	.230		.105	-.027	-.347	-.442	-.164	-.142	-.137	-.085
4.3	00.0			0.470	0.241	0.222		0.111	-0.021	-0.343	-0.390	-0.171	-0.137	-0.127	-0.076
	20.0		0.490		.248		0.031	-.147	-.126	-.397	-.368	-.159	-.137		
	26.0					.108									
	29.0						-.135								
	32.0				.169										
	40.0			.319											
	43.0	0.424			-.005	-.040	-.152		-.267		-.330	-.146		-.142	
	48.0			.183											
	60.0	.296			.012	-.072	-.164			-.352		-.140	-.136		
	80.0				.042				-.268		-.262	-.152			
	P.L.	.296		.178	.042	-.013	-.112		-.212	-.236	-.271	-.152	-.136	-.142	-.076
-8.7	P.L.	0.519		0.467	0.347	0.290	0.175		0.029	-0.014	-0.154	-0.365	-0.208	-0.227	-0.127
	80.0				.347				.042		-.183	-.365			
	60.0	.519			.371	.276	.181			-.060		-.436	-.208		
	48.0			.466											
	43.0	.495			.358	.290	.178		.033		-.354	-.447		-.227	
	40.0			.414											
	32.0				.334										
	29.0						.173								
	26.0					.253									
	20.0		0.438		.292		.167	0.102	-.006	-.247	-.487	-.318	-.203		
	00.0			.421	.211	.196		.096	-.183	-.408	-.578	-.239	-.190	-.190	-.127
8.7	00.0			0.434	0.194	0.166		0.081	-0.098	-0.396	-0.542	-0.253	-0.191	-0.176	-0.116
	20.0		0.454		.172		-0.105	-.365	-.280	-.536	-.601	-.219	-.191		
	26.0					-.048									
	29.0						-.427								
	32.0				.019										
	40.0			.208											
	43.0	0.323			-.318	-.320	-.358		-.471		-.394	-.218		-.186	
	48.0			-.046											
	60.0	.135			-.281	-.293	-.321			-.505		-.214	-.219		
	80.0				-.152				-.370		-.324	-.201			
	P.L.	.135		.034	-.152	-.151	-.219		-.328	-.361	-.364	-.201	-.219	-.186	-.116

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(n) M = 1.02; α = 5.1°

β, deg	∅, deg	Pressure coefficients for x/l of –													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0	P.L.	0.326		0.256	0.140	0.089	-0.015		-0.153	-0.167	-0.270	-0.234	-0.150	-0.125	-0.054
	80.0				.140				-.166		-.278	-.234			
	60.0	.326			.156	.074	-.019			-.224		-.202	-.150		
	48.0			.285											
	43.0	.384			.174	.109	-.017		-.150		-.355	-.188		-.125	
	40.0			.336											
	32.0				.218										
	29.0						.000								
	26.0					.141									
	20.0		0.410		.226		.045	-0.071	-.089	-.337	-.364	-.161	-.132		
	00.0			.399	.191	.165		.038	-.079	-.372	-.357	-.154	-.131	-.105	-.054
-4.3	P.L.	0.425		0.354	0.232	0.176	0.068		-0.082	-0.111	-0.249	-0.332	-0.179	-0.152	-0.076
	80.0				.232				-.082		-.266	-.332			
	60.0	.425			.250	.160	.070			-.154		-.307	-.179		
	48.0			.374											
	43.0	.448			.262	.187	.072		-.082		-.396	-.278		-.152	
	40.0			.368											
	32.0				.265										
	29.0						.081								
	26.0					.178									
	20.0		0.422		.238		.096	-0.003	-.063	-.299	-.449	-.217	-.166		
	00.0			.405	.175	.154		.024	-.108	-.393	-.448	-.185	-.173	-.130	-.076
4.3	00.0			0.397	0.172	0.149		0.042	-0.098	-0.390	-0.401	-0.190	-0.167	-0.126	-0.068
	20.0		0.411		.183		-0.045	-.212	-.180	-.440	-.362	-.168	-.171		
	26.0					.044									
	29.0						-.171								
	32.0				.119										
	40.0			.275											
	43.0	0.344			-.022	-.050	-.166		-.276		-.340	-.160		-.168	
	48.0			.153											
	60.0	.239			.008	-.067	-.160			-.338		-.158	-.137		
	80.0				.031				-.268		-.288	-.175			
	P.L.	.239		.151	.031	-.017	-.111		-.232	-.241	-.294	-.175	-.137	-.168	-.068
-8.7	P.L.	0.428		0.406	0.312	0.263	0.155		0.009	-0.057	-0.201	-0.449	-0.227	-0.179	-0.097
	80.0				.312				.027		-.238	-.449			
	60.0	.428			.322	.232	.143			-.124		-.559	-.227		
	48.0			.397											
	43.0	.395			.286	.224	.117		-.020		-.441	-.475		-.179	
	40.0			.336											
	32.0				.259										
	29.0						.097								
	26.0					.166									
	20.0		0.374		.224		.091	0.022	-.082	-.318	-.576	-.304	-.216		
	00.0			.362	.138	.120		.014	-.264	-.457	-.622	-.291	-.212	-.137	-.097
8.7	00.0			0.362	0.119	0.091		0.010	-0.207	-0.458	-0.621	-0.289	-0.216	-0.142	-0.093
	20.0		0.377		.104		-0.181	-.418	-.360	-.584	-.513	-.260	-.226		
	26.0					-.106									
	29.0						-.433								
	32.0				-.036										
	40.0			.174											
	43.0	0.253			-.338	-.303	-.351		-.463		-.384	-.264		-.191	
	48.0			-.052											
	60.0	.104			-.258	-.237	-.318			-.461		-.276	-.237		
	80.0				-.133				-.359		-.330	-.165			
	P.L.	.104		.019	-.133	-.129	-.216		-.329	-.345	-.351	-.165	-.237	-.191	-.093

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(o) M = 1.02; α = 10.3°

β, deg	∅, deg	Pressure coefficients for x/l of −													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0.2	P.L.	0.288		0.228	0.115	0.075	-0.020		-0.164	-0.186	-0.306	-0.258	-0.151	-0.133	-0.039
	80.0				.115				-.165		-.316	-.258			
	60.0	.288			.138	.055	-.036			-.235		-.222	-.151		
	48.0			.262											
	43.0	.343			.142	.080	-.040		-.177		-.382	-.201		-.133	
	40.0			.298											
	32.0				.173										
	29.0						-.039								
	26.0					.090									
	20.0		0.368		.170		-.007	-0.126	-.144	-.374	-.360	-.169	-.132		
	00.0			.356	.135	.104		-.019	-.139	-.413	-.337	-.161	-.122	-.088	-.039
-4.1	P.L.	0.318		0.286	0.191	0.152	0.055		-0.088	-0.145	-0.281	-0.368	-0.179	-0.133	-0.066
	80.0				.191				-.074		-.308	-.368			
	60.0	.318			.221	.136	.046			-.191		-.330	-.179		
	48.0			.313											
	43.0	.333			.217	.144	.032		-.117		-.456	-.280		-.133	
	40.0			.305											
	32.0				.207										
	29.0						.026								
	26.0					.119									
	20.0		0.340		.184		.031	-0.061	-.119	-.343	-.480	-.230	-.168		
	00.0			.331	.130	.095		-.027	-.159	-.426	-.407	-.206	-.214	-.111	-.066
4.5	00.0			0.334	0.117	0.084		-0.026	-0.164	-0.445	-0.405	-0.226	-0.221	-0.115	-0.072
	20.0		0.343		.128		-0.089	-.250	-.224	-.462	-.348	-.184	-.157		
	26.0					.003									
	29.0						-.182								
	32.0				.086										
	40.0			.241											
	43.0	0.288			-.019	-.045	-.155		-.270		-.346	-.178		-.135	
	48.0			.148											
	60.0	.208			.016	-.054	-.140			-.313		-.181	-.139		
	80.0				.019				-.244		-.311	-.208			
	P.L.	.208		.138	.019	-.014	-.101		-.227	-.238	-.314	-.208	-.139	-.135	-.072
-8.4	P.L.	0.339		0.339	0.265	0.226	0.128		-0.018	-0.091	-0.242	-0.491	-0.234	-0.168	-0.079
	80.0				.265				.010		-.285	-.491			
	60.0	.339			.274	.189	.099			-.186		-.589	-.234		
	48.0			.332											
	43.0	.307			.218	.156	.051		-.081		-.520	-.390		-.168	
	40.0			.268											
	32.0				.185										
	29.0						.011								
	26.0					.088									
	20.0		0.310		.164		.018	-0.062	-.146	-.381	-.646	-.337	-.192		
	00.0			.306	.083	.056		-.059	-.310	-.497	-.607	-.397	-.187	-.123	-.079
8.9	00.0			0.311	0.056	0.029		-0.060	-0.272	-0.519	-0.646	-0.388	-0.187	-0.126	-0.079
	20.0		0.327		.052		-0.222	-.442	-.371	-.601	-.430	-.321	-.322		
	26.0					-.140									
	29.0						-.412								
	32.0				-.061										
	40.0			-.060											
	43.0	0.230			-.286	-.251	-.310		-.411		-.363	-.277		-.197	
	48.0			-.013											
	60.0	.114			-.172	-.195	-.259			-.401		-.204	-.156		
	80.0				-.094				-.314		-.327				
	P.L.	.114		-.112	-.094	-.182	-.300		-.313	-.331			-.156	-.197	-.079

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(p) $M = 1.08$; $\alpha = 0^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of –													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0	P.L.	0.449		0.332	0.176	0.131	0.022		-0.087	-0.110	-0.165	-0.116	-0.086	-0.077	-0.014
	80.0				.176				-.129		-.171	-.116			
	60.0	.449			.197	.116	.011			-.184		-.111	-.086		
	48.0			.369											
	43.0	.530			.219	.167	.045		-.081		-.249	-.108		-.077	
	40.0			.431											
	32.0				.300										
	29.0						.080								
	26.0					.246									
	20.0		0.537		.317		.152	0.032	.017	-.246	-.280	-.101	-.071		
	00.0			.513	.286	.276		.158	.044	-.261	-.296	-.088	-.069	-.064	-.014
-4.4	P.L.	0.528		0.426	0.278	0.224	0.109		-0.016	-0.039	-0.135	-0.192	-0.113	-0.106	-0.033
	80.0				.278				-.034		-.147	-.192			
	60.0	.528			.312	.222	.126			-.094		-.179	-.113		
	48.0			.457											
	43.0	.565			.338	.268	.153		.000		-.252	-.177		-.106	
	40.0			.468											
	32.0				.358										
	29.0						.180								
	26.0					.296									
	20.0		0.521		.335		.205	0.117	.046	-.197	-.316	-.157	-.094		
	00.0			.502	.282	.269		.152	.015	-.275	-.361	-.121	-.090	-.082	-.033
4.4	00.0			0.505	0.268	0.252		0.155	0.012	-0.283	-0.360	-0.124	-0.094	-0.089	-0.031
	20.0		0.526		.270		0.065	-.107	-.094	-.355	-.339	-.113	-.094		
	26.0					.141									
	29.0						-.105								
	32.0				.193										
	40.0			.356											
	43.0	0.461			.002	-.026	-.120		-.228		-.288	-.099		-.101	
	48.0			.217											
	60.0	.331			.001	-.056	-.146			-.318		-.092	-.091		
	80.0				.036				-.237		-.210	-.094			
	P.L.	.331		.211	.036	.011	-.081		-.178	-.195	-.220	-.094	-.091	-.101	-.031
-8.7	P.L.	0.550		0.492	0.371	0.320	0.206		0.069	0.030	-0.097	-0.274	-0.141	-0.154	-0.027
	80.0				.371				.073		-.122	-.274			
	60.0	.550			.398	.309	.214			-.023		-.324	-.141		
	48.0			.499											
	43.0	.533			.390	.325	.219		.077		-.275	-.376		-.154	
	40.0			.459											
	32.0				.372										
	29.0						.217								
	26.0					.299									
	20.0		0.485		.332		.219	0.152	.050	-.193	-.394	-.251	-.132		
	00.0			.469	.255	.246		.149	-.112	-.326	-.465	-.180	-.127	-.111	-.027
8.7	00.0			0.482	0.241	0.209		0.123	-0.084	-0.336	-0.497	-0.203	-0.144	-0.124	-0.024
	20.0		0.501		.219		-0.068	-.314	-.263	-.491	-.577	-.172	-.144		
	26.0					-.002									
	29.0						-.402								
	32.0				.066										
	40.0			.258											
	43.0	0.373			-.278	-.299	-.345		-.444		-.344	-.174		-.127	
	48.0			.001											
	60.0	.184			-.247	-.278	-.331			-.474		-.180	-.193		
	80.0				-.130				-.332		-.270	-.139			
	P.L.	.184		.077	-.130	-.135	-.197		-.290	-.314	-.307	-.139	-.193	-.127	-.024

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(q) M = 1.08; $\alpha = 5.1^\circ$

β, deg	∅, deg	Pressure coefficients for x/l of –													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0	P.L.	0.339		0.272	0.160	0.126	0.028		-0.101	-0.121	-0.208	-0.174	-0.093	-0.075	-0.004
	80.0				.160				-.122		-.212	-.174			
	60.0	.339			.180	.110	.018			-.183		-.150	-.093		
	48.0			.307											
	43.0	.401			.194	.147	.031		-.099		-.283	-.141		-.075	
	40.0			.367											
	32.0				.244										
	29.0						.045								
	26.0					.185									
	20.0		0.436		.256		.096	-0.021	-.037	-.282	-.298	-.121	-.080		
	00.0			.427	.226	.210		.098	-.018	-.294	-.297	-.116	-.076	-.054	-.004
-4.4	P.L.	0.425		0.365	0.255	0.213	0.109		-0.032	-0.063	-0.184	-0.268	-0.117	-0.091	-0.001
	80.0				.255				-.036		-.197	-.268			
	60.0	.425			.279	.200	.111			-.109		-.239	-.117		
	48.0			.399											
	43.0	.454			.292	.229	.123		-.033		-.312	-.218		-.091	
	40.0			.401											
	32.0				.301										
	29.0						.134								
	26.0					.229									
	20.0		0.447		.275		.151	0.051	-.011	-.244	-.363	-.169	-.105		
	00.0			.435	.216	.204		.088	-.045	-.310	-.360	-.141	-.113	-.072	-.001
4.4	00.0			0.429	0.201	0.186		0.088	-0.046	-0.315	-0.359	-0.148	-0.117	-0.082	-0.010
	20.0		0.439		.209		0.001	-.157	-.127	-.374	-.316	-.124	-.121		
	26.0					.083									
	29.0						-.125								
	32.0				.141										
	40.0			.315											
	43.0	0.371			-.008	-.018	-.114		-.215		-.283	-.114		-.118	
	48.0			.190											
	60.0	.267			.011	-.036	-.108			-.281		-.112	-.086		
	80.0				.041				-.210		-.229	-.121			
	P.L.	.267		.183	.041	.016	-.059		-.174	-.185	-.233	-.121	-.086	-.118	.010
-8.7	P.L.	0.454		0.438	0.345	0.300	0.198		0.056	-0.001	-0.144	-0.375	-0.169	-0.085	-0.021
	80.0				.345				.069		-.180	-.375			
	60.0	.454			.358	.275	.189			-.073		-.476	-.169		
	48.0			.432											
	43.0	.424			.324	.265	.166		.033		-.367	-.482		-.085	
	40.0			.378											
	32.0				.297										
	29.0						.145								
	26.0					.211									
	20.0		0.410		.260		.142	0.066	-.026	-.264	-.497	-.264	-.162		
	00.0			.401	.174	.163		.059	-.214	-.384	-.538	-.252	-.159	-.052	-.021
8.7	00.0			0.403	0.162	0.126		0.045	-0.175	-0.387	-0.554	-0.248	-0.178	-0.057	-0.020
	20.0		0.415		.147		-0.159	-.371	-.302	-.522	-.473	-.213	-.173		
	26.0					-.075									
	29.0						-.423								
	32.0				.010										
	40.0			.226											
	43.0	0.294			-.291	-.293	-.314		-.408		-.323	-.217		-.111	
	48.0			.001											
	60.0	.148			-.227	-.237	-.276			-.397		-.225	-.183		
	80.0				-.113				-.299		-.271	-.101			
	P.L.	.148		.067	-.113	-.115	-.171		-.269	-.285	-.282	-.101	-.183	-.111	-.020

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(r) M = 1.08; α = 10.3°

β, deg	ϕ, deg	Pressure coefficient for x/l of −													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0.2	P.L.	0.295		0.257	0.167	0.132	0.051		-0.091	-0.125	-0.236	-0.236	-0.101	-0.074	0.053
	80.0				.167				-.095		-.248	-.236			
	60.0	.295			.189	.123	.040			-.170		-.195	-.101		
	48.0			.291											
	43.0	.345			.199	.142	.032		-.102		-.330	-.166		-.074	
	40.0			.325											
	32.0				.222										
	29.0						.037								
	26.0					.150									
	20.0		0.382		.219		.064	-0.044	-.071	-.292	-.318	-.133	-.082		
	00.0			.375	.186	.161		.049	-.074	-.338	-.295	-.122	-.070	-.035	.053
-4.1	P.L.	0.329		0.319	0.241	0.207	0.118		-0.030	-0.083	-0.215	-0.370	-0.133	-0.077	0.012
	80.0				.241				-.019		-.241	-.370			
	60.0	.329			.271	.195	.109			-.134		-.342	-.133		
	48.0			.348											
	43.0	.345			.264	.198	.091		-.057		-.401	-.260		-.077	
	40.0			.339											
	32.0				.254										
	29.0						.083								
	26.0					.172									
	20.0		0.359		.228		.095	0.005	-.069	-.282	-.444	-.203	-.119		
	00.0			.357	.176	.146		.034	-.121	-.371	-.399	-.188	-.164	-.058	.012
4.6	00.0			0.362	0.159	0.139		0.040	-0.099	-0.361	-0.333	-0.170	-0.168	-0.048	0.008
	20.0		0.365		.172		-0.012	-.160	-.144	-.365	-.294	-.131	-.094		
	26.0					.062									
	29.0						-.096								
	32.0				.125										
	40.0			.279											
	43.0	0.305			.032	.020	-.076		-.192		-.290	-.123		-.058	
	48.0			.185											
	60.0	.227			.058	.016	-.056			-.243		-.132	-.085		
	80.0				.065				-.172		-.249	-.162			
	P.L.	.227		.171	.065	.047	-.024		-.156	-.175	-.251	-.162	-.085	-.058	.008
-8.4	P.L.	0.353		0.366	0.303	0.267	0.177		0.036	-0.030	-0.186	-0.426	-0.162	-0.086	-0.010
	80.0				.303				.058		-.228	-.426			
	60.0	.353			.316	.234	.154			-.124		-.565	-.162		
	48.0			.367											
	43.0	.325			.259	.199	.109		-.022		-.451	-.360		-.086	
	40.0			.306											
	32.0				.227										
	29.0						.063								
	26.0					.133									
	20.0		0.339		.204		.070	-0.006	-.085	-.329	-.580	-.302	-.116		
	00.0			.337	.122	.101		-.003	-.270	-.435	-.572	-.373	-.107	-.047	-.010
8.9	00.0			0.348	0.106	0.072		-0.007	-0.221	-0.432	-0.549	-0.336	-0.107	-0.053	-0.009
	20.0		0.358		.099		-0.162	-.367	-.302	-.499	-.361	-.257	-.241		
	26.0					-.097									
	29.0						-.344								
	32.0				-.011										
	40.0			.210											
	43.0	0.256			-.232	-.209	-.243		-.332		-.296	-.219		-.119	
	48.0			.040											
	60.0	.147			-.145	-.144	-.195			-.323		-.147	-.063		
	80.0				-.063				-.246		-.259	-.127			
	P.L.	.147		.078	-.063	-.066	-.122		-.229	-.242	-.258	-.127	-.063	-.119	-.009

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(s) M = 1.13; $\alpha = 0^\circ$

β, deg	ø, deg	Pressure coefficients for x/l of –													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0	P.L.	0.472		0.352	0.178	0.136	0.055		-0.057	-0.086	-0.139	-0.149	-0.091	-0.087	-0.027
	80.0				.178				-.097		-.149	-.149			
	60.0	.472			.197	.131	.054			-.155		-.140	-.091		
	48.0			.394											
	43.0	.556			.235	.185	.075		-.048		-.233	-.136		-.087	
	40.0			.459											
	32.0				.312										
	29.0						.105								
	26.0					.264									
	20.0		0.566		.332		.169	0.062	.043	-.208	-.281	-.120	-.072		
	00.0			.546	.319	.294		.184	.062	-.218	-.311	-.105	-.068	-.078	-.027
-4.3	P.L.	0.556		0.448	0.293	0.247	0.152		0.025	-0.017	-0.095	-0.241	-0.124	-0.115	-0.053
	80.0				.293				.011		-.114	-.241			
	60.0	.556			.319	.258	.171			-.068		-.244	-.124		
	48.0			.485											
	43.0	.581			.357	.298	.192		.039		-.229	-.252		-.115	
	40.0			.492											
	32.0				.374										
	29.0						.216								
	26.0					.324									
	20.0		0.554		.353		.232	0.149	.069	-.171	-.310	-.197	-.101		
	00.0			.535	.319	.293		.180	.005	-.252	-.380	-.149	-.099	-.104	-.053
4.3	00.0			0.542	0.302	0.278		0.175	0.040	-0.233	-0.342	-0.131	-0.098	-0.091	-0.038
	20.0		0.562		.294		0.073	-.079	-.060	-.300	-.324	-.122	-.098		
	26.0					.164									
	29.0						-.073								
	32.0				.218										
	40.0			.389											
	43.0	0.496			.038	-.002	-.080		-.191		-.265	-.113		-.103	
	48.0			.252											
	60.0	.363			.020	-.040	-.101			-.280		-.108	-.097		
	80.0				.050				-.206		-.187	-.110			
	P.L.	.363		.242	.050	.019	-.049		-.150	-.165	-.193	-.110	-.097	-.103	-.038
-8.8	P.L.	0.522		0.487	0.375	0.331	0.232		0.102	0.058	-0.064	-0.269	-0.157	-0.173	-0.079
	80.0				.375				.107		-.094	-.269			
	60.0	.522			.396	.334	.250			-.009		-.336	-.157		
	48.0			.508											
	43.0	.506			.399	.354	.257		.117		-.250	-.411		-.173	
	40.0			.469											
	32.0				.388										
	29.0						.251								
	26.0					.328									
	20.0		0.500		.349		.248	0.178	.083	-.180	-.382	-.290	-.146		
	00.0			.493	.301	.269		.170	-.104	-.306	-.456	-.195	-.138	-.147	-.079
8.8	00.0			0.509	0.274	0.237		0.147	-0.061	-0.286	-0.445	-0.213	-0.149	-0.132	-0.071
	20.0		0.528		.247		-0.037	-.256	-.216	-.426	-.511	-.181	-.150		
	26.0					.026									
	29.0						-.343								
	32.0				.100										
	40.0			.293											
	43.0	0.401			-.218	-.250	-.296		-.389		-.342	-.182		-.140	
	48.0			.038											
	60.0	.217			-.198	-.228	-.273			-.442		-.188	-.208		
	80.0				-.093				-.306		-.262	-.158			
	P.L.	.217		.108	-.093	-.105	-.160		-.260	-.290	-.295	-.158	-.208	-.140	-.071

TABLE V.- Continued

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

(t) M = 1.13; $\alpha = 5.1^\circ$

β, deg	ϕ, deg	Pressure coefficients for x/l of –													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0	P.L.	0.339		0.288	0.168	0.132	0.060		-0.066	-0.100	-0.175	-0.215	-0.102	-0.090	-0.024
	80.0				.168				-.087		-.185	-.215			
	60.0	.339			.185	.126	.057			-.155		-.188	-.102		
	48.0			.325											
	43.0	.397			.206	.156	.059		-.071		-.273	-.174		-.090	
	40.0			.377											
	32.0				.250										
	29.0						.075								
	26.0					.193									
	20.0		0.439		.256		.117	0.011	-.020	-.250	-.304	-.132	-.085		
	00.0			.434	.221	.212		.114	-.019	-.281	-.321	-.124	-.083	-.073	-.024
-4.4	P.L.	0.386		0.364	0.271	0.234	0.148		0.009	-0.035	-0.142	-0.318	-0.136	-0.116	-0.048
	80.0				.271				.005		-.164	-.318			
	60.0	.386			.298	.231	.149			-.085		-.329	-.136		
	48.0			.397											
	43.0	.406			.307	.248	.144		.002		-.307	-.326		-.116	
	40.0			.396											
	32.0				.304										
	29.0						.145								
	26.0					.236									
	20.0		0.429		.276		.155	0.072	-.002	-.231	-.390	-.200	-.128		
	00.0			.426	.215	.201		.097	-.082	-.319	-.430	-.173	-.135	-.094	-.048
4.4	00.0			0.441	0.213	0.193		0.103	-0.035	-0.282	-0.352	-0.145	-0.114	-0.094	-0.031
	20.0		0.447		.221		.023	-.130	-.110	-.334	-.309	-.125	-.117		
	26.0					.090									
	29.0						-.095								
	32.0				.156										
	40.0			.332											
	43.0	0.368			.009	-.019	-.089		-.192		-.265	-.117		-.126	
	48.0			.210											
	60.0	.267			.014	-.031	-.085			-.255		-.114	-.087		
	80.0				.042				-.190		-.204	-.126			
	P.L.	.267		.198	.042	.014	-.042		-.151	-.166	-.205	-.126	-.087	-.126	-.031
8.7	00.0			0.424	0.187	0.149		0.065	-0.159	-0.347	-0.515	-0.270	-0.195	-0.103	-0.052
	20.0		0.434		.173		-0.128	-.332	-.284	-.478	-.503	-.227	-.185		
	26.0					-.055									
	29.0						-.390								
	32.0				.041										
	40.0			.259											
	43.0	0.311			-.246	-.272	-.293		-.384		-.314	-.228		-.150	
	48.0			.040											
	60.0	.171			-.197	-.223	-.252			-.378		-.227	-.183		
	80.0				-.093				-.282		-.256	-.104			
	P.L.	.171		.097	-.093	-.109	-.159		-.251	-.267	-.262	-.104	-.183	-.150	-.052

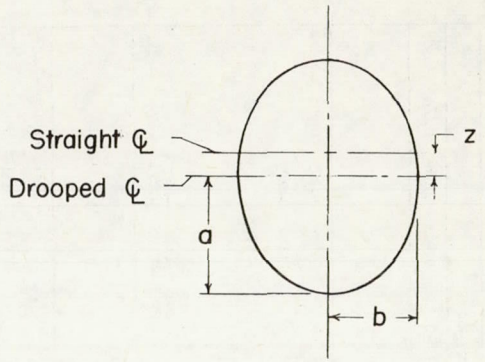
TABLE V.- Concluded

PRESSURE COEFFICIENTS FOR REARWARD-LOCATED SMALL FLAT-WINDSHIELD CANOPY 4

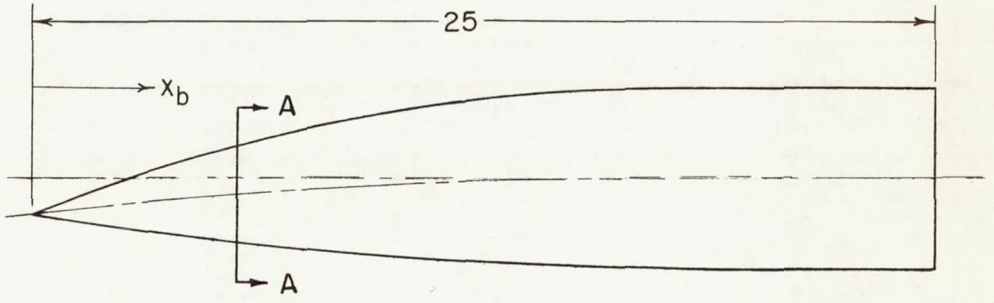
(u) $M = 1.13$; $\alpha = 10.3^\circ$

α, deg	ϕ, deg	Pressure coefficients for x/l of —													
		-0.011	0	0.004	0.052	0.102	0.142	0.149	0.193	0.249	0.324	0.467	0.662	0.804	0.985
0.2	P.L.	0.254		0.225	0.122	0.102	0.043		-0.080	-0.117	-0.206	-0.227	-0.105	-0.103	-0.011
	80.0				.122				-.087		-.219	-.227			
	60.0	.254			.148	.097	.038			-.161		-.185	-.105		
	48.0			.261											
	43.0	.305			.160	.114	.031		-.094		-.298	-.154		-.103	
	40.0			.303											
	32.0				.186										
	29.0						.033								
	26.0					.124									
	20.0		0.352		.187		.063	-0.037	-.066	-.271	-.292	-.119	-.085		
	00.0			.349	.156	.136		.050	-.071	-.315	-.275	-.110	-.076	-.056	-.011
-4.1	P.L.	0.282		0.281	0.209	0.191	0.117		-0.018	-0.068	-0.177	-0.368	-0.131	-0.100	-0.034
	80.0				.209				-.014		-.203	-.368			
	60.0	.282			.248	.185	.110			-.117		-.333	-.131		
	48.0			.316											
	43.0	.303			.245	.187	.093		-.038		-.355	-.253		-.100	
	40.0			.314											
	32.0				.236										
	29.0						.082								
	26.0					.165									
	20.0		0.337		.210		.094	0.012	-.051	-.258	-.402	-.189	-.119		
	00.0			.337	.154	.133		.039	-.101	-.336	-.364	-.168	-.166	-.079	-.034
4.6	00.0			0.347	0.146	0.120		0.040	-0.090	-0.334	-0.325	-0.164	-0.175	-0.079	-0.035
	20.0		0.349		.156		-0.016	-.158	-.133	-.340	-.282	-.124	-.101		
	26.0					.042									
	29.0						-.098								
	32.0				.109										
	40.0			.265											
	43.0	0.278			.007	-.009	-.079		-.175		-.270	-.117		-.101	
	48.0			.173											
	60.0	.201			.025	-.012	-.062			-.221		-.123	-.090		
	80.0				.033				-.157		-.225	-.153			
	P.L.	.201		.153	.033	.017	-.033		-.137	-.154	-.225	-.153	-.090	-.101	-.035
-8.5	P.L.	0.279		0.318	0.290	0.272	0.187		0.049	-0.009	-0.154	-0.386	-0.190	-0.130	-0.037
	80.0				.290				.068		-.193	-.386			
	60.0	.279			.316	.245	.169			-.095		-.506	-.190		
	48.0			.329											
	43.0	.257			.266	.211	.126		-.007		-.412	-.391		-.130	
	40.0			.279											
	32.0				.238										
	29.0						.082								
	26.0					.149									
	20.0		0.309		.212		.089	0.013	-.060	-.314	-.527	-.288	-.146		
	00.0			.314	.130	.111		.019	-.246	-.398	-.499	-.354	-.136	-.090	-.037
8.9	00.0			0.335	0.122	0.078		0.000	-0.220	-0.406	-0.513	-0.356	-0.148	-0.095	-0.038
	20.0		0.337		.111		-.153	-.348	-.287	-.472	-.361	-.263	-.259		
	26.0					-.094									
	29.0						-.342								
	32.0				.003										
	40.0			.209											
	43.0	0.233			-.210	-.219	-.233		-.321		-.290	-.224		-.151	
	48.0			.045											
	60.0	.129			-.139	-.155	-.187			-.309		-.151	-.118		
	80.0				-.067				-.234		-.247	-.130			
	P.L.	.129		.072	-.067	-.078	-.120		-.214	-.226	-.242	-.130	-.118	-.151	-.038

BODY DIMENSIONS			
x_b	a	b	z
0	0	0	1.000
.250	.073	.058	.973
.500	.144	.115	.945
.750	.214	.171	.917
1.000	.283	.226	.896
1.250	.351	.281	.863
1.500	.418	.334	.837
1.750	.483	.386	.811
2.000	.548	.438	.785
2.250	.611	.489	.760
2.500	.674	.539	.735
3.750	.969	.775	.617
5.000	1.237	.990	.510
6.250	1.479	1.183	.413
7.500	1.695	1.356	.326
8.750	1.885	1.508	.250
10.000	2.049	1.639	.183
11.250	2.187	1.750	.127
12.500	2.300	1.840	.081
13.750	2.388	1.910	.046
15.000	2.450	1.960	.020
16.250	2.480	1.990	.005
17.500	2.500	2.000	.000
	↓	↓	↓
25.000	2.500	2.000	.000



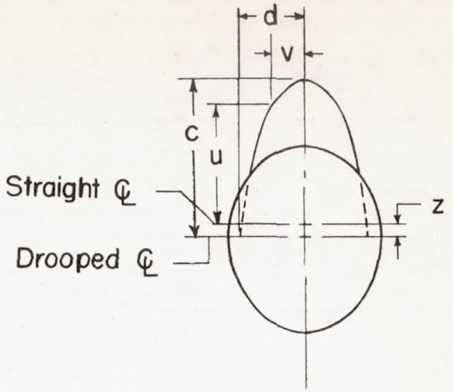
Section A-A



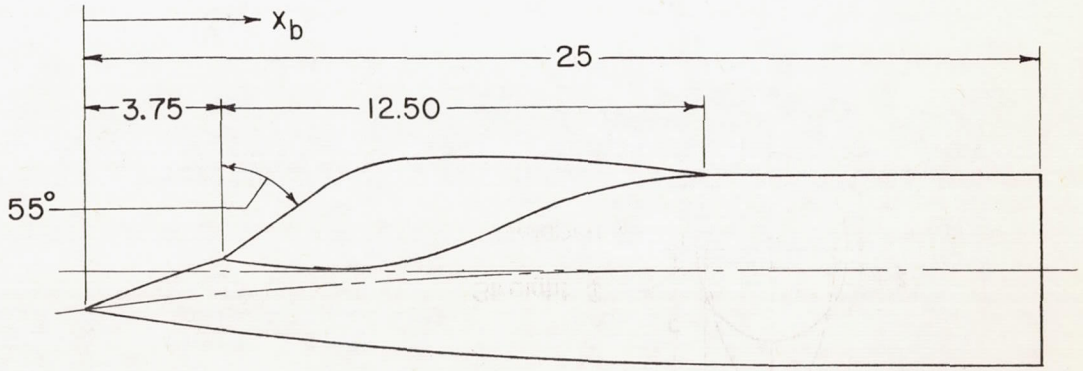
(a) Body.

Figure 1.- Model details. All dimensions are in inches.

CANOPY FACE					
x_b = 3.750		x_b = 5.000		x_b = 6.250	
v	u	v	u	v	u
0.000	0.358	0.000	1.227	0.000	2.117
	↓		↓		↓
.350	.358	.350	1.227	.350	2.117
.438	.244	.438	1.130	.438	2.015
.563	.050	.563	.956	.563	1.814
		.688	.694	.688	1.562
		.813	.330	.813	1.230
		.878	.120		
				.938	.762
				1.063	.271



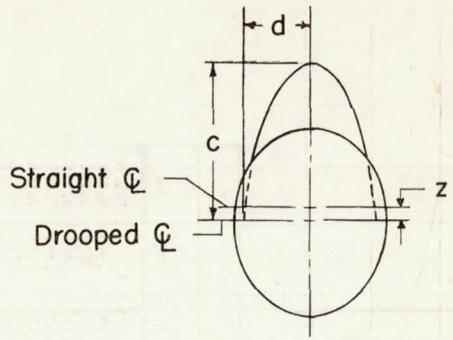
CANOPY BODY		
x_b	c	d
7.500	3.096	1.238
8.750	3.175	1.270
10.000	3.148	1.259
11.250	3.077	1.231
12.500	2.961	1.184
13.750	2.811	1.124
15.000	2.655	1.062
16.250	2.480	.992

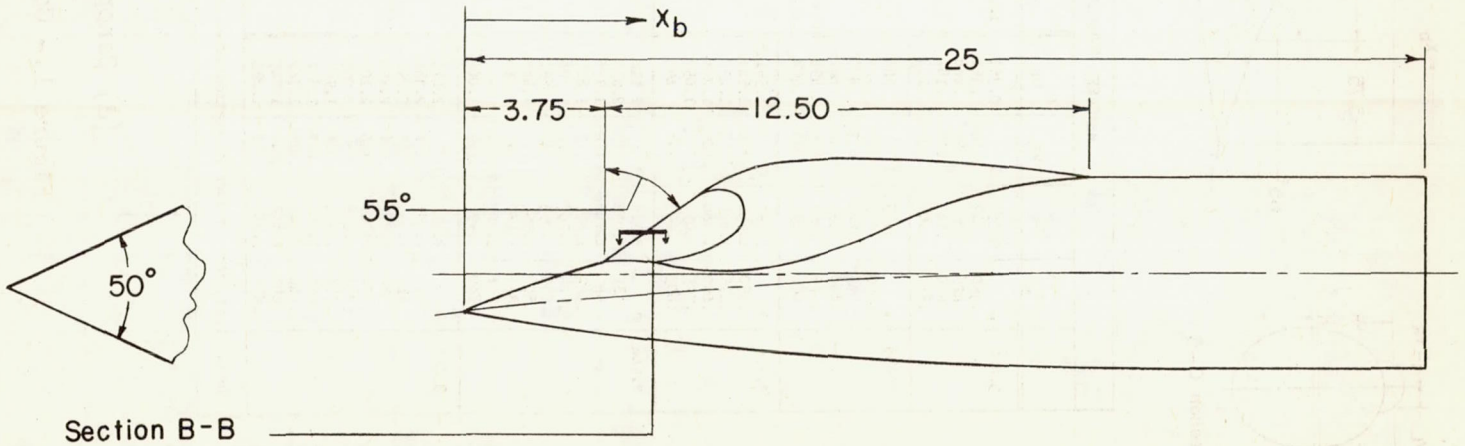


(b) Canopy 1.

Figure 1.- Continued.

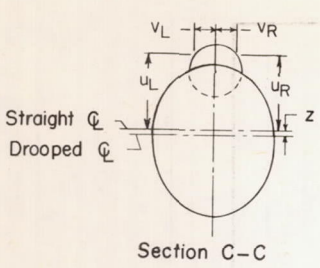
CANOPY BODY		
x_b	c	d
3.750	0.969	
5.000	1.737	
6.250	2.516	1.006
7.500	3.096	1.238
8.750	3.175	1.270
10.000	3.148	1.259
11.250	3.077	1.231
12.500	2.961	1.184
13.750	2.811	1.124
15.000	2.655	1.062
16.250	2.480	.992

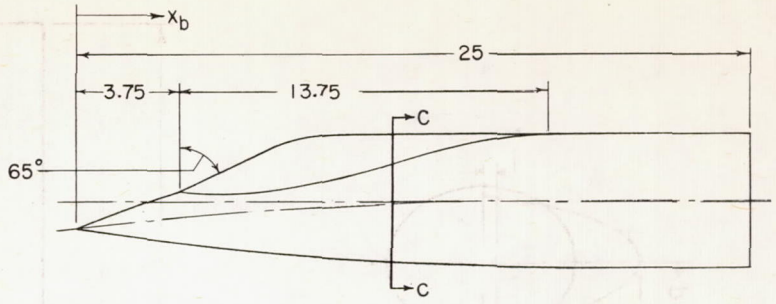




(c) Canopy 2.

Figure 1.- Continued.





MEASURED COORDINATES

x_b	v_L	u_L	v_R	u_R	x_b	v_L	u_L	v_R	u_R
3.816	0	0.352	0	0.352	10.066	0	2.476	0	2.476
	.350	.322	.350	.352		.390	2.385	.390	2.382
	.425	.244	.425	.268		.533	2.293	.533	2.288
	.475	.163	.475	.187		.629	2.198	.629	2.195
	.508	.109	.508	.132		.698	2.101	.698	2.098
5.066	0	.945	0	.945		.748	2.010	.748	2.006
	.350	.919	.350	.945		.782	1.937	.782	1.916
	.475	.803	.475	.820		.802	1.886	.802	1.832
	.600	.594	.600	.641		.809	1.867	.809	1.795
	.675	.407	.675	.454		.863	1.545	.805	1.552
	.684	.393	.684	.402	11.316	0	2.476	0	2.476
6.316	0	1.551	0	1.551		.370	2.378	.370	2.380
	.350	1.530	.350	1.541		.503	2.284	.503	2.283
	.475	1.435	.475	1.430		.591	2.185	.591	2.187
	.600	1.280	.600	1.276		.653	2.095	.653	2.086
	.725	1.052	.725	1.059		.695	2.021	.695	1.991
	.803	.693	.796	.693		.721	1.968	.721	1.905
7.566	0	2.118	0	2.118		.771	1.809	.735	1.811
	.381	2.036	.381	2.033	12.566	0	2.475	0	2.475
	.540	1.945	.540	1.935		.348	2.371	.348	2.381
	.647	1.851	.647	1.824		.472	2.269	.472	2.283
	.724	1.757	.724	1.708		.552	2.172	.552	2.174
	.782	1.653	.782	1.592		.615	2.054	.615	2.034
	.823	1.554	.823	1.489	13.816	0	2.477	0	2.477
	.851	1.467	.851	1.388		.326	2.373	.326	2.383
	.866	1.403	.866	---		.439	2.274	.439	2.284
	.860	.997	.829	1.000		.471	2.229	.483	2.223
8.816	0	2.411	0	2.411	15.066	0	2.485	0	2.485
	.212	2.391	.212	2.384		.332	2.351	.345	2.359
	.447	2.310	.447	2.292	16.316	0	2.492	0	2.492
	.578	2.226	.578	2.198		.193	2.438	.222	2.433
	.670	2.140	.670	2.103					
	.737	2.058	.737	2.005					
	.786	1.974	.786	1.903					
	.819	1.900	.819	1.810					
	.840	1.841	.840	1.749					
	.849	1.810	.849	1.745					
	.878	1.283	.830	1.290					

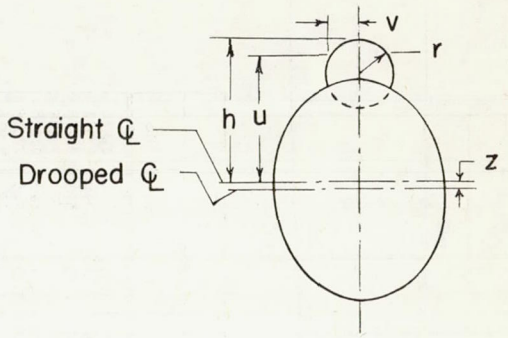
Note: Last entry at each x_b-station gives canopy-body intersection.

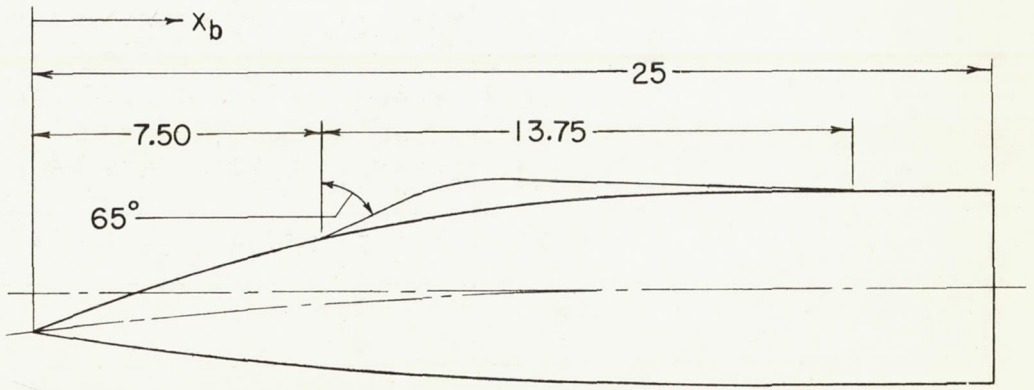
(d) Canopy 3.

Figure 1.- Continued.

CANOPY FACE			
x_b = 7.500		x_b = 8.750	
v	u	v	u
0	1.395	0	1.952
	↓		↓
.350	1.395	.350	1.952
.375	1.379	.400	1.922
.400	1.361	.450	1.880
.425	1.351	.500	1.823
.450	1.320	.550	1.750
.475	1.297	.600	1.643
.500	1.274	.625	1.575
.525	1.249	.650	1.500
.550	1.229	.673	1.425

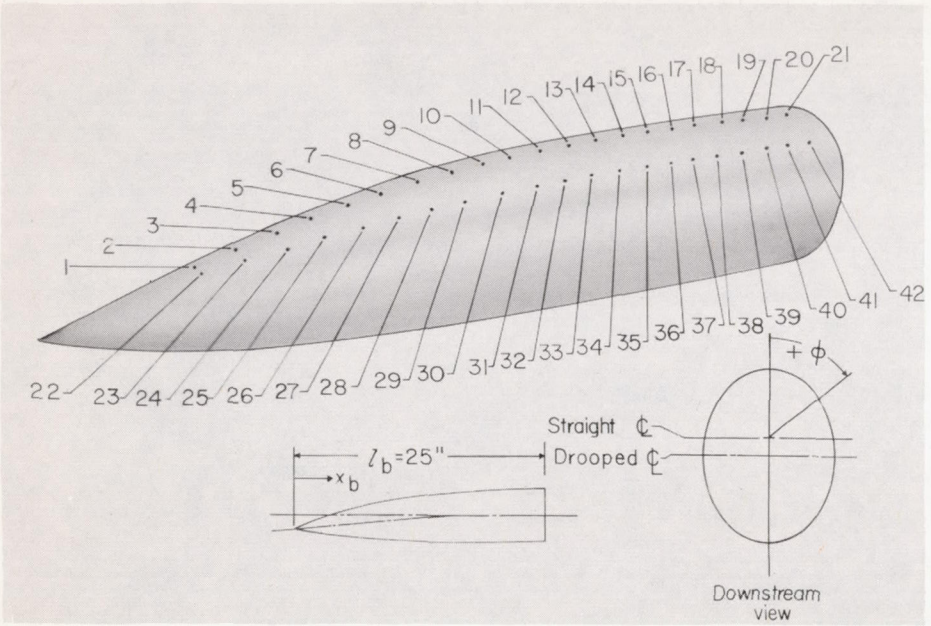
CANOPY BODY		
x_b	h	r
10.000	2.514	0.772
11.250	2.833	.758
12.500	2.882	.738
13.750	2.827	.683
15.000	2.773	.629
16.250	2.718	.574
17.500	2.664	.520
19.375	2.582	.438
21.250	2.500	.356





(e) Canopy 4.

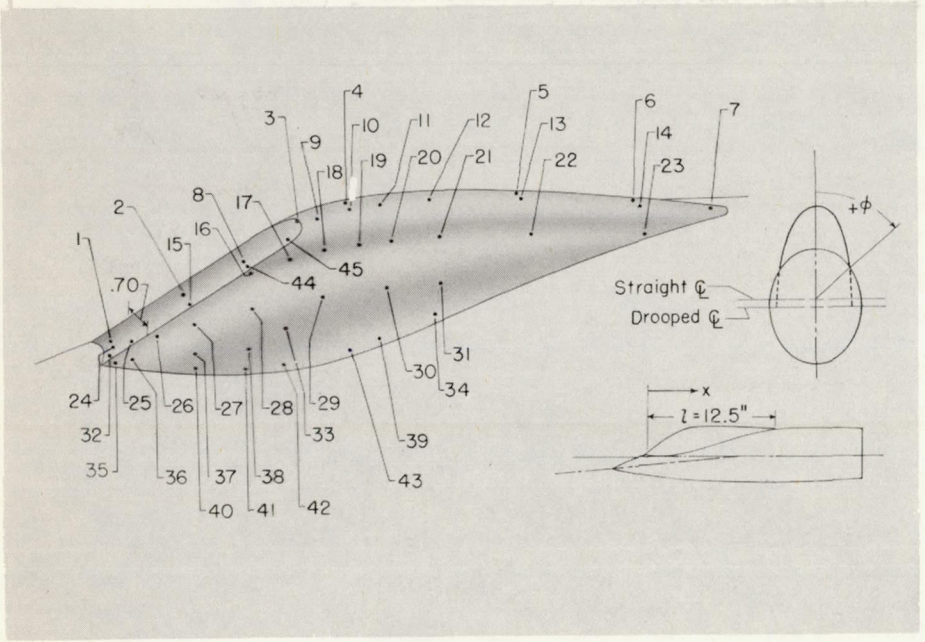
Figure 1.- Concluded.



Orifice location					
Orifice number	Longitudinal station, x_b/l_b	Radial station, ϕ, deg	Orifice number	Longitudinal station, x_b/l_b	Radial station, ϕ, deg
1	0.160	0	22	0.160	30
2	.200	0	23	.200	30
3	.240	0	24	.240	30
4	.280	0	25	.280	30
5	.320	0	26	.320	30
6	.360	0	27	.360	30
7	.400	0	28	.400	30
8	.440	0	29	.440	30
9	.480	0	30	.480	30
10	.520	0	31	.520	30
11	.560	0	32	.560	30
12	.600	0	33	.600	30
13	.640	0	34	.640	30
14	.680	0	35	.680	30
15	.720	0	36	.720	30
16	.760	0	37	.760	30
17	.800	0	38	.800	30
18	.840	0	39	.840	30
19	.880	0	40	.880	30
20	.920	0	41	.920	30
21	.960	0	42	.960	30

(a) Fuselage forebody alone.

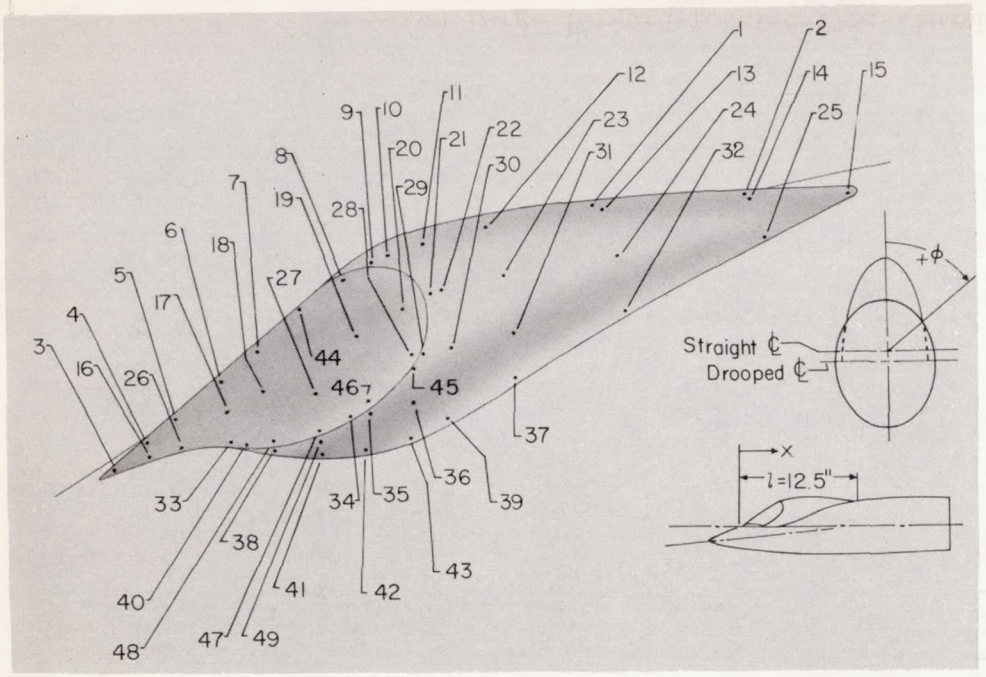
Figure 2.- Location of pressure orifices for the five models tested.



Orifice location					
Orifice number	Longitudinal station, x/l	Radial station, ϕ, deg	Orifice number	Longitudinal station, x/l	Radial station, ϕ, deg
1	0.006	0	24	0.004	30
2	.092	0	25	.017	30
3	.240	0	26	.046	30
4	.311	0	27	.092	30
5	.600	0	28	.164	30
6	.828	0	29	.260	30
7	.988	0	30	.356	30
8	.164	3	31	.440	30
9	.260	3	32	.000	45
10	.311	3	33	.216	45
11	.356	3	34	.440	45
12	.440	3	35	.001	57.5
13	.600	3	36	.017	57.5
14	.828	3	37	.092	57.5
15	.092	15	38	.164	57.5
16	.164	15	39	.356	57.5
17	.216	15	40	.092	80
18	.260	15	41	.164	80.5
19	.311	15	42	.216	79
20	.356	15	43	.311	66
21	.440	15	44	.164	10
22	.600	15	45	.216	7
23	.828	15			

(b) Large forward-located flat-windshield canopy 1.

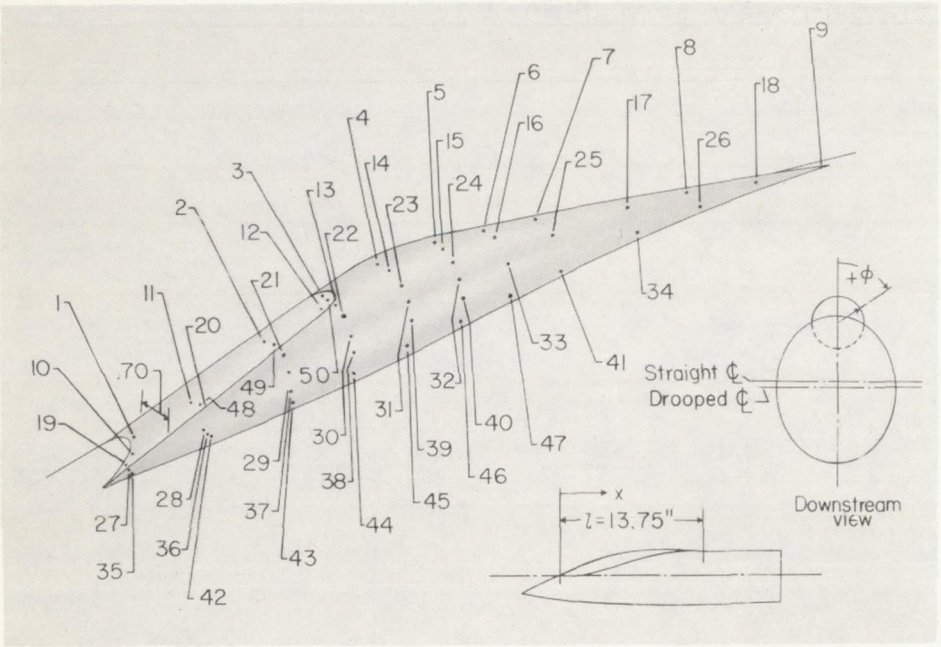
Figure 2.- Continued.



Orifice location					
Orifice number	Longitudinal station, x/l	Radial station, ϕ, deg	Orifice number	Longitudinal station, x/l	Radial station, ϕ, deg
1	0.600	0	26	0.076	30
2	.828	0	27	.212	30
3	.008	3	28	.311	30
4	.044	3	29	.324	30
5	.076	3	30	.356	30
6	.124	3	31	.440	30
7	.164	3	32	.600	30
8	.260	3	33	.124	45
9	.295	3	34	.244	45
10	.311	3	35	.260	45
11	.356	3	36	.311	45
12	.440	3	37	.440	45
13	.600	3	38	.164	57.5
14	.828	3	39	.356	57.5
15	.988	3	40	.140	53
16	.044	15	41	.212	62
17	.124	15	42	.260	68
18	.164	15	43	.311	66
19	.260	15	44	.212	1
20	.311	15	45	.311	34
21	.345	15	46	.260	41
22	.356	15	47	.212	48
23	.440	15	48	.164	51
24	.600	15	49	.212	51
25	.828	15			

(c) Large forward-located vee-windshield canopy 2.

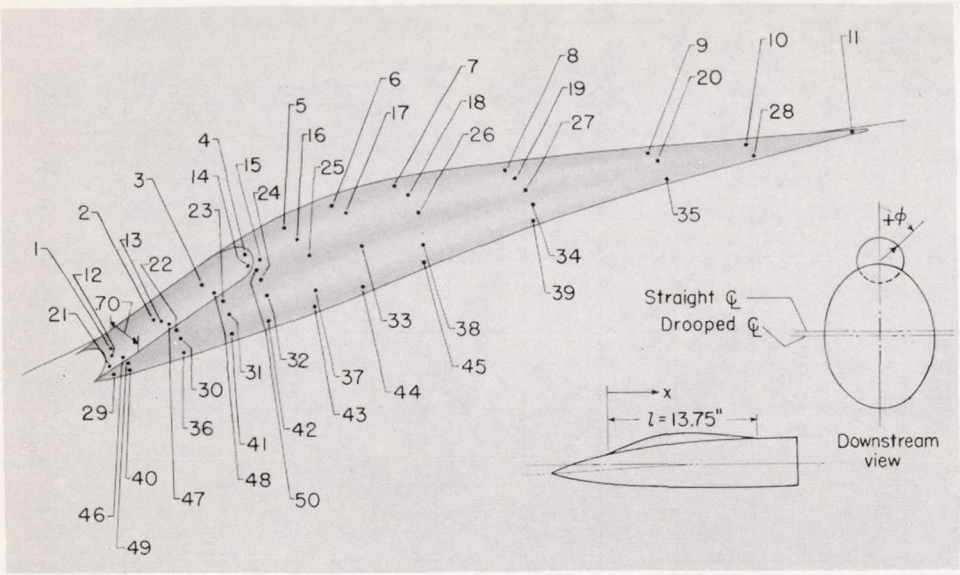
Figure 2.- Continued.



Orifice location					
Orifice number	Longitudinal station, x/l	Radial station, ϕ, deg	Orifice number	Longitudinal station, x/l	Radial station, ϕ, deg
1	0.004	0	26	0.760	40
2	.164	0	27	-.015	60
3	.239	0	28	.065	60
4	.309	0	29	.164	60
5	.382	0	30	.239	60
6	.455	0	31	.309	60
7	.527	0	32	.382	60
8	.760	0	33	.455	60
9	.993	0	34	.655	60
10	.000	20	35	-.015	80
11	.065	20	36	.065	80
12	.223	20	37	.164	80
13	.239	20	38	.239	80
14	.309	20	39	.309	80
15	.382	20	40	.382	80
16	.455	20	41	.527	80
17	.655	20	42	.065	98
18	.869	20	43	.164	104
19	-.015	40	44	.239	100
20	.065	40	45	.309	102
21	.164	40	46	.382	105
22	.239	40	47	.455	102
23	.309	40	48	.065	32
24	.382	40	49	.164	23
25	.527	40	50	.239	11

(d) Small forward-located flat-windshield canopy 3.

Figure 2.- Continued.



Orifice location					
Orifice number	Longitudinal station, x/l	Radial station, ϕ, deg	Orifice number	Longitudinal station, x/l	Radial station, ϕ, deg
1	0.004	0	26	0.324	43
2	.052	0	27	.467	43
3	.102	0	28	.804	43
4	.149	0	29	-.011	60
5	.193	0	30	.052	60
6	.249	0	31	.102	60
7	.324	0	32	.142	60
8	.467	0	33	.249	60
9	.662	0	34	.467	60
10	.804	0	35	.662	60
11	.985	0	36	.052	80
12	.000	20	37	.193	80
13	.052	20	38	.324	80
14	.142	20	39	.467	80
15	.149	20	40	.004	66
16	.193	20	41	.102	88
17	.249	20	42	.142	91
18	.324	20	43	.193	98
19	.467	20	44	.249	102
20	.662	20	45	.324	100
21	-.011	43	46	.004	40
22	.052	43	47	.052	32
23	.102	43	48	.102	26
24	.142	43	49	.004	48
25	.193	43	50	.142	29

(e) Small rearward-located flat-windshield canopy 4.

Figure 2.- Concluded.

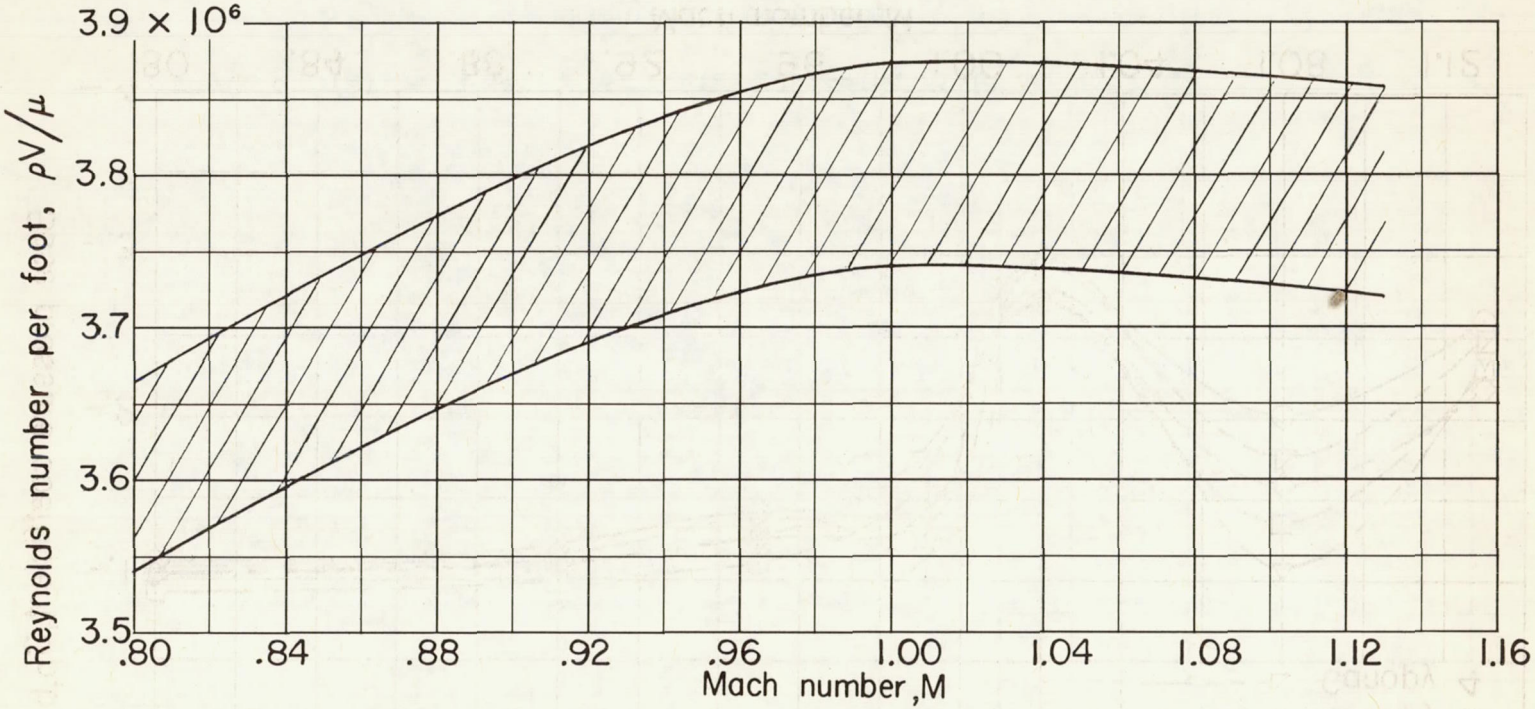


Figure 3.- Variation of Reynolds number with Mach number.

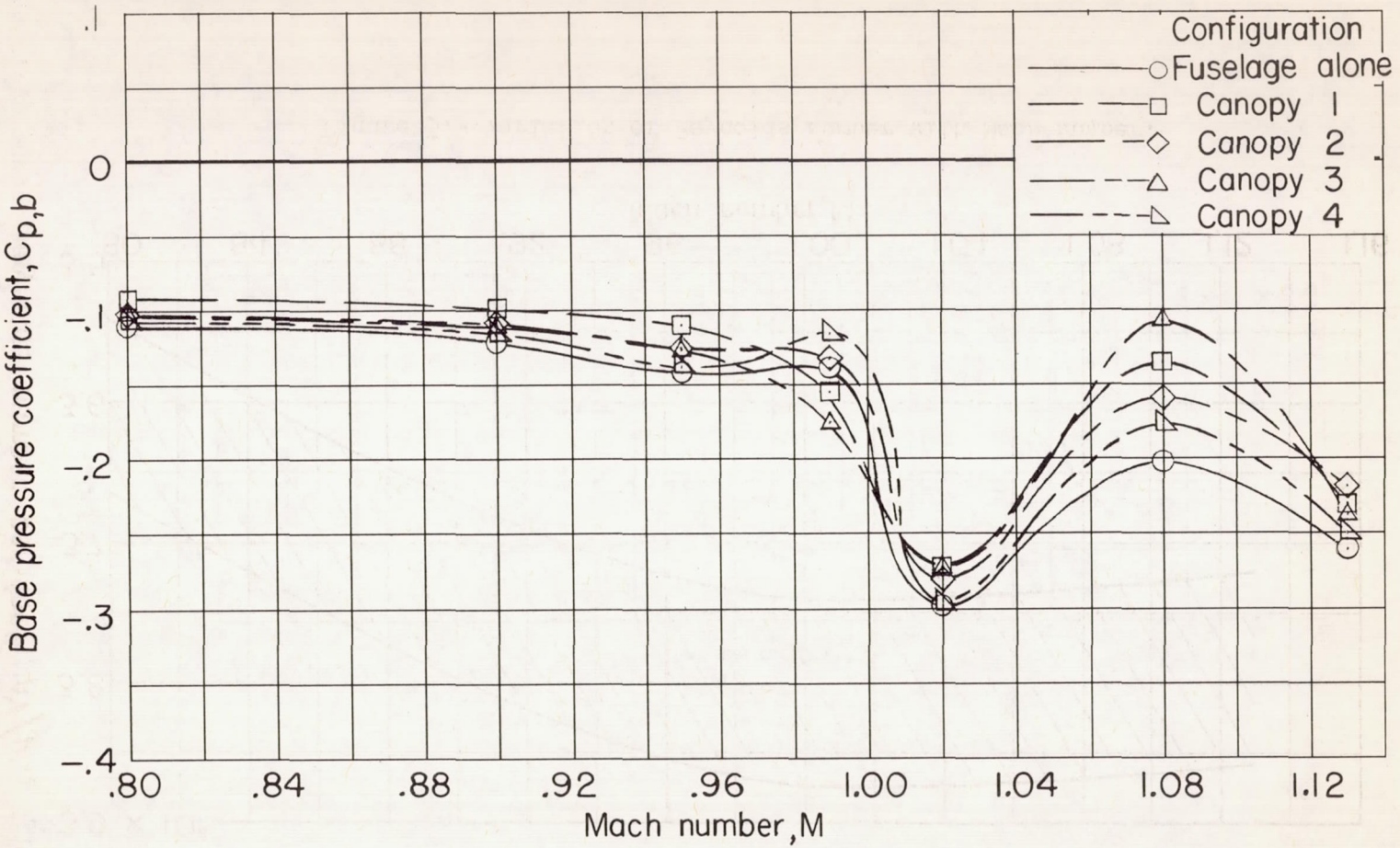
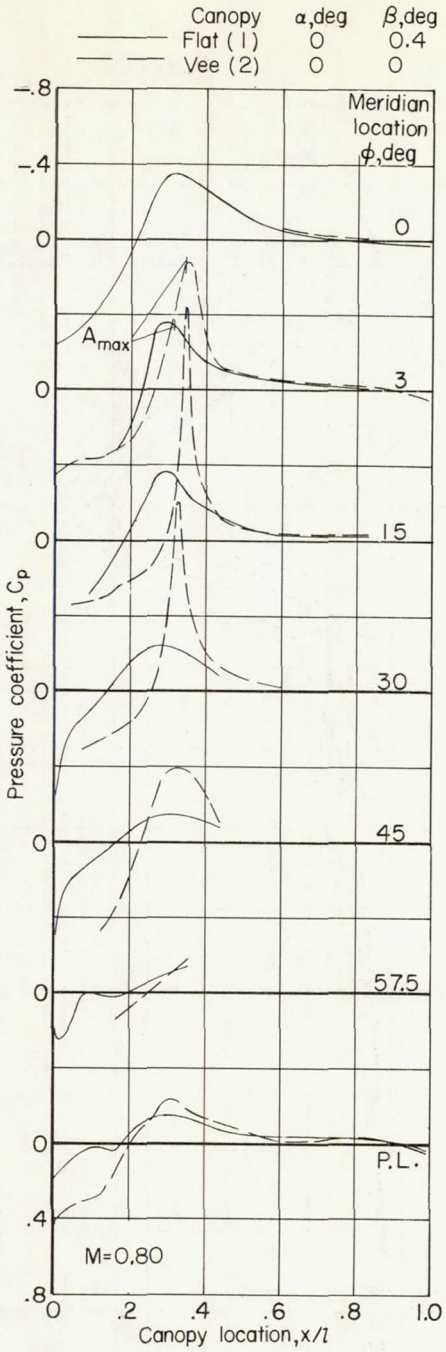
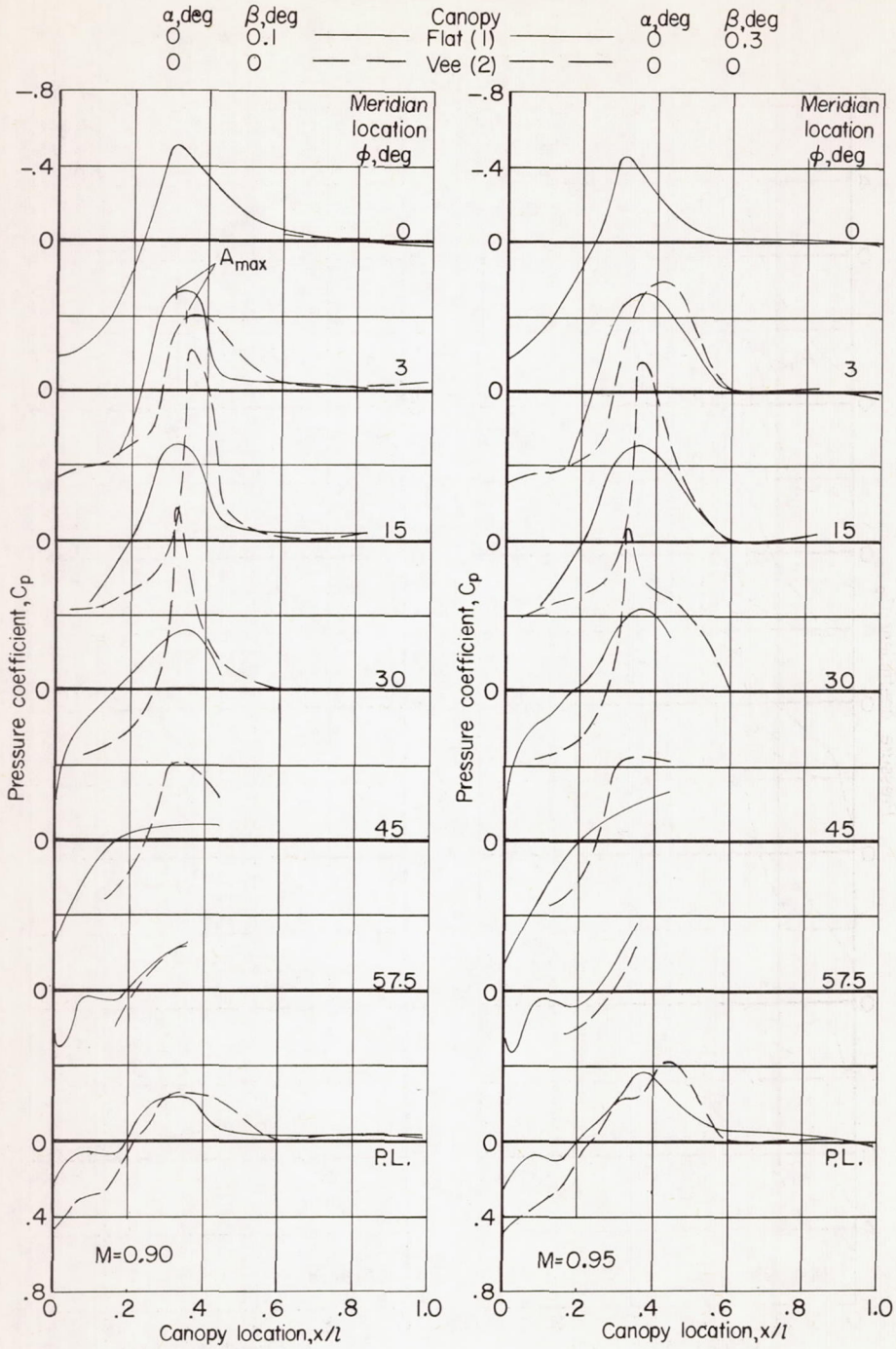


Figure 4.- Variation of base-pressure coefficient with Mach number. $\beta = 0^{\circ}$; $\alpha = 0^{\circ}$ (approx.).



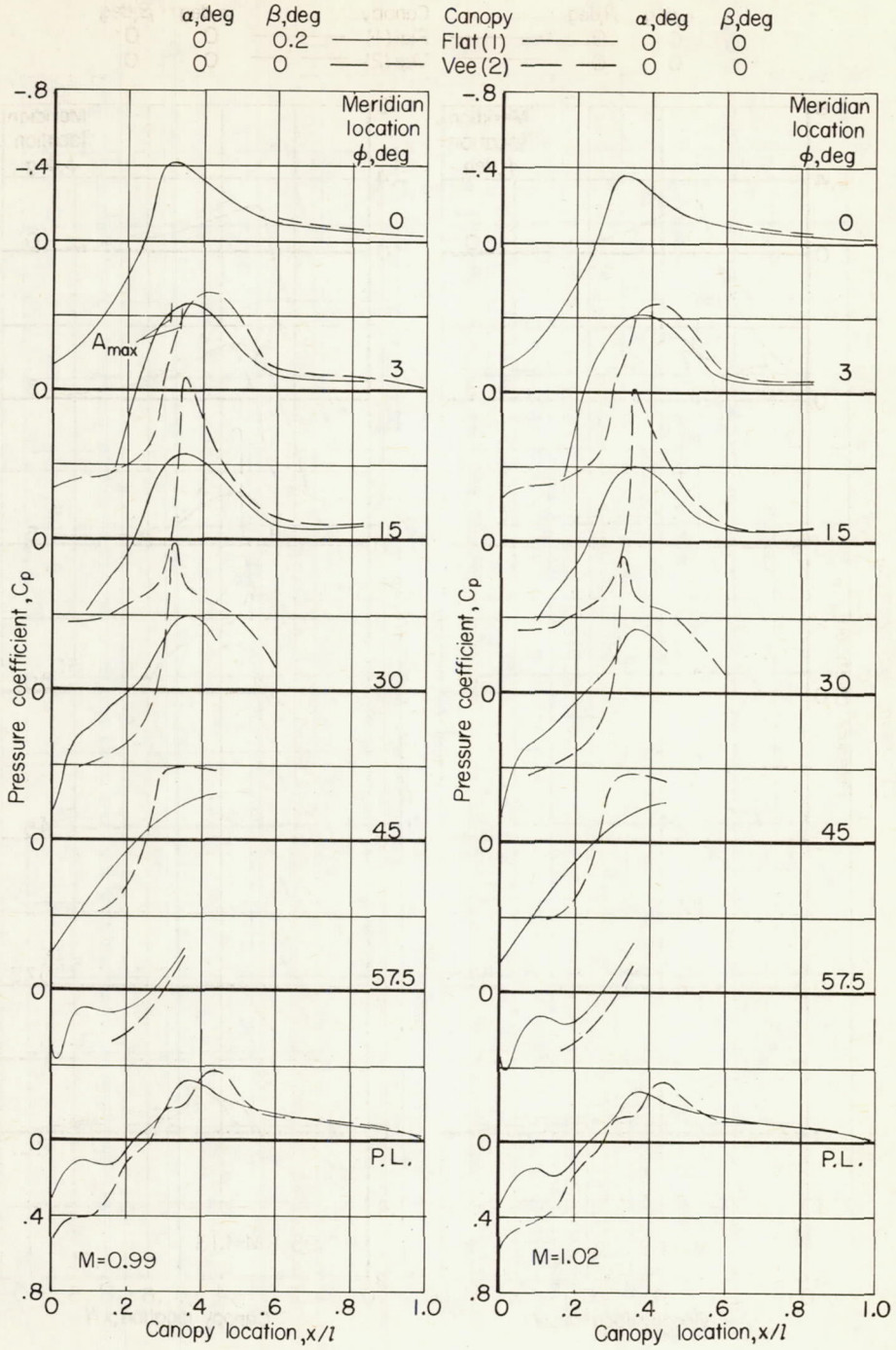
(a) $\alpha = 0^{\circ}$; $\beta \approx 0^{\circ}$.

ure 5.- Effect of windshield shape on pressure-coefficient distributions on large forward-located canopies 1 and 2.



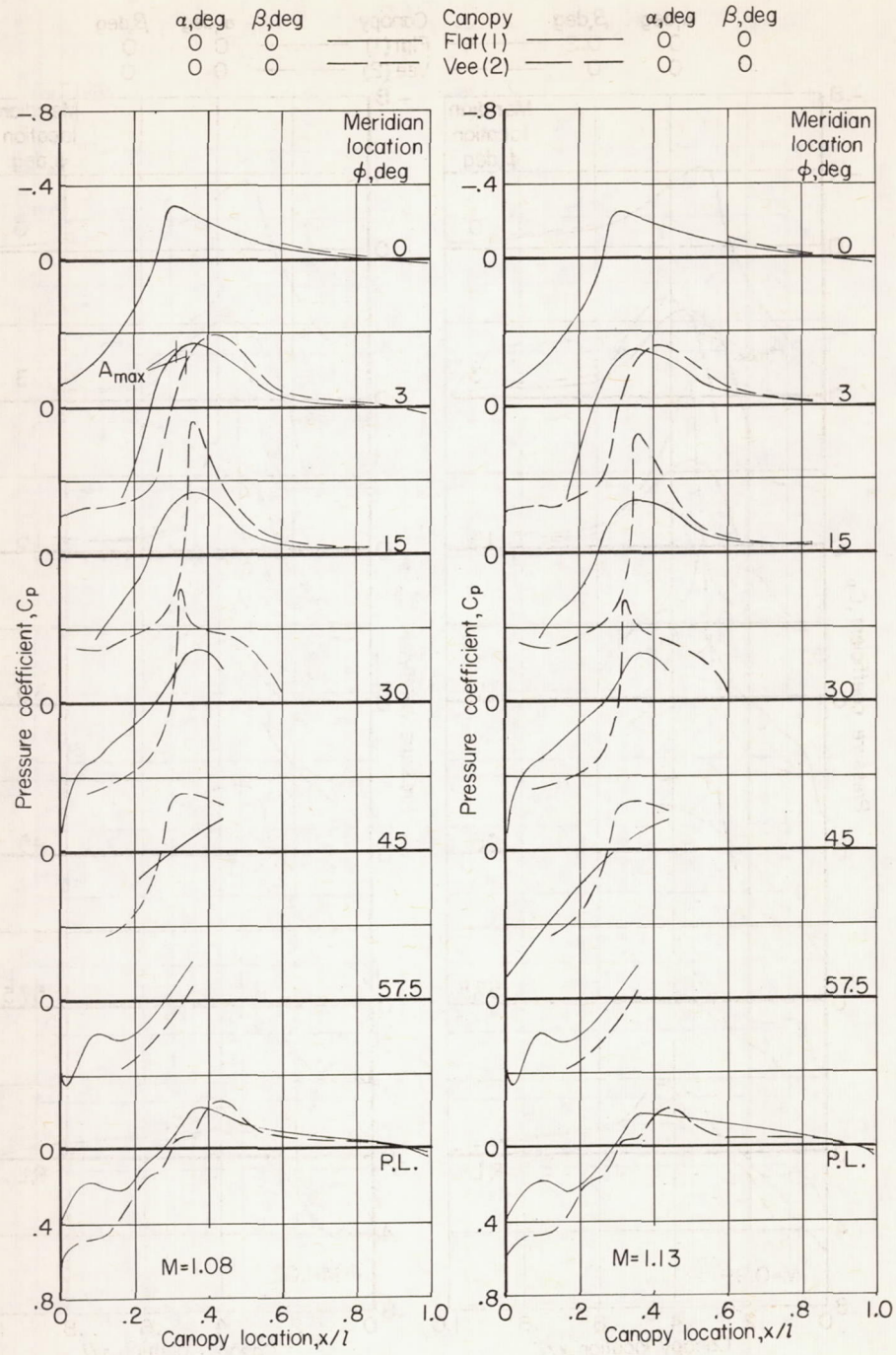
(a) $\alpha = 0^{\circ}$; $\beta \approx 0^{\circ}$. Continued.

Figure 5.- Continued.



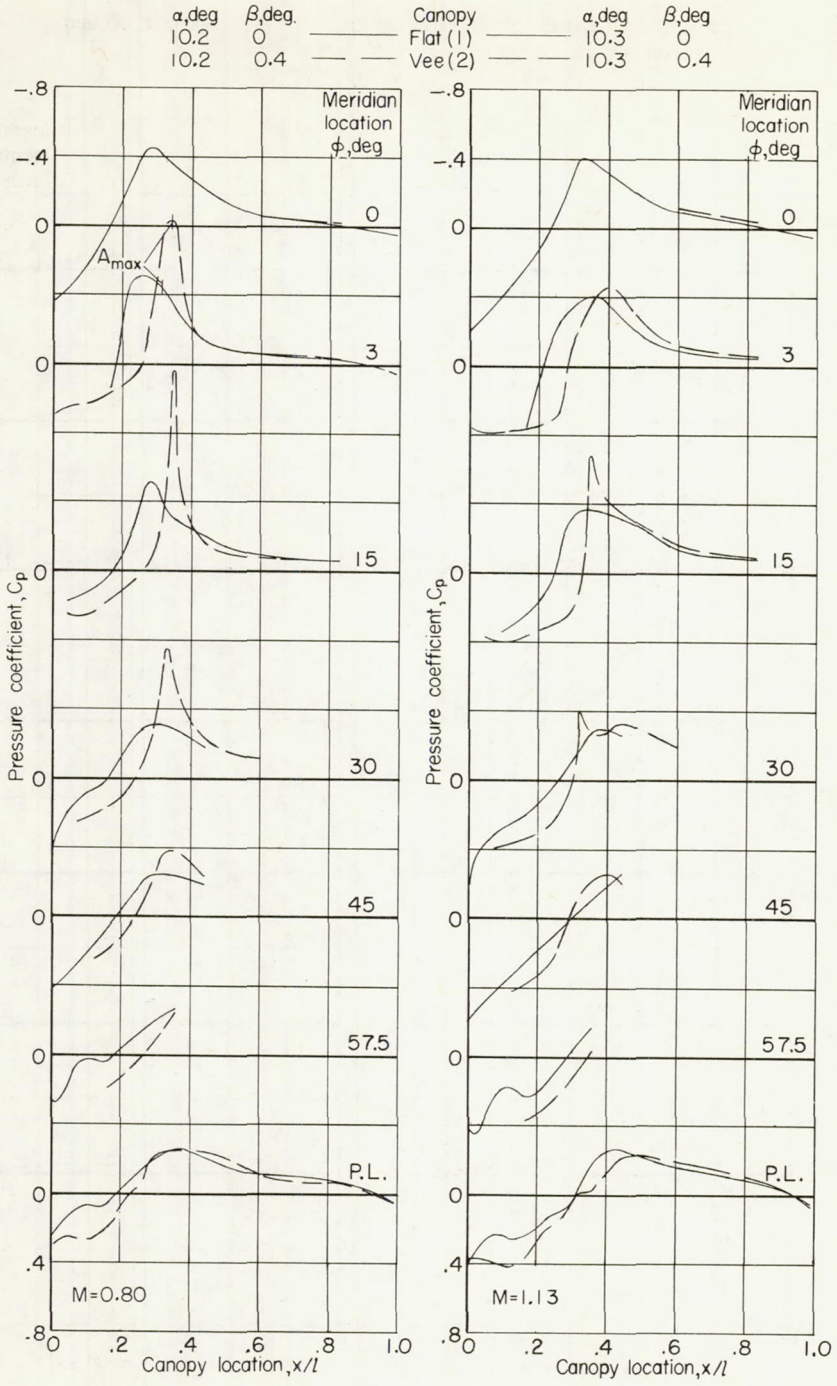
(a) $\alpha = 0^{\circ}$; $\beta \approx 0^{\circ}$. Continued.

Figure 5.- Continued.



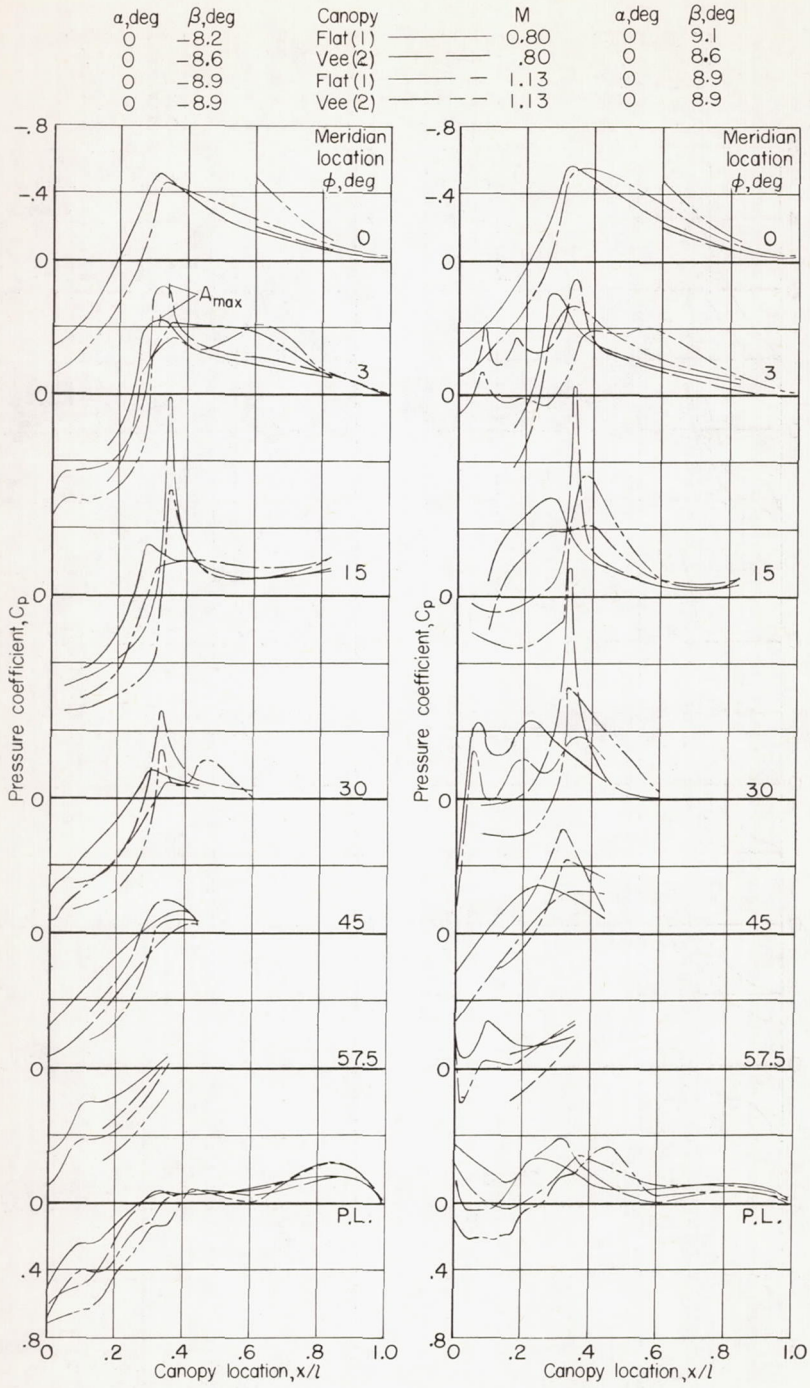
(a) $\alpha = 0^{\circ}$; $\beta \approx 0^{\circ}$. Concluded.

Figure 5.- Continued.



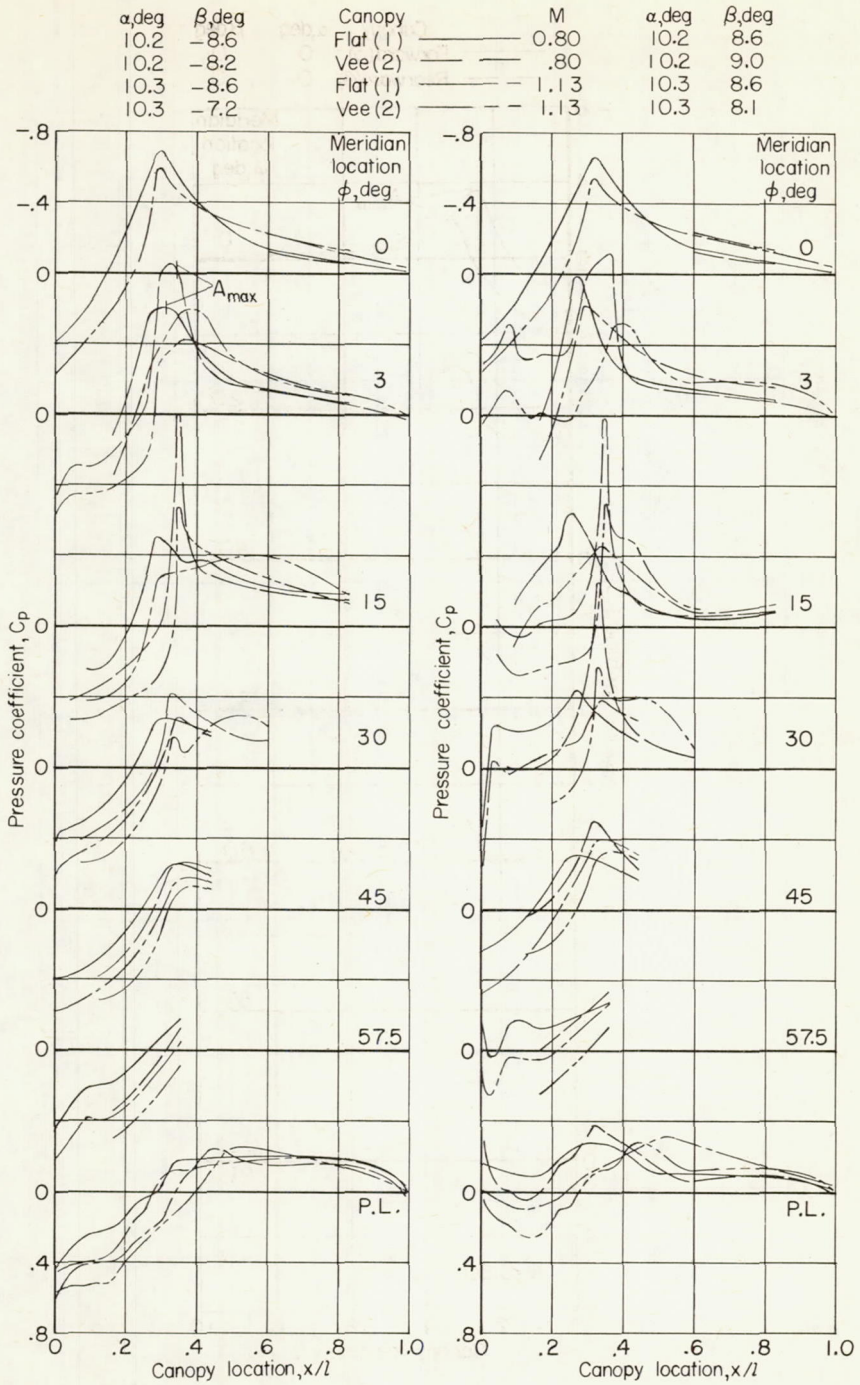
(b) $\alpha \approx 10^{\circ}$; $\beta \approx 0^{\circ}$.

Figure 5.- Continued.



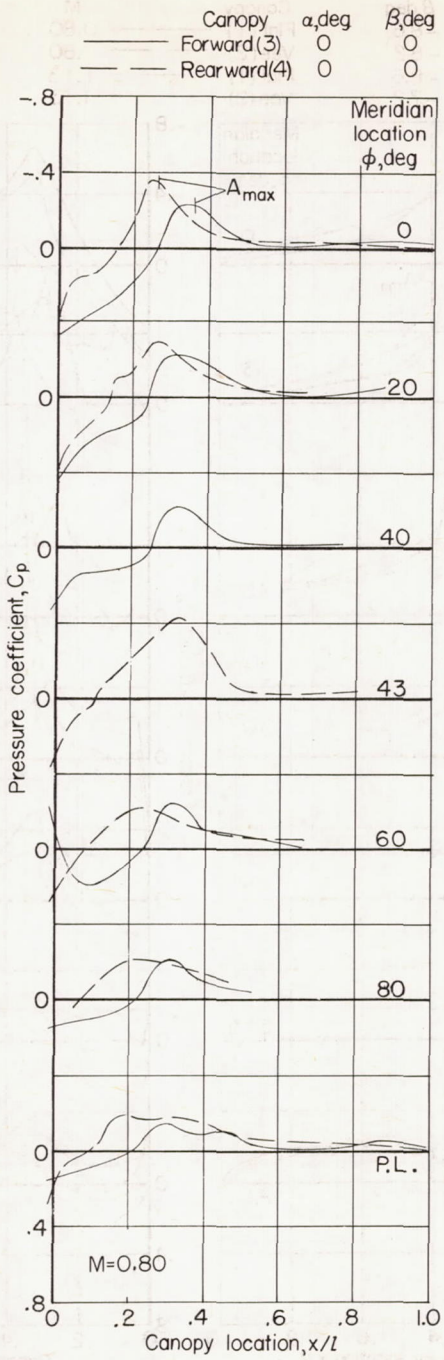
(c) $\alpha = 0^{\circ}$; $\beta \approx \pm 8^{\circ}$.

Figure 5.- Continued.



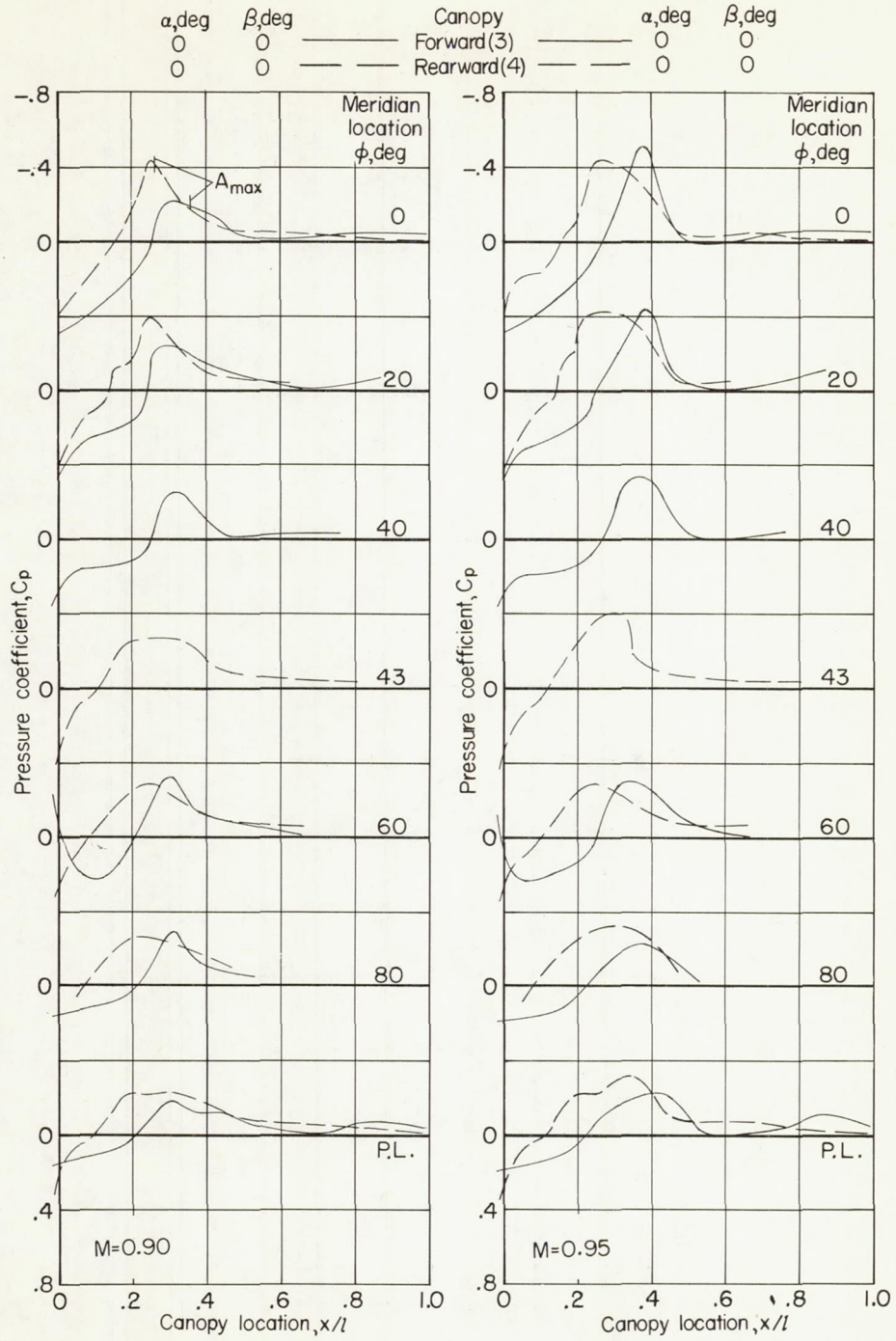
(d) $\alpha \approx 10^{\circ}$; $\beta \approx \pm 8^{\circ}$.

Figure 5.- Concluded.



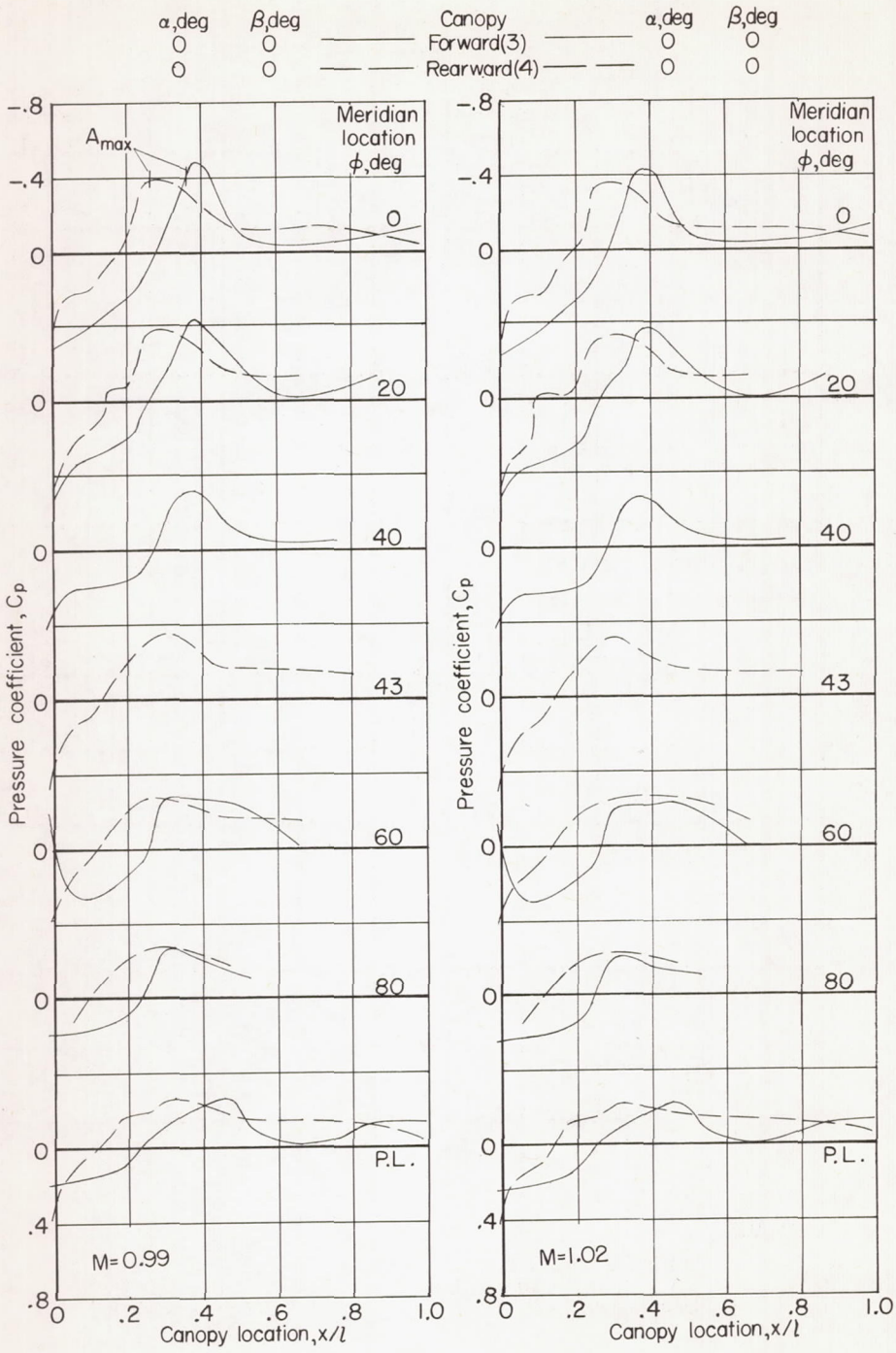
(a) $\alpha = 0^{\circ}$; $\beta = 0^{\circ}$.

Figure 6.- Pressure-coefficient distributions on small forward-located canopy 3 and rearward-located canopy 4.



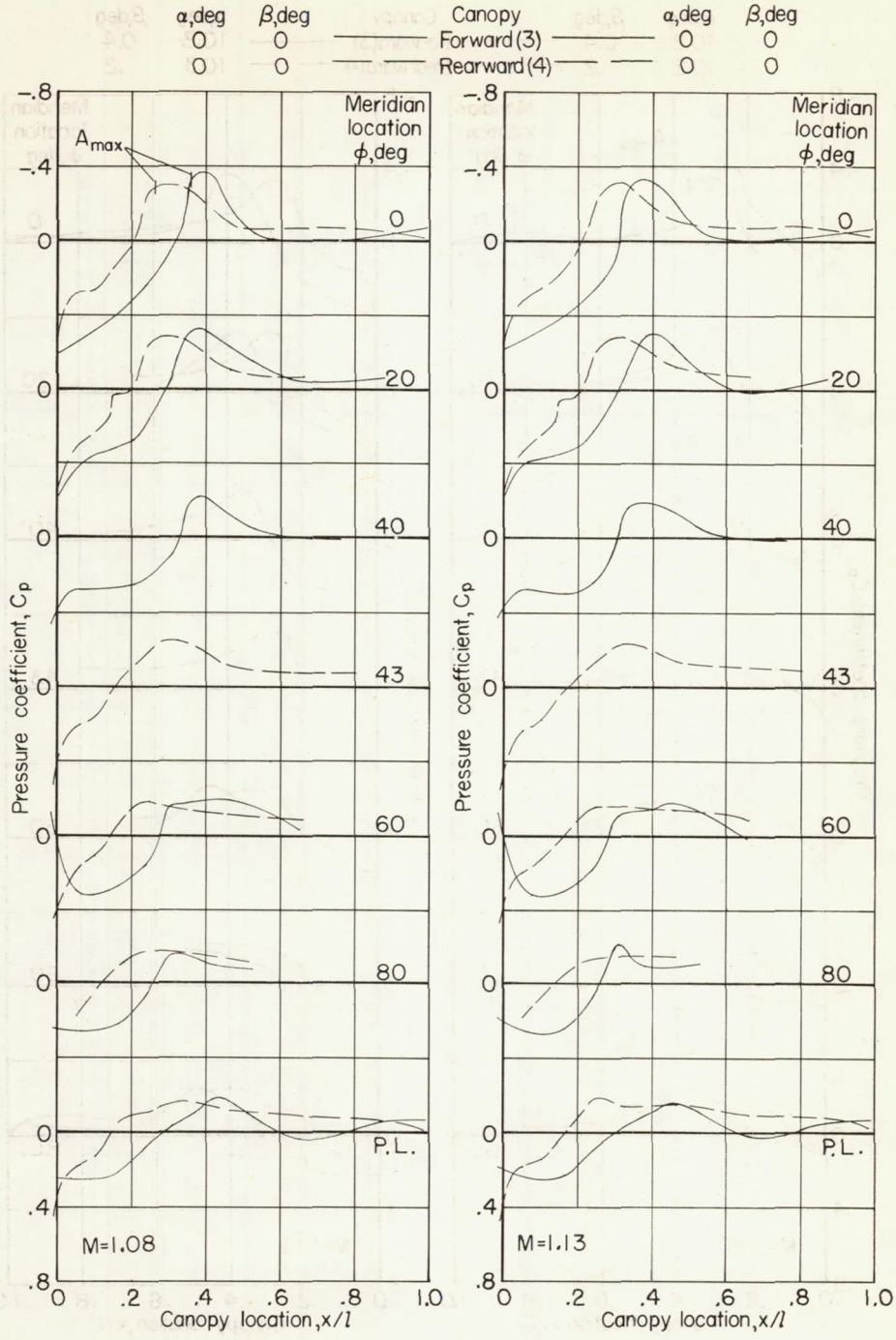
(a) $\alpha = 0^{\circ}$; $\beta = 0^{\circ}$. Continued.

Figure 6.- Continued.



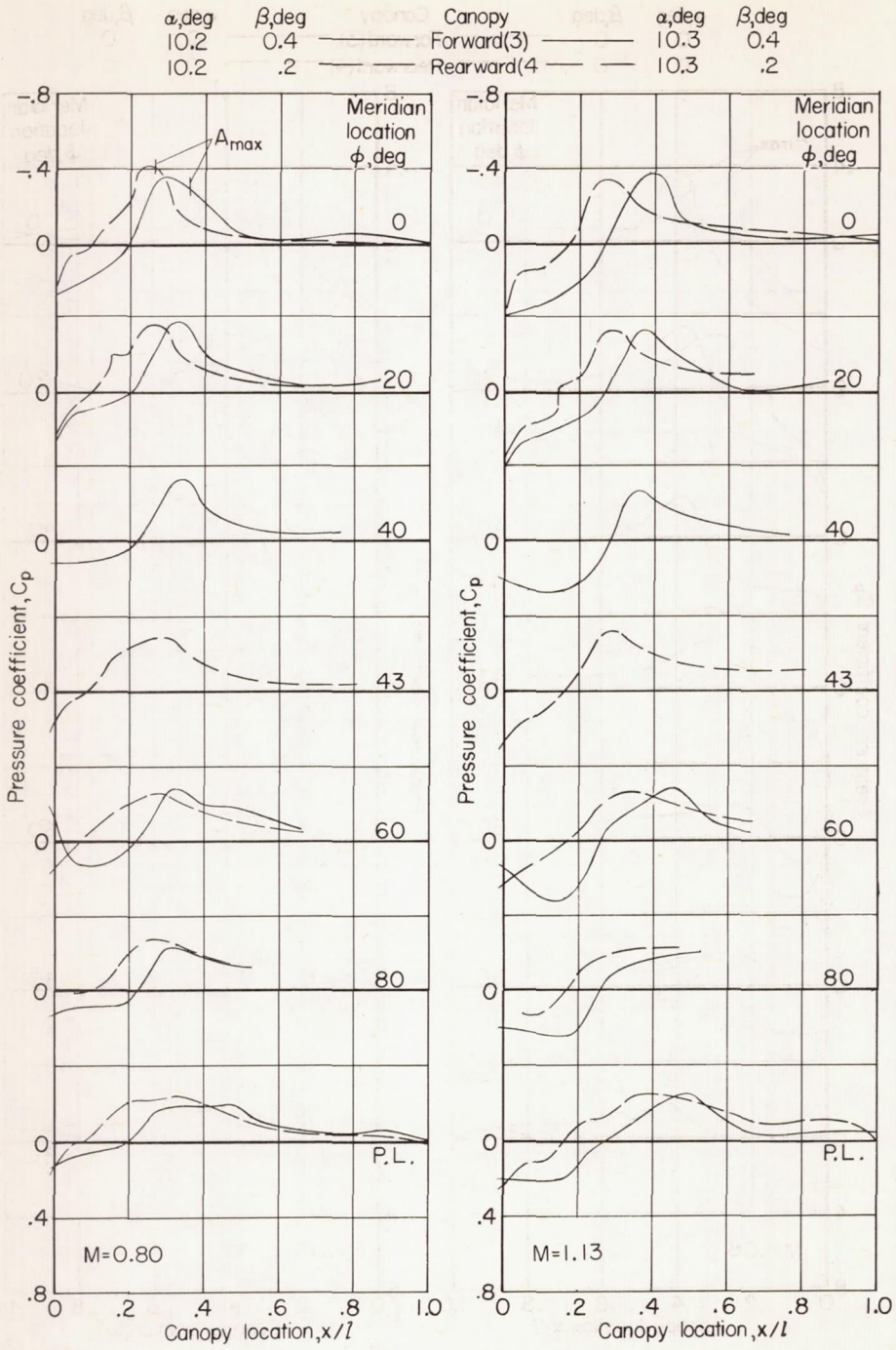
(a) $\alpha = 0^{\circ}$; $\beta = 0^{\circ}$. Continued.

Figure 6.- Continued.



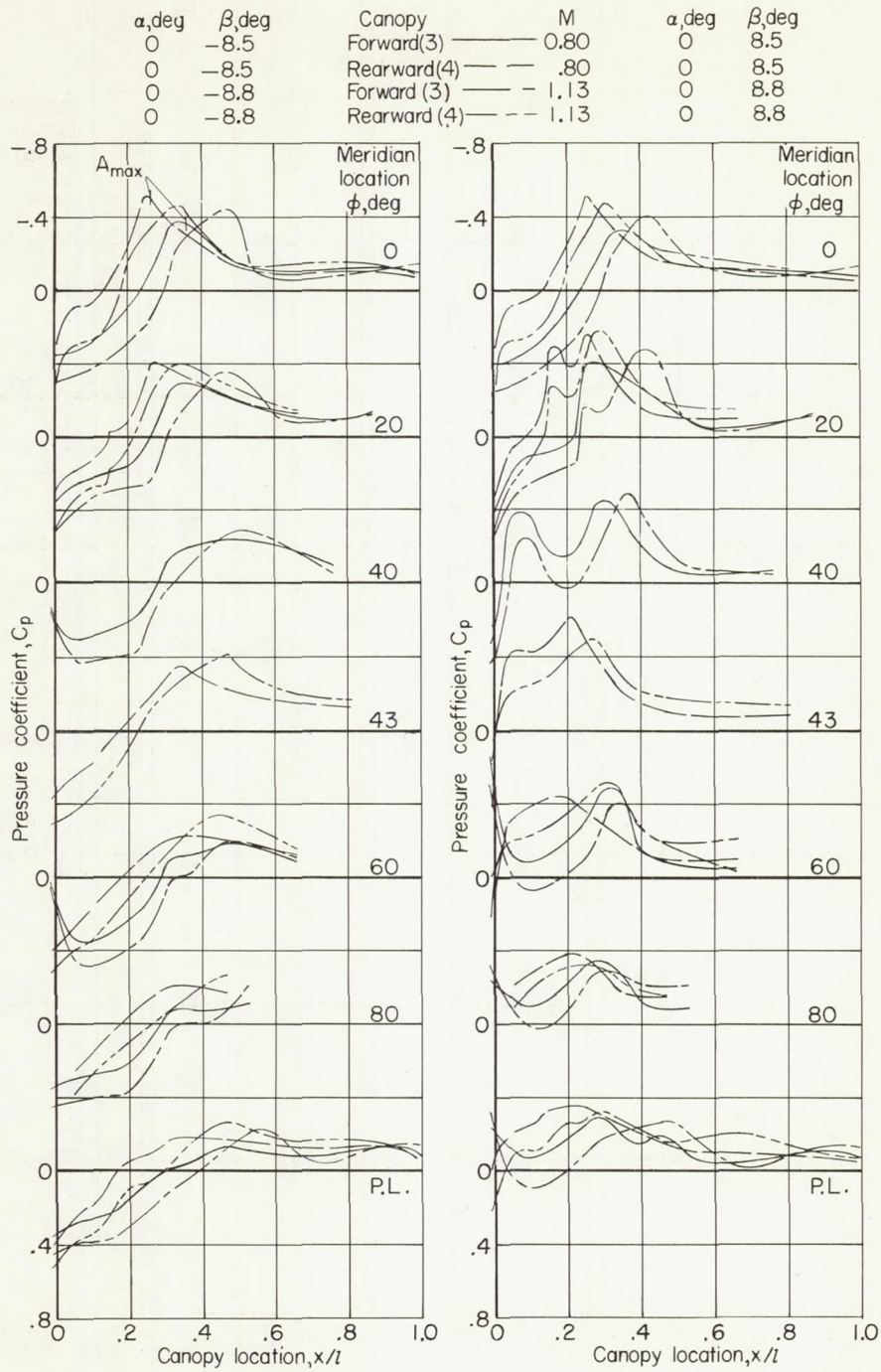
(a) $\alpha = 0^{\circ}$; $\beta = 0^{\circ}$. Concluded.

Figure 6.- Continued.



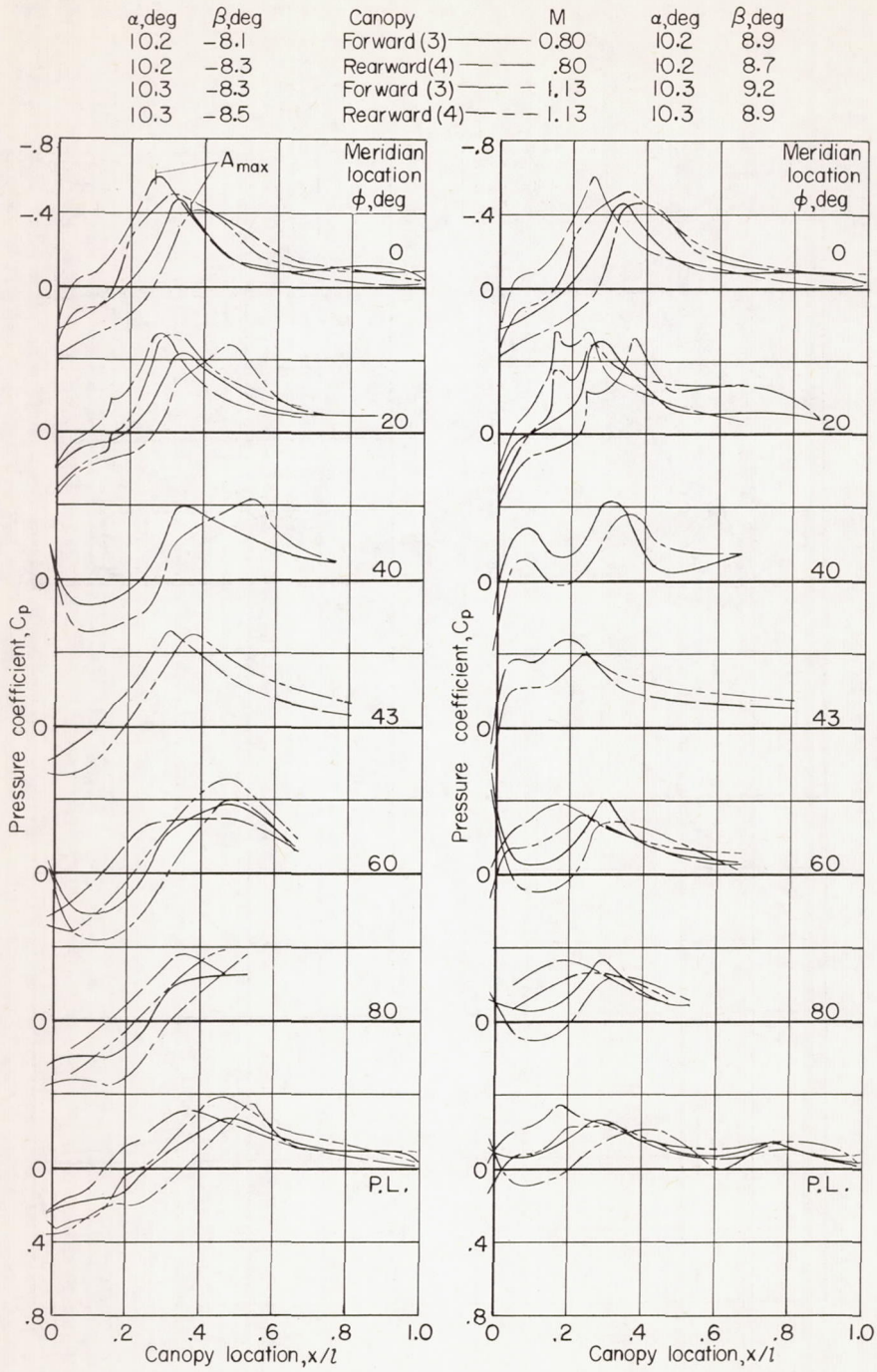
(b) $\alpha \approx 10^{\circ}$; $\beta \approx 0^{\circ}$.

Figure 6.- Continued.



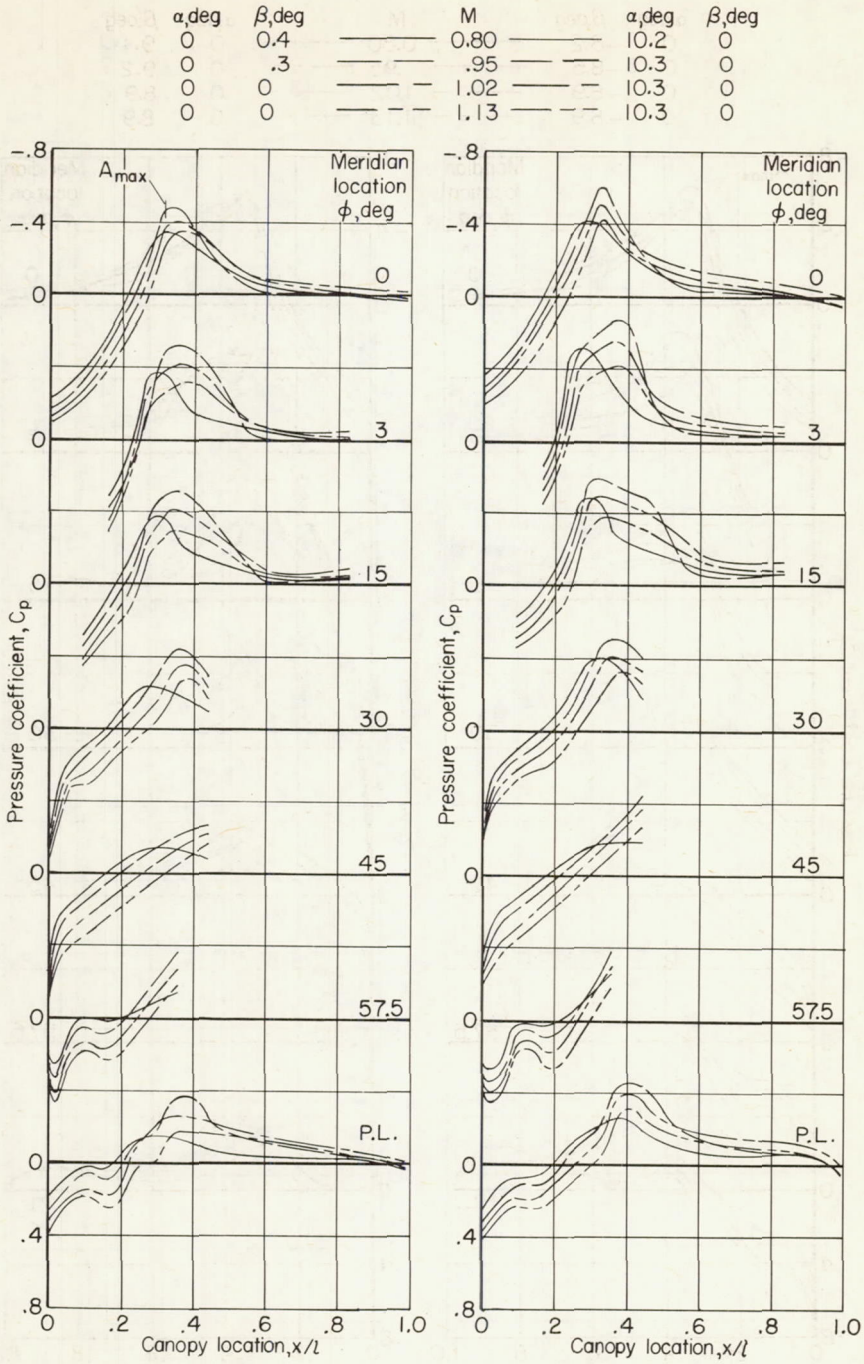
(c) $\alpha = 0^{\circ}$; $\beta \approx \pm 8^{\circ}$.

Figure 6.- Continued.



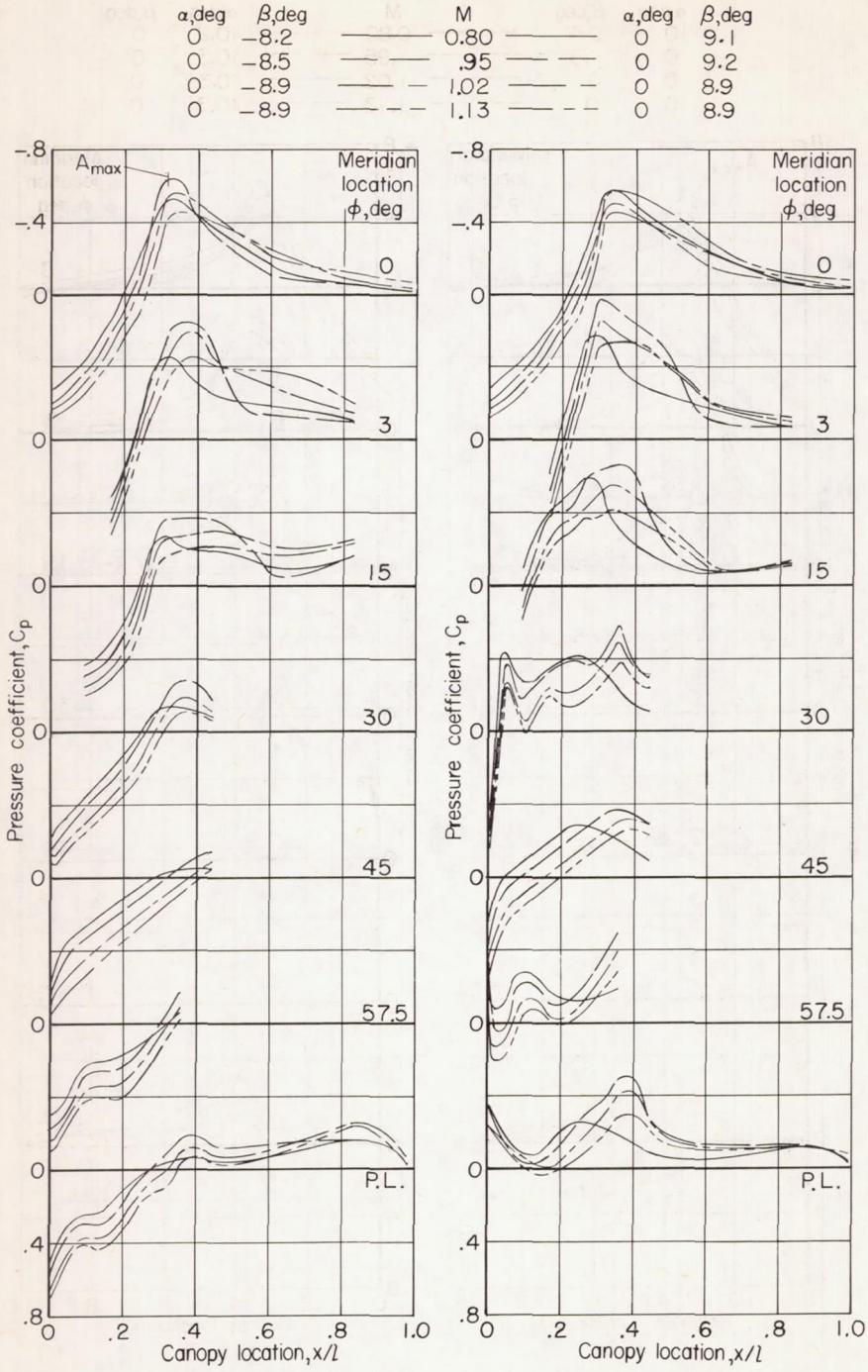
(d) $\alpha \approx 10^{\circ}$; $\beta \approx \pm 8^{\circ}$.

Figure 6.- Concluded.



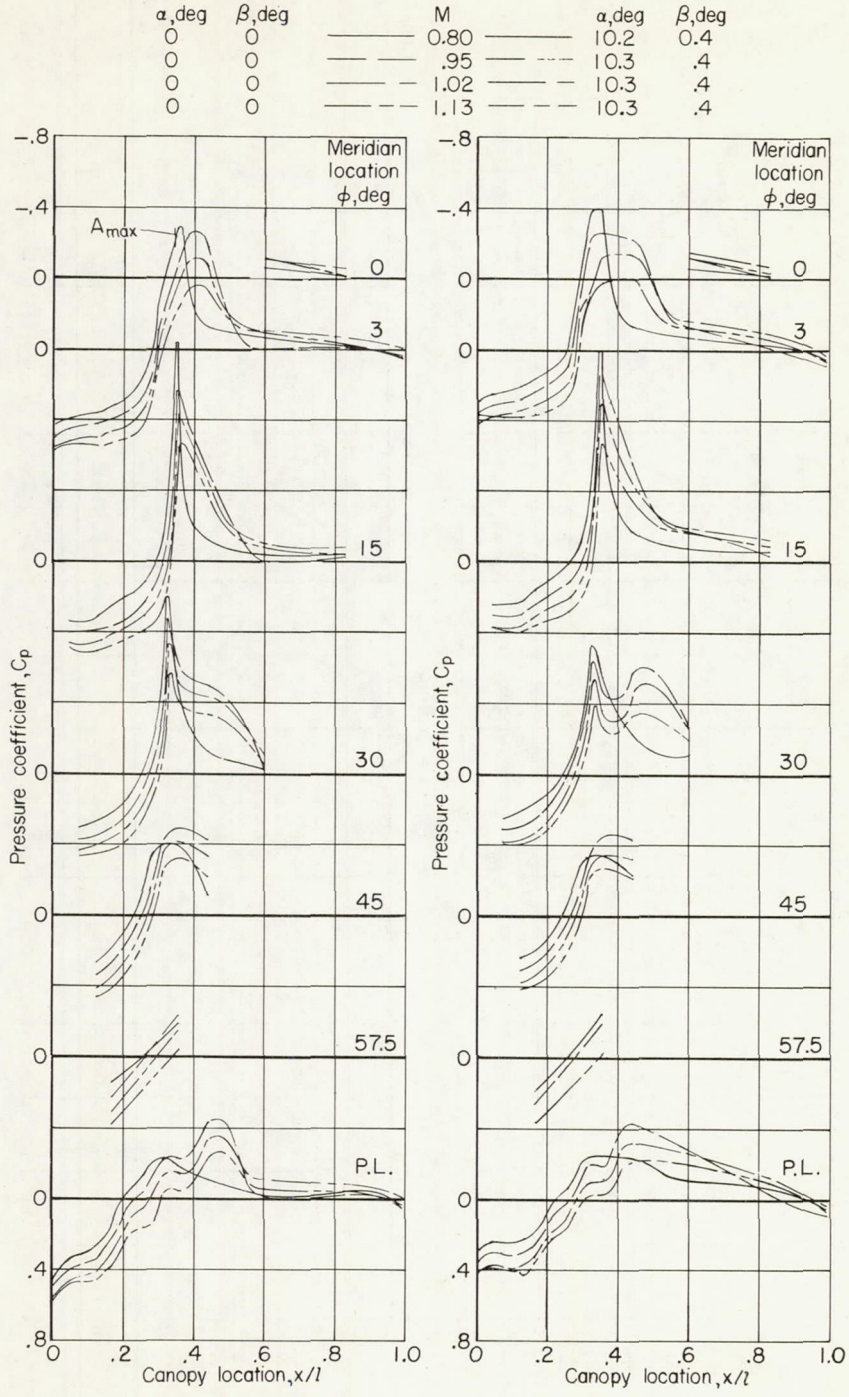
(a) Canopy 1.

Figure 7.- Effect of Mach number on pressure-coefficient distributions for all canopies and fuselage alone.



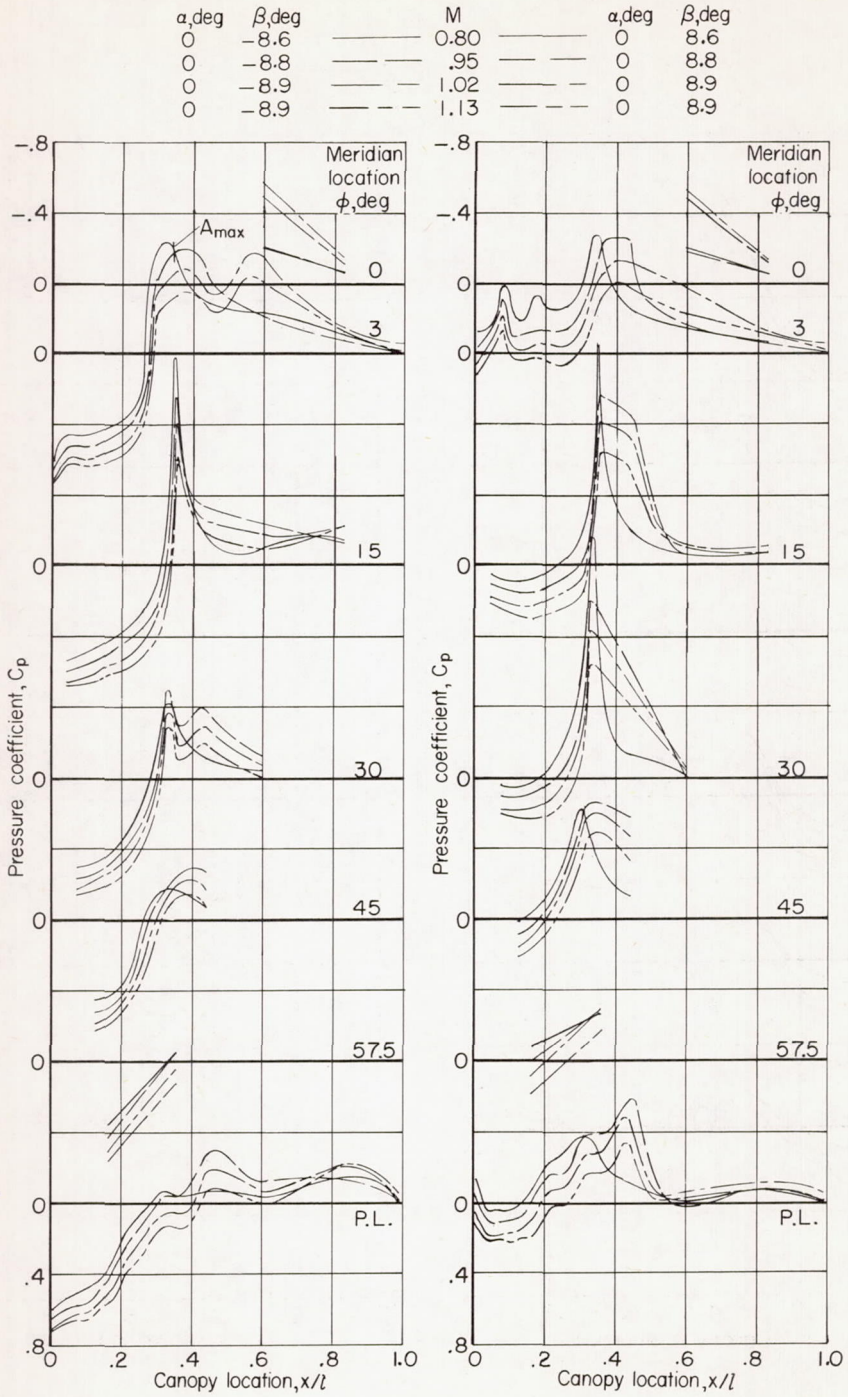
(a) Canopy 1. Concluded.

Figure 7.- Continued.



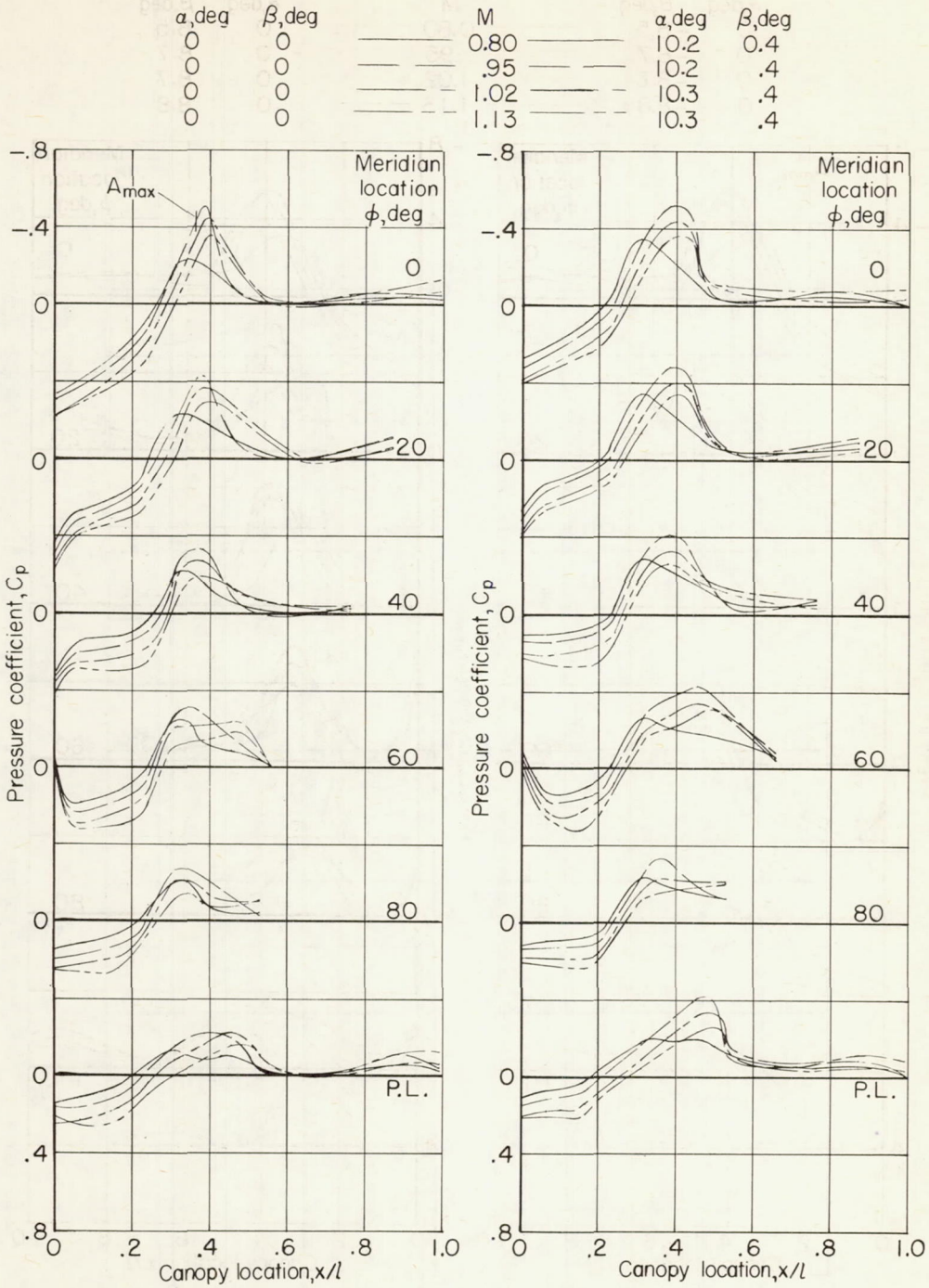
(b) Canopy 2.

Figure 7.- Continued.



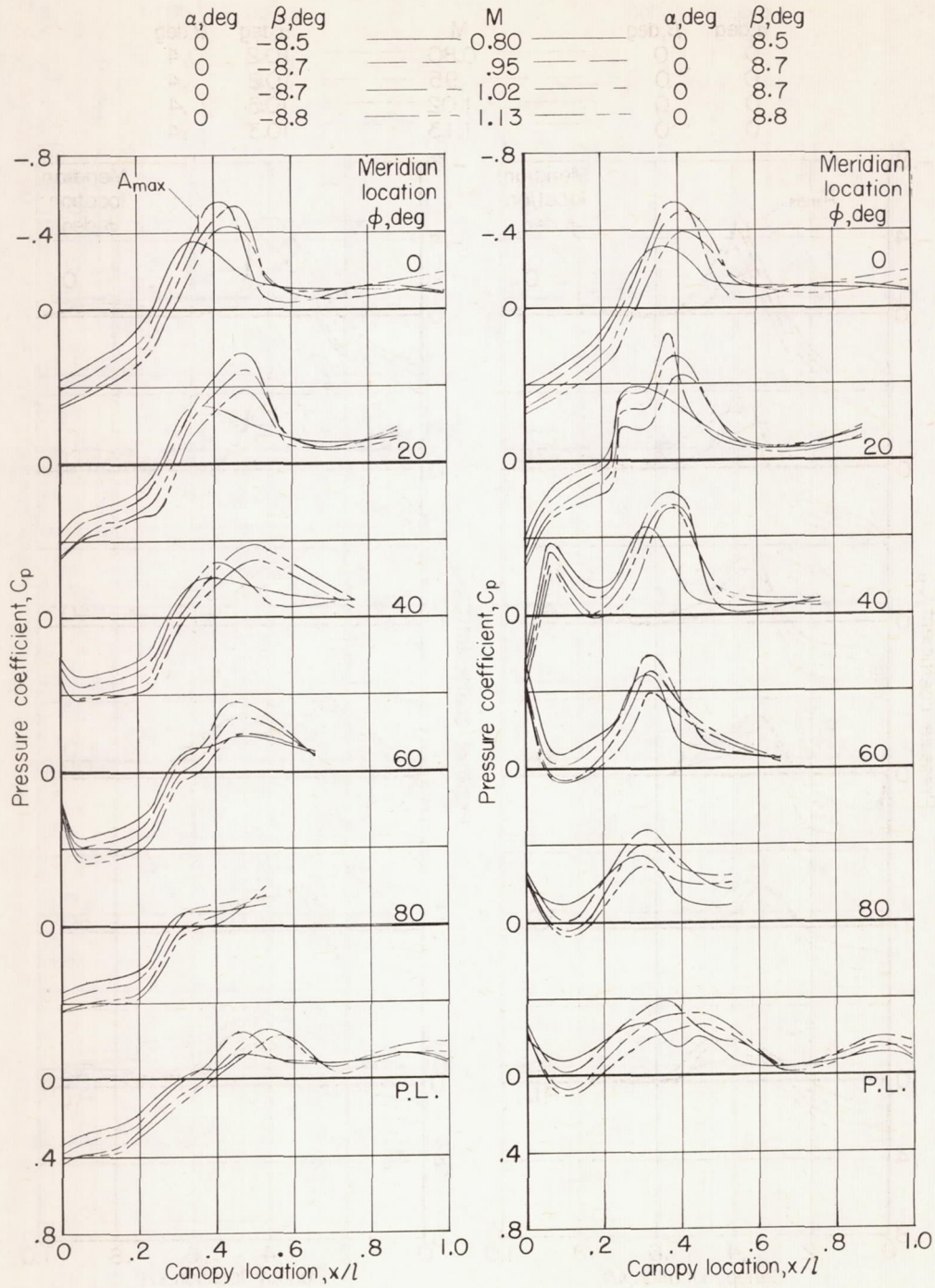
(b) Canopy 2. Concluded.

Figure 7.- Continued.



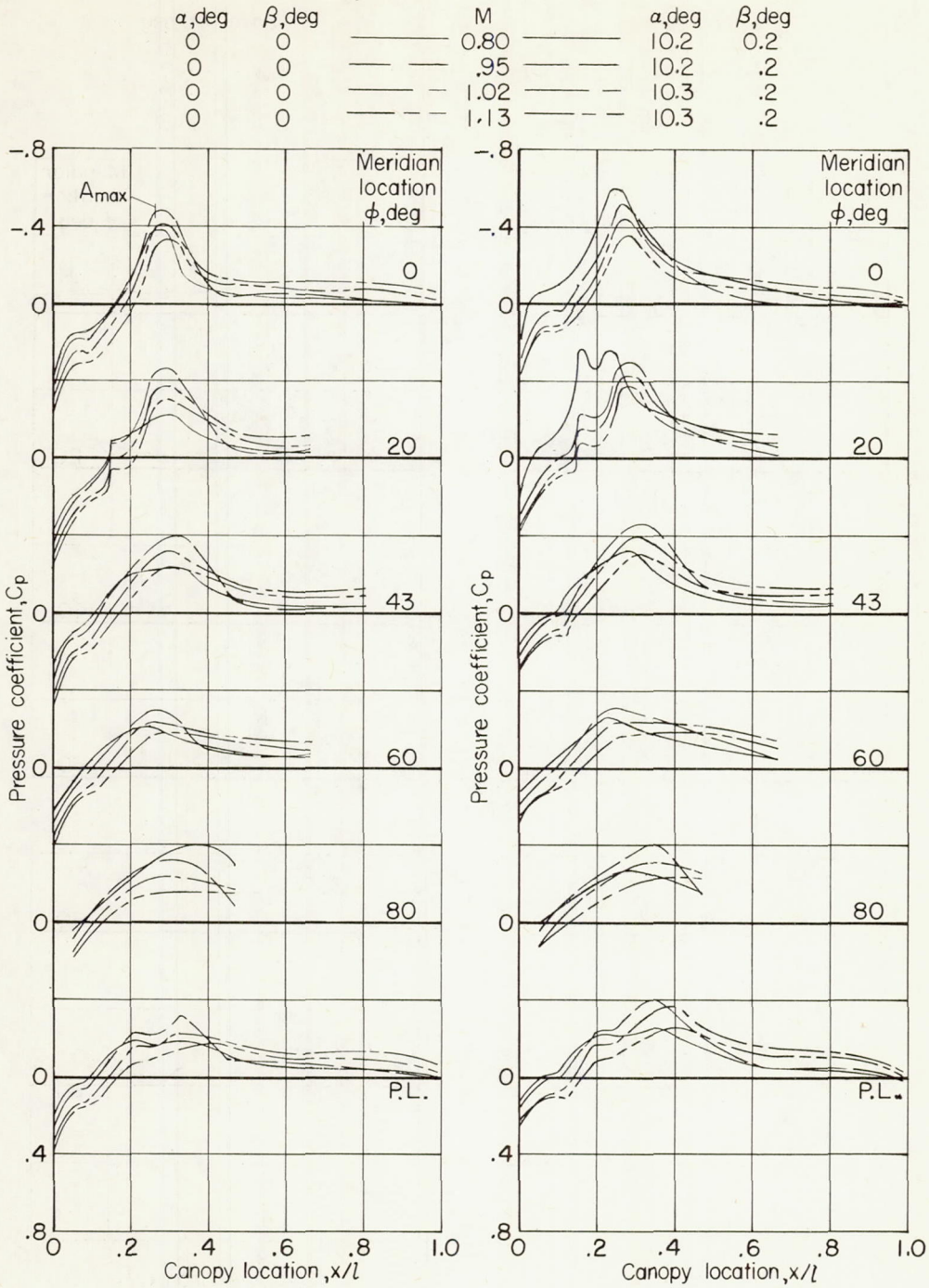
(c) Canopy 3.

Figure 7.- Continued.



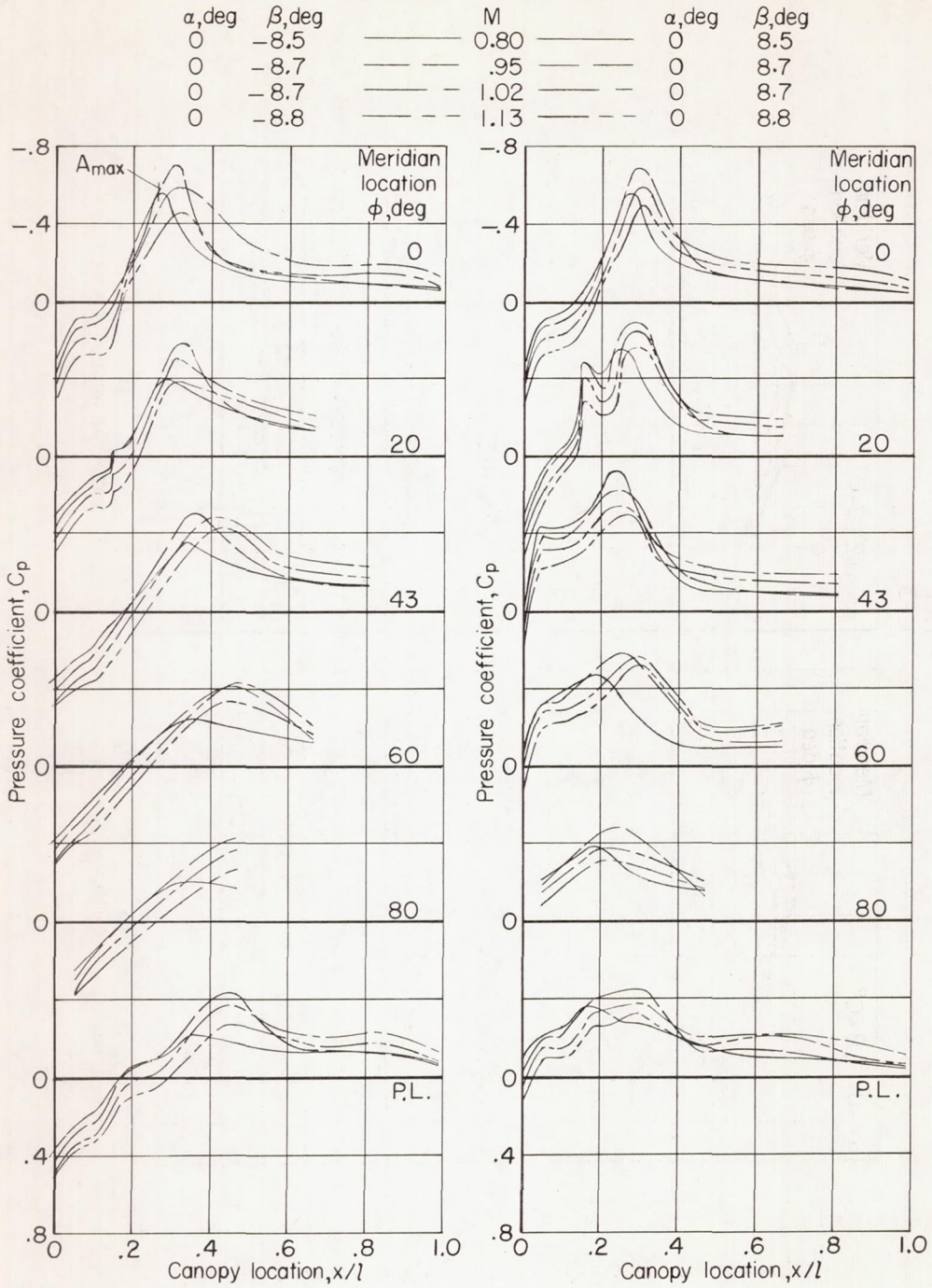
(c) Canopy 3. Concluded.

Figure 7.- Continued.



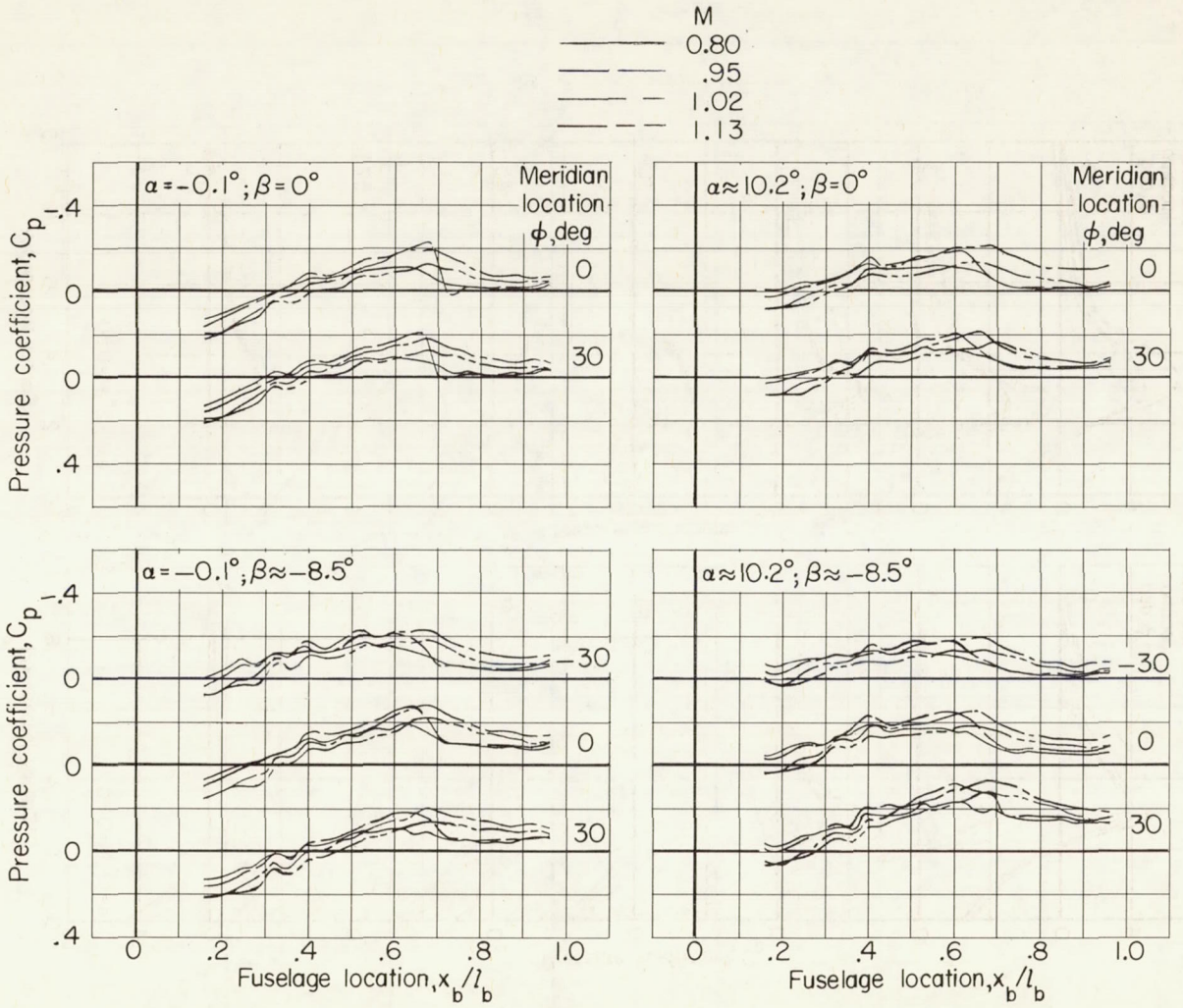
(d) Canopy 4.

Figure 7.- Continued.



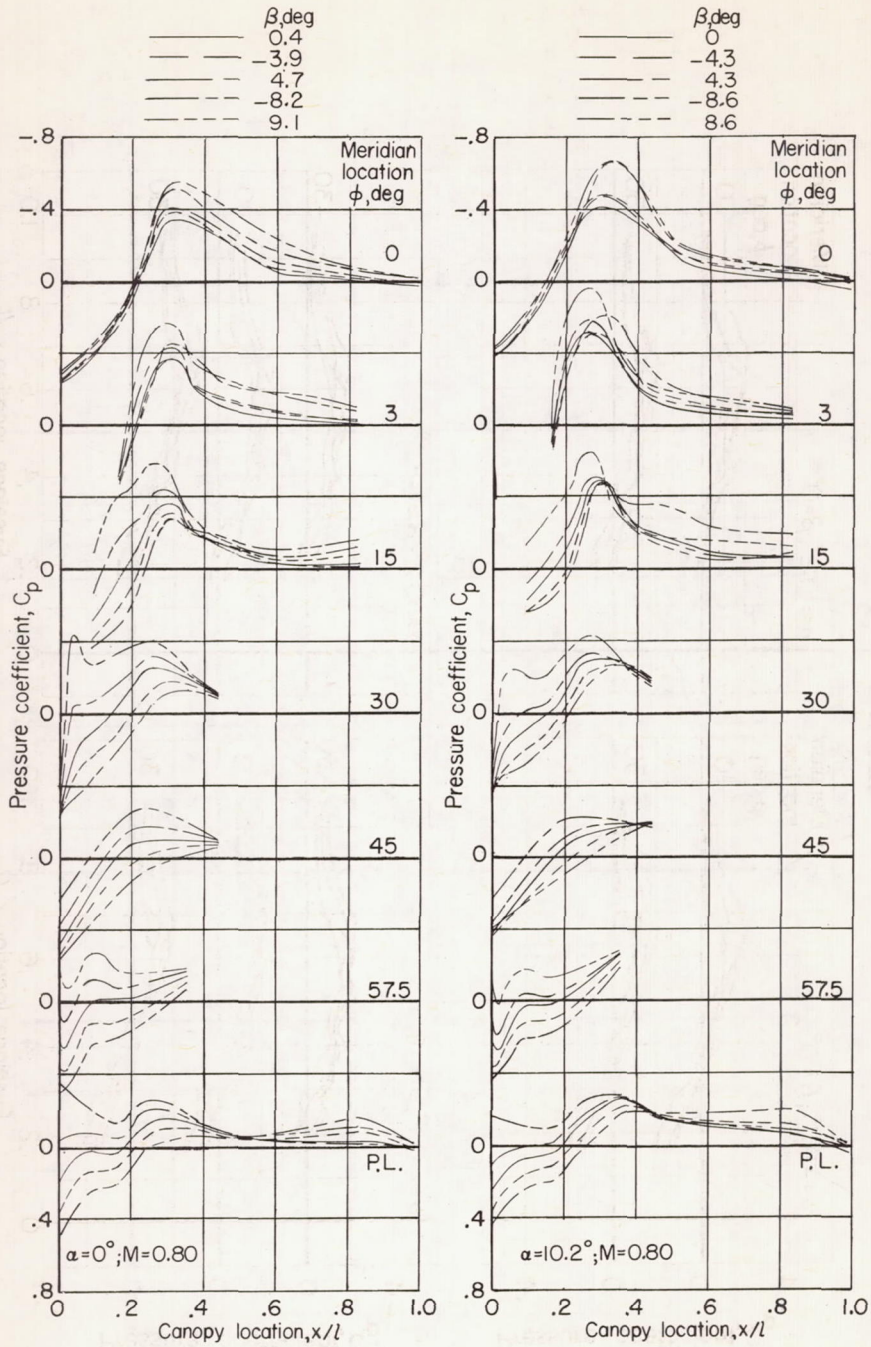
(d) Canopy 4. Concluded.

Figure 7.- Continued.



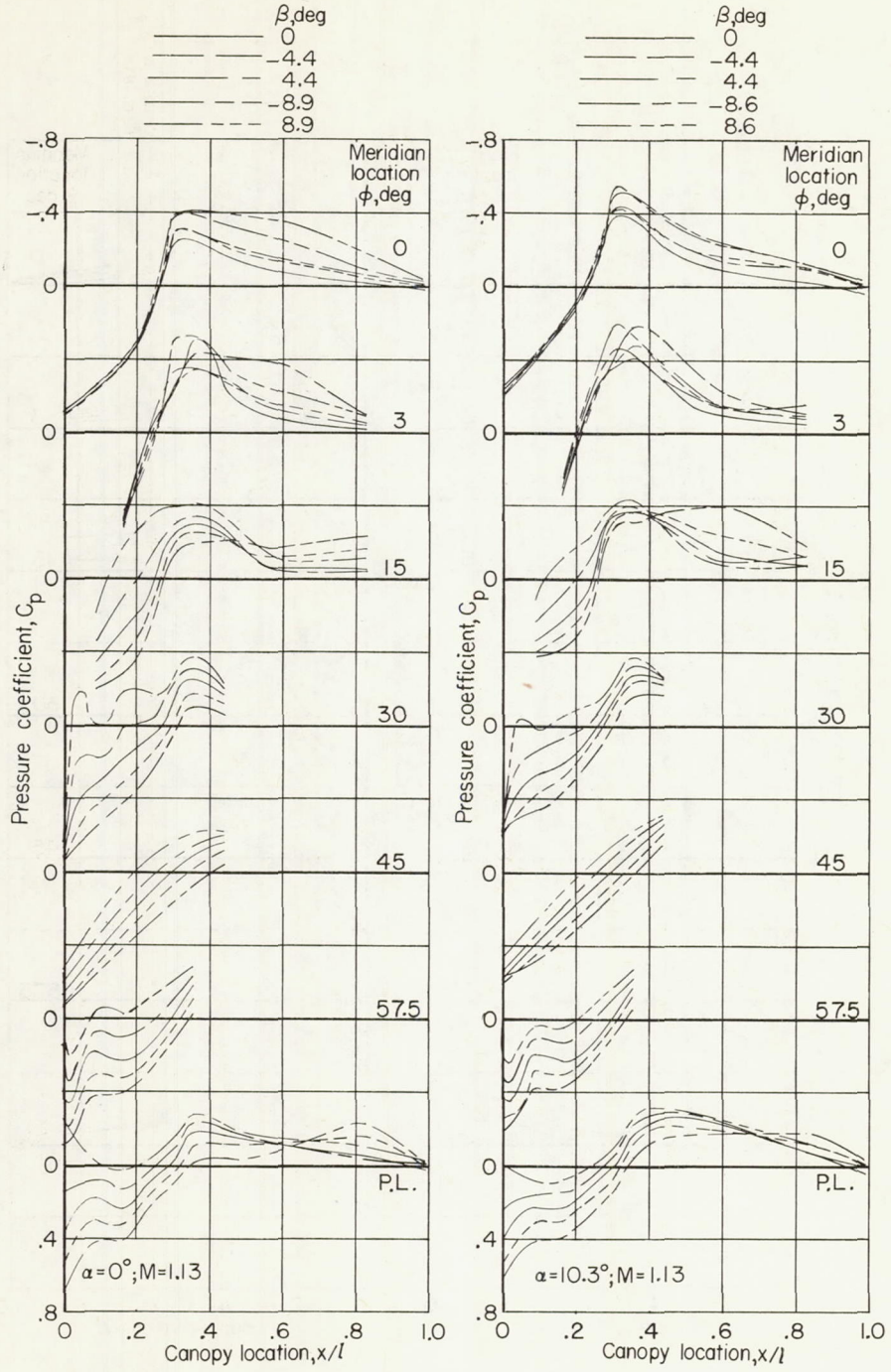
(e) Fuselage alone.

Figure 7.- Concluded.



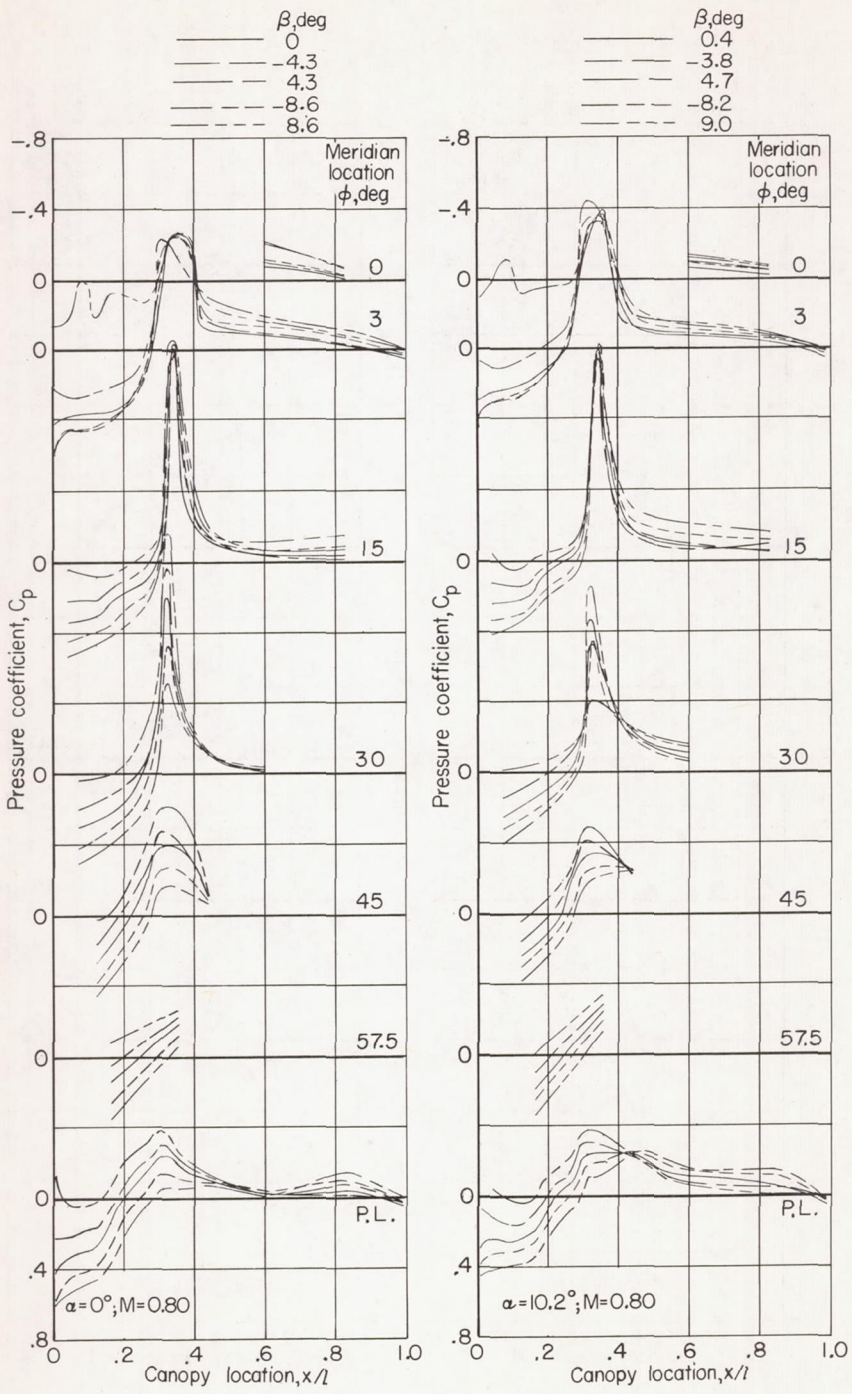
(a) Canopy 1.

Figure 8.- Effect of sideslip on pressure-coefficient distributions for all canopies and fuselage alone.



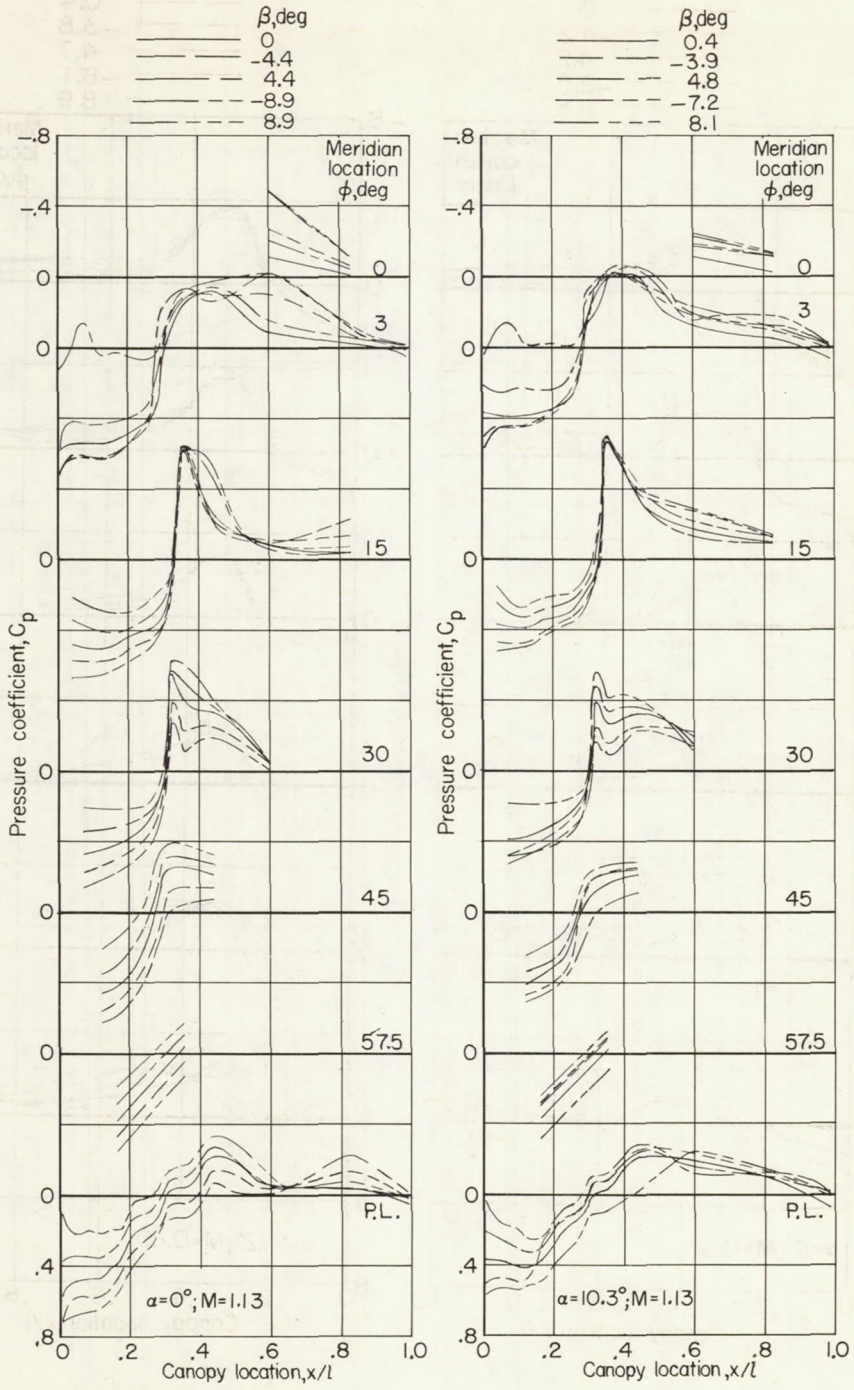
(a) Canopy 1. Concluded.

Figure 8.- Continued.



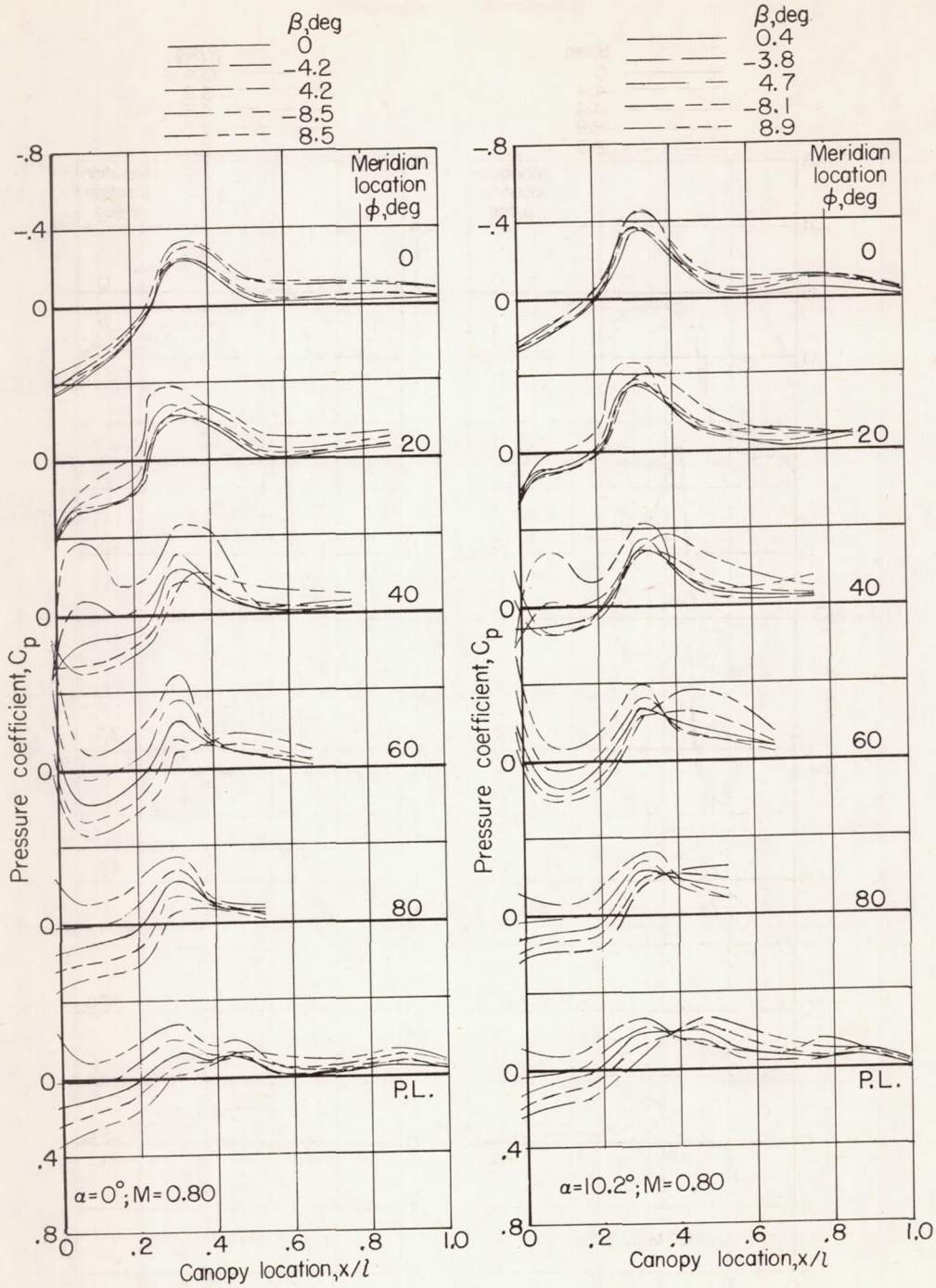
(b) Canopy 2.

Figure 8.- Continued.



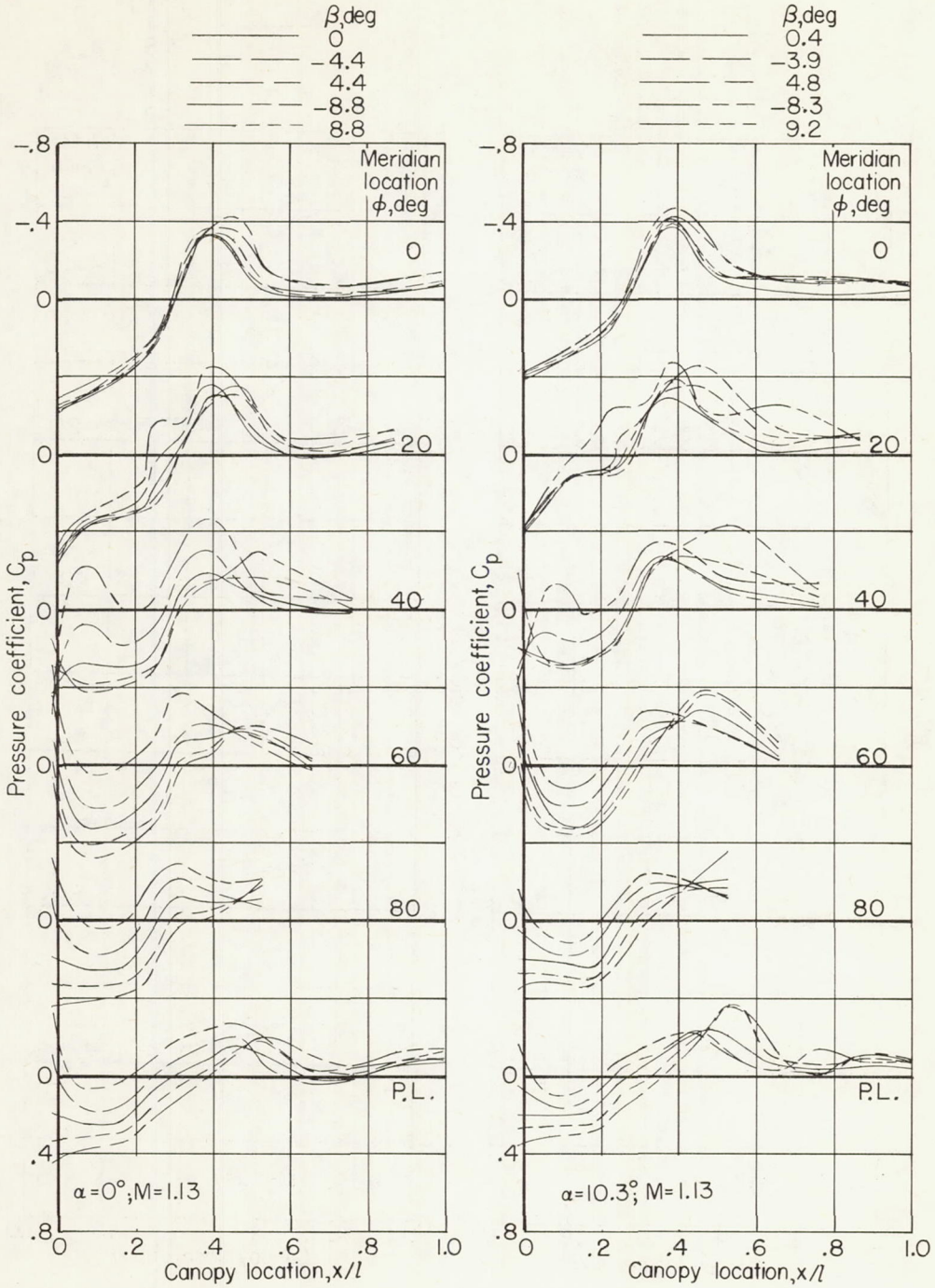
(b) Canopy 2. Concluded.

Figure 8.- Continued.



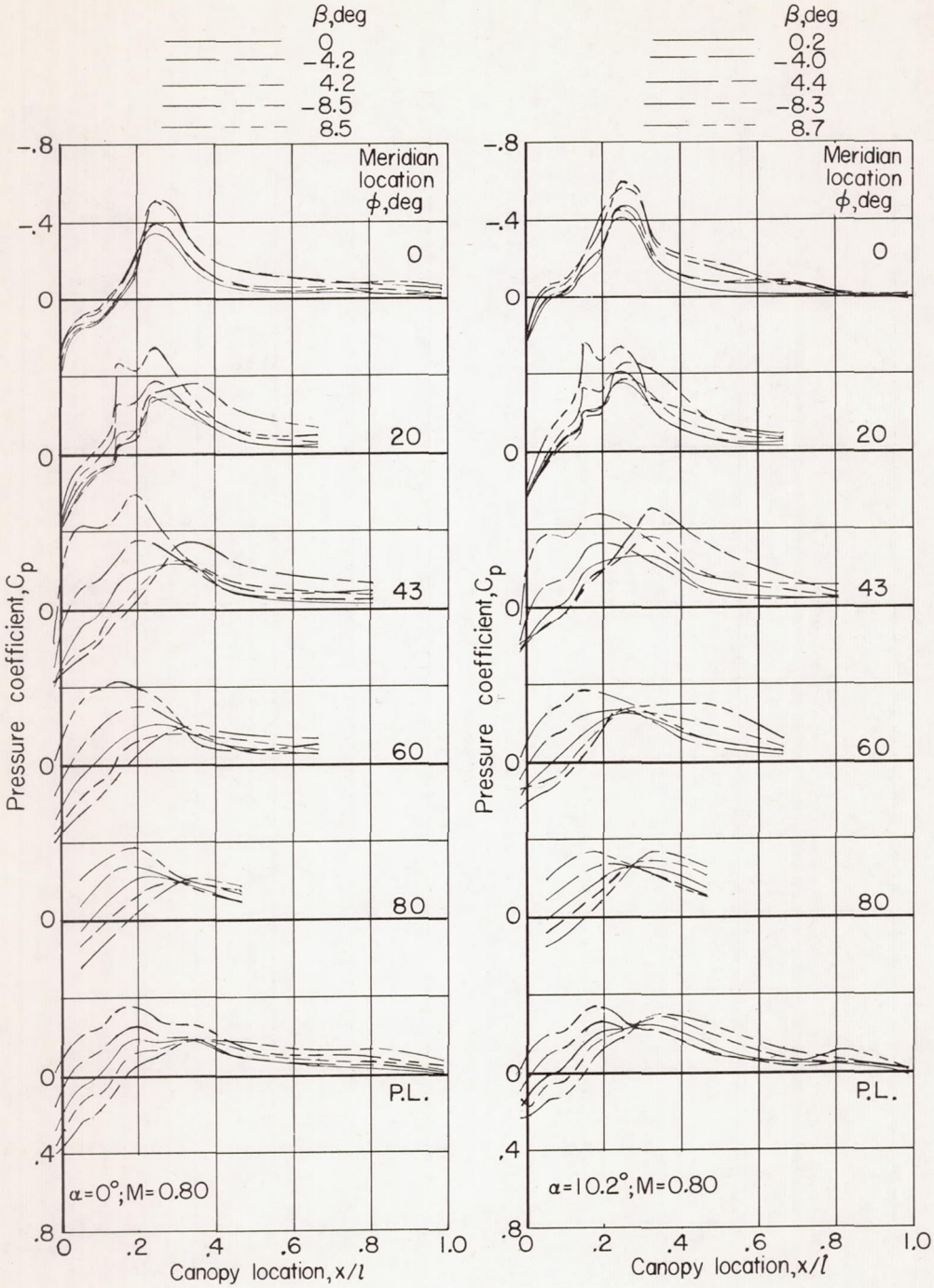
(c) Canopy 3.

Figure 8.- Continued.



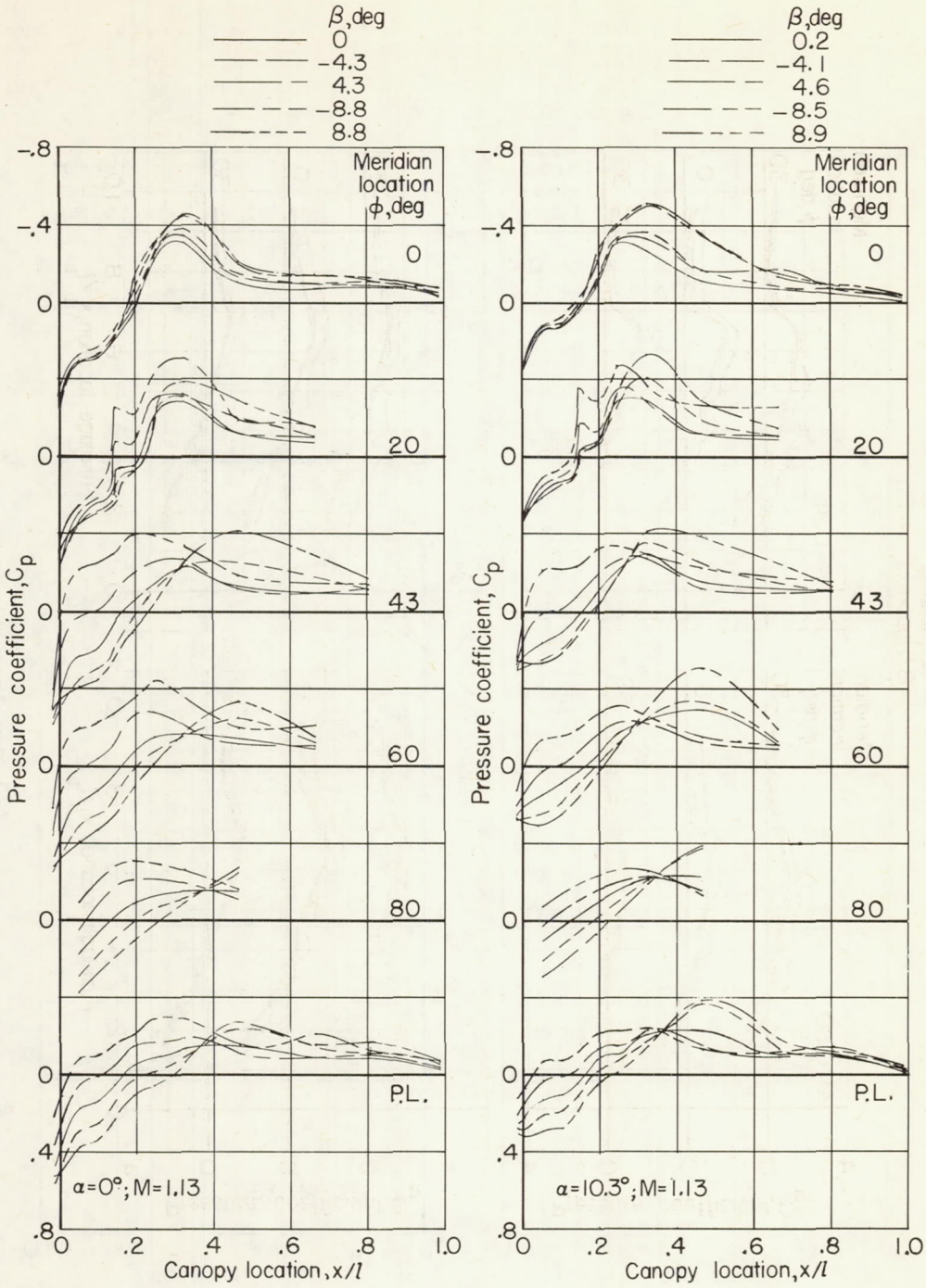
(c) Canopy 3. Concluded.

Figure 8.- Continued.



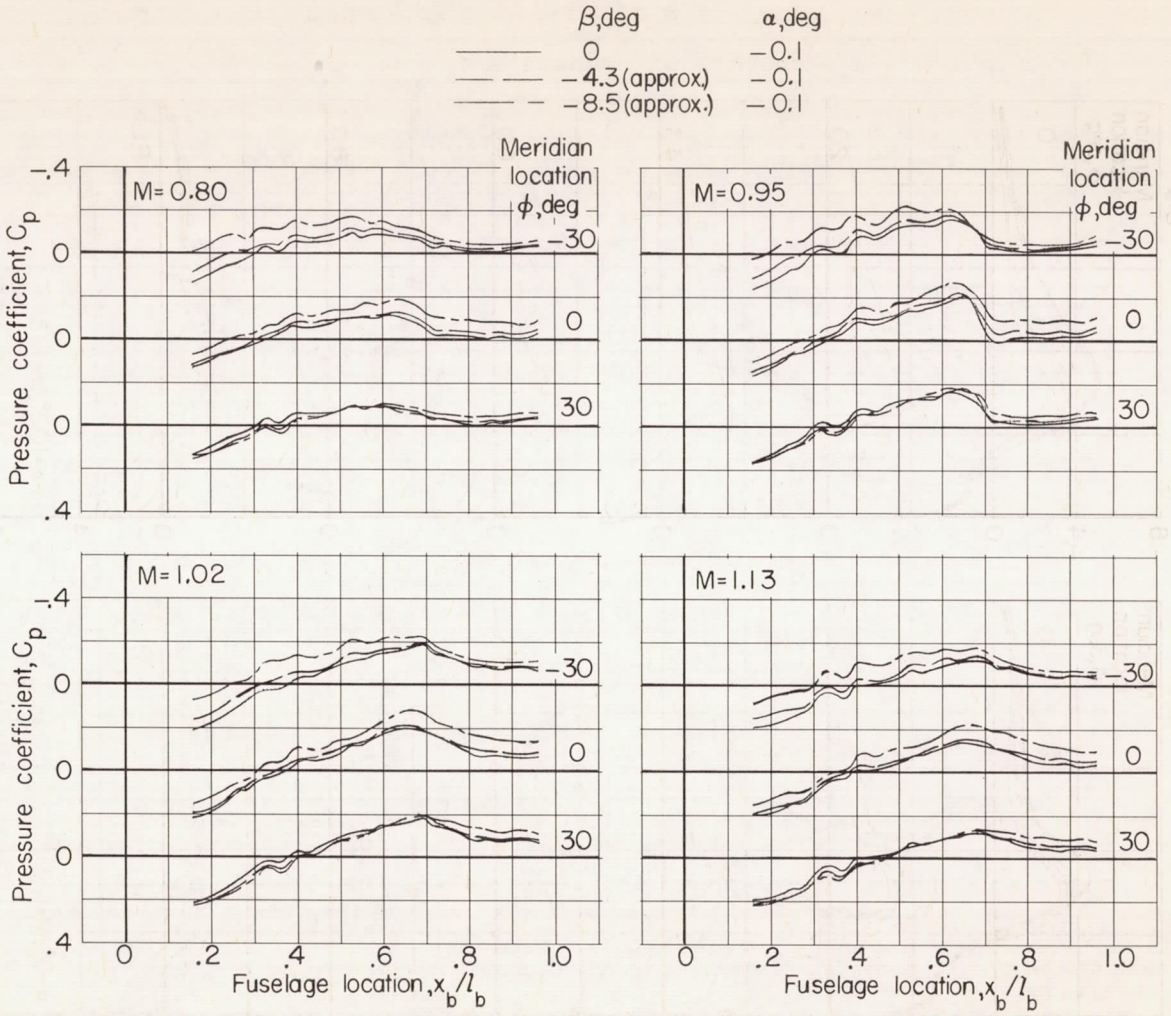
(d) Canopy 4.

Figure 8.- Continued.



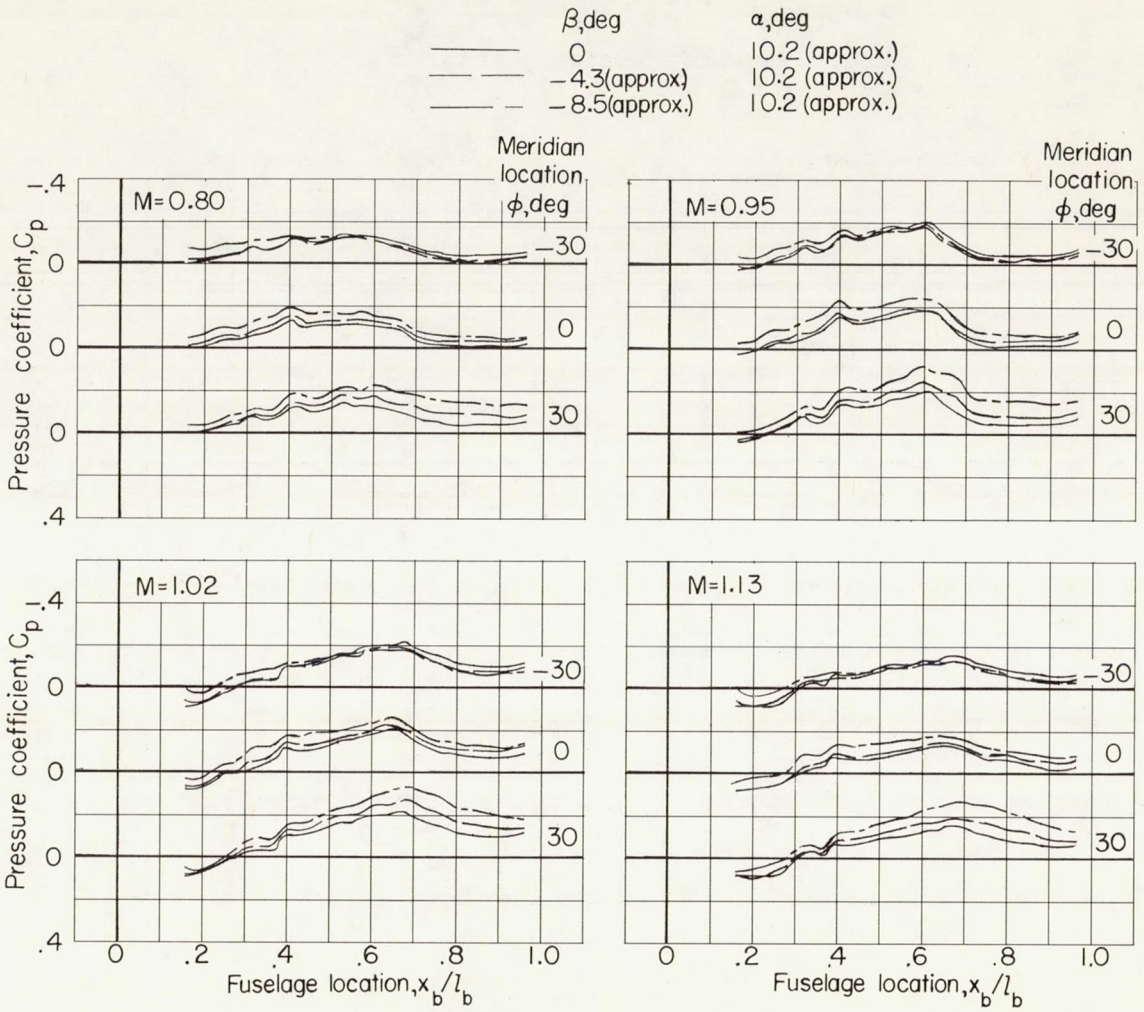
(d) Canopy 4. Concluded.

Figure 8.- Continued.



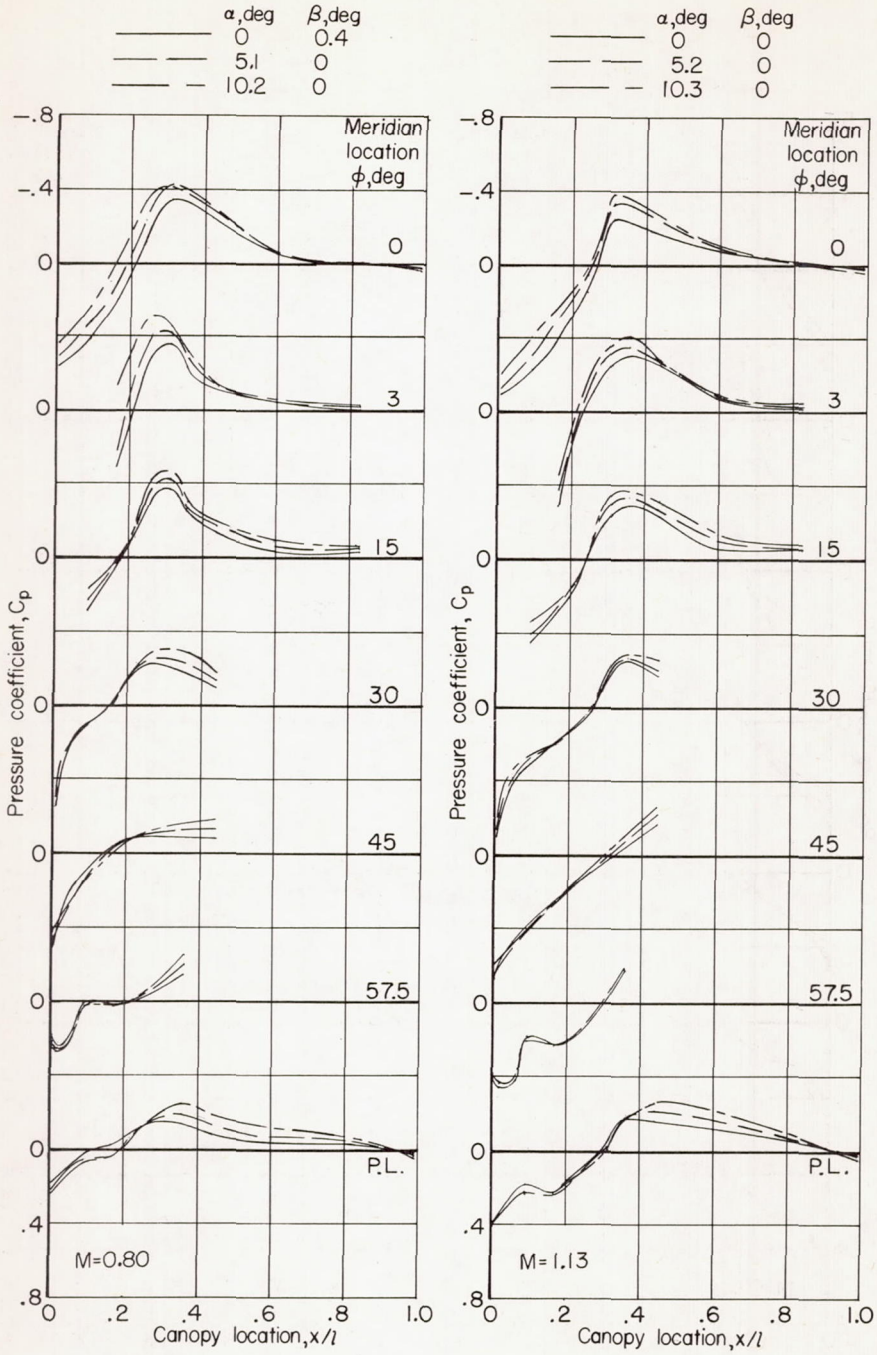
(e) Fuselage alone.

Figure 8.- Continued.



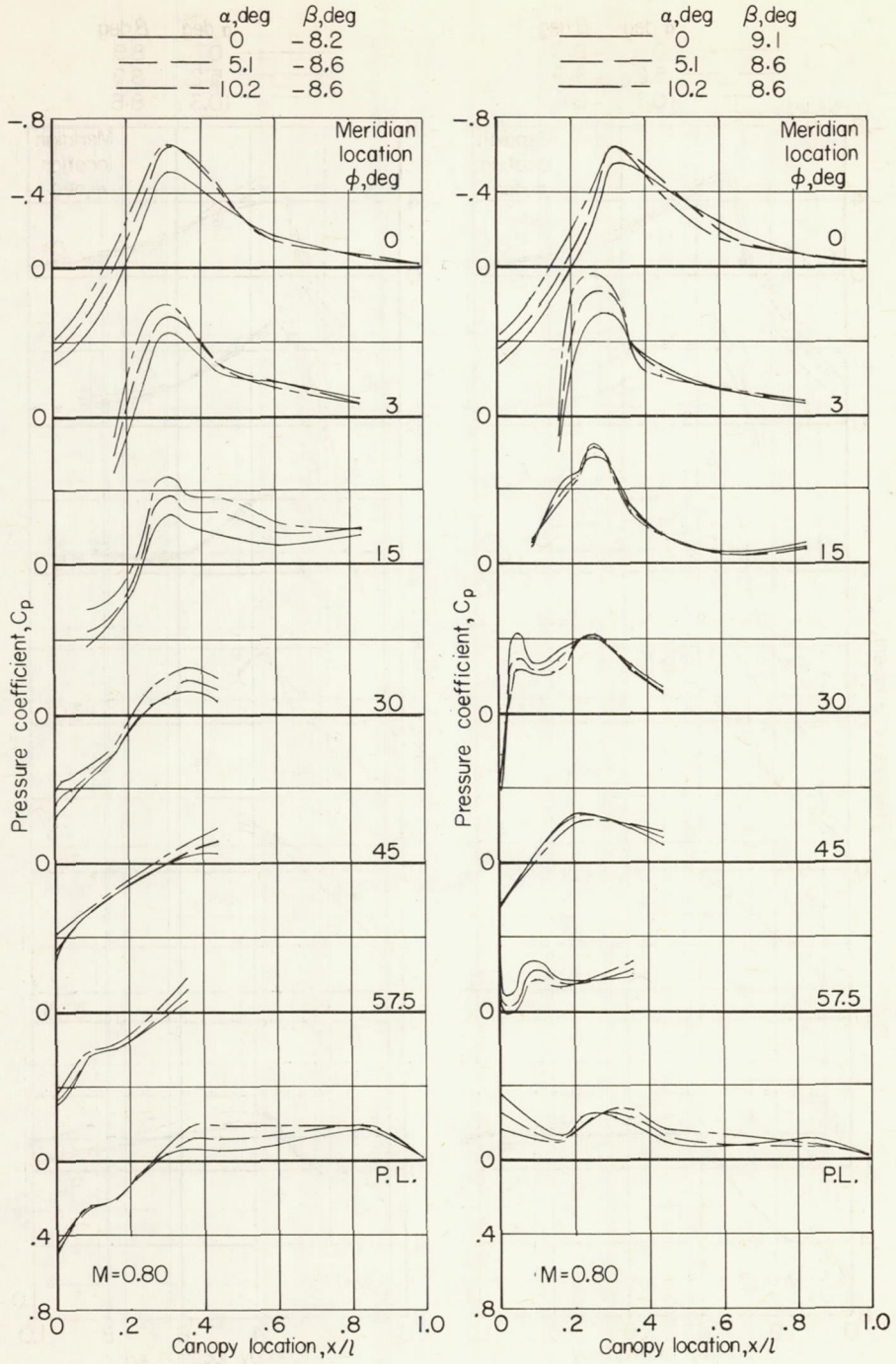
(e) Fuselage alone. Concluded.

Figure 8.- Concluded.



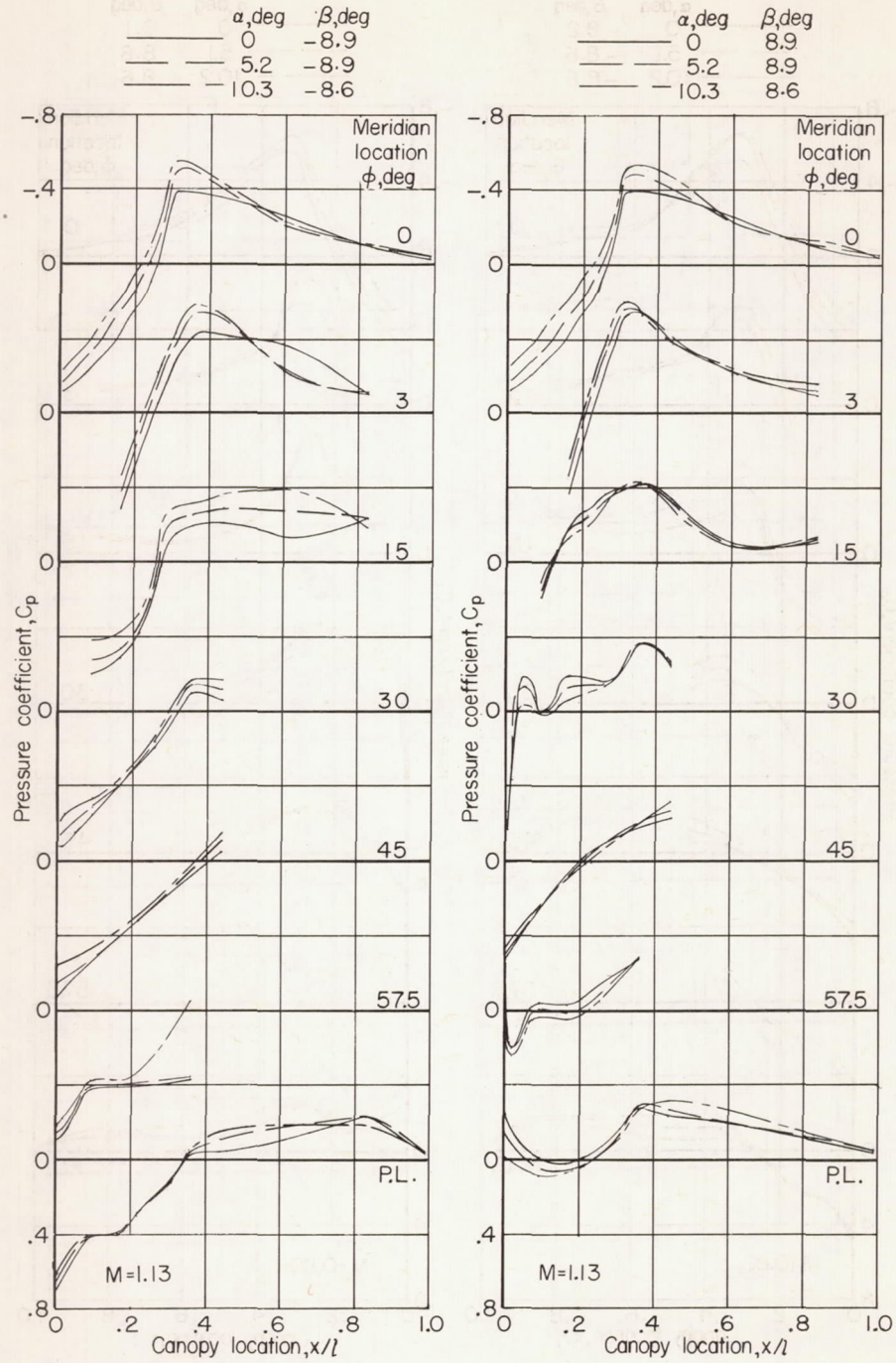
(a) Canopy 1.

Figure 9.- Effect of angle of attack on pressure-coefficient distributions for all canopies and fuselage alone.



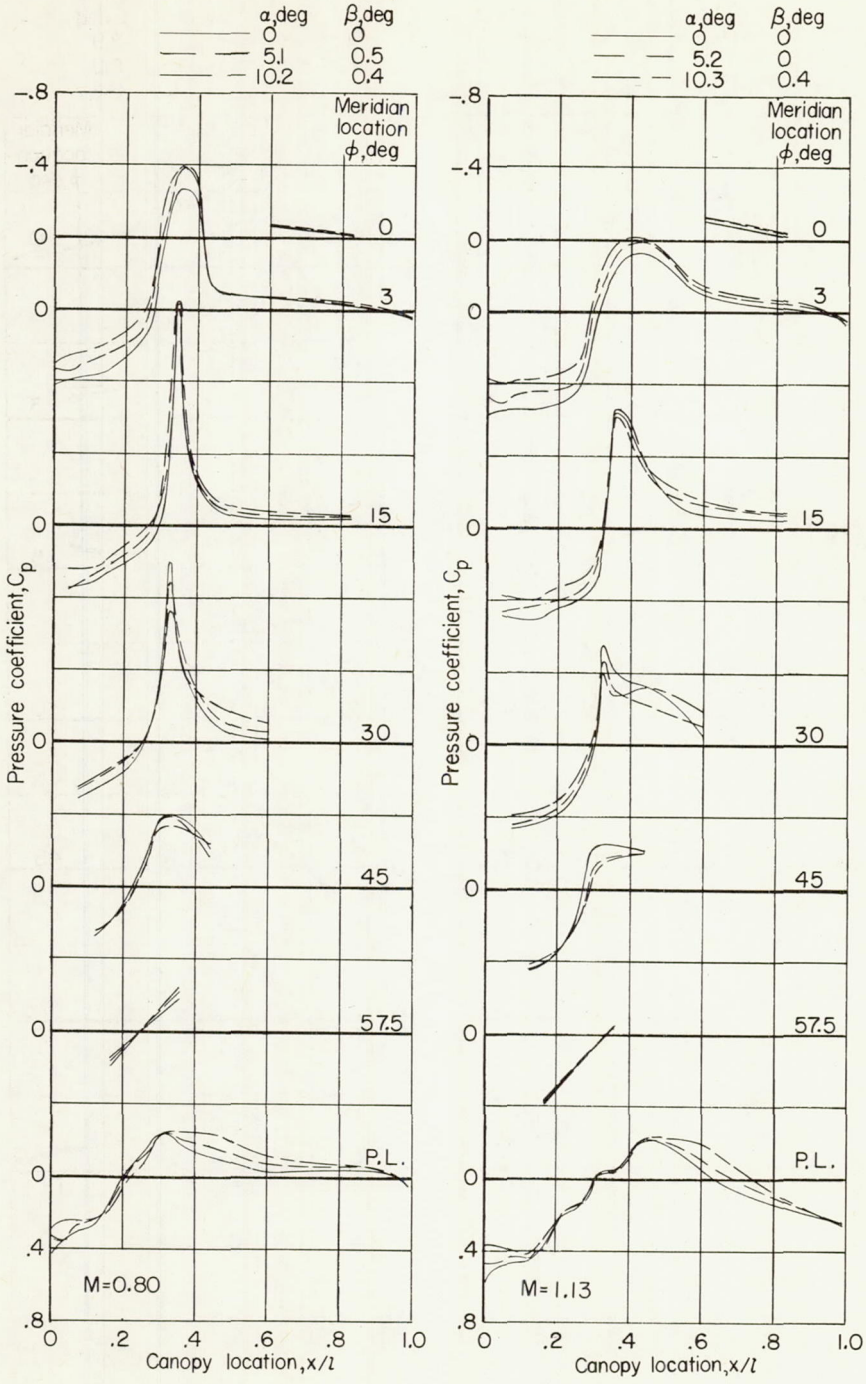
(a) Canopy 1. Continued.

Figure 9.- Continued.



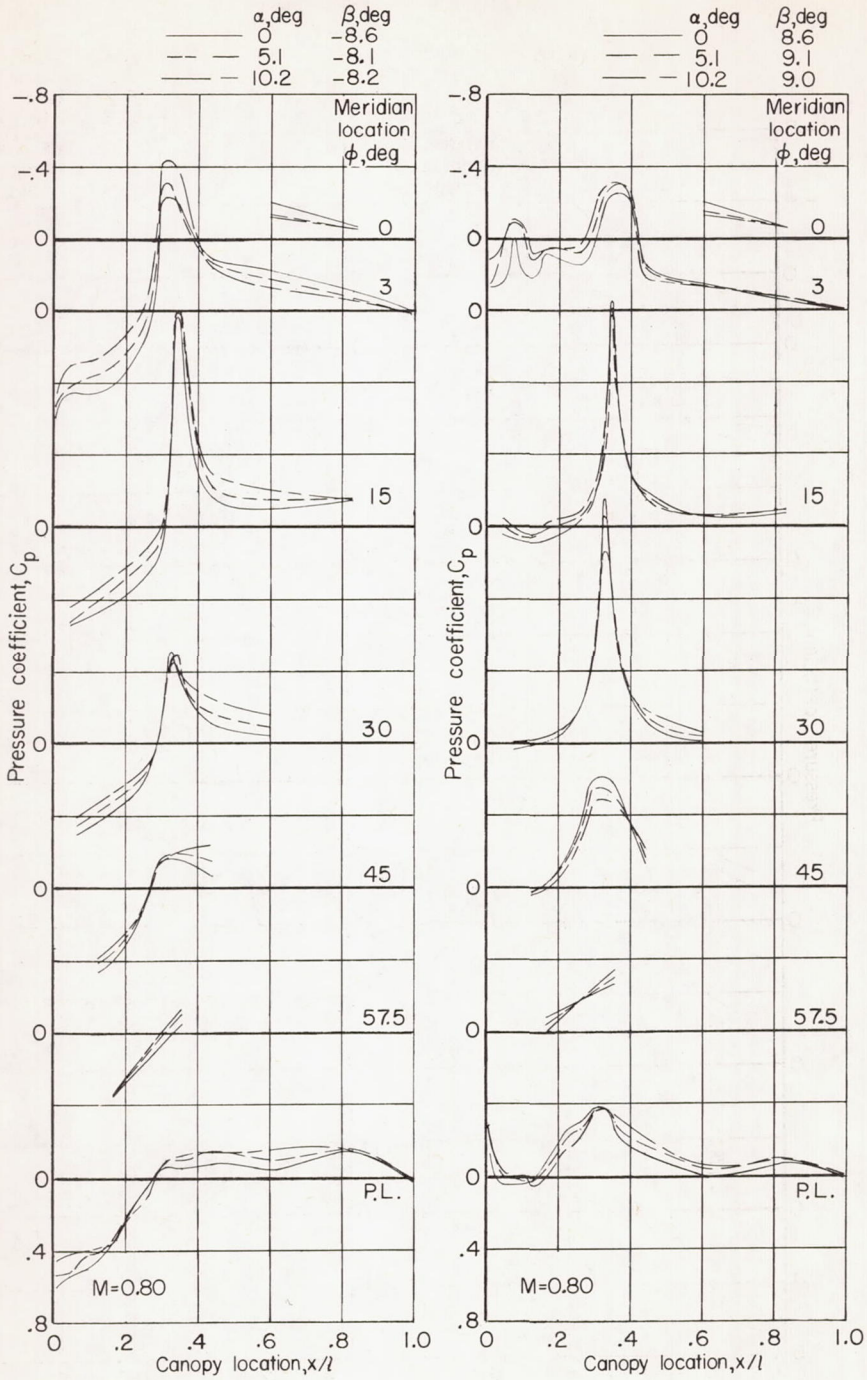
(a) Canopy 1. Concluded.

Figure 9.- Continued.



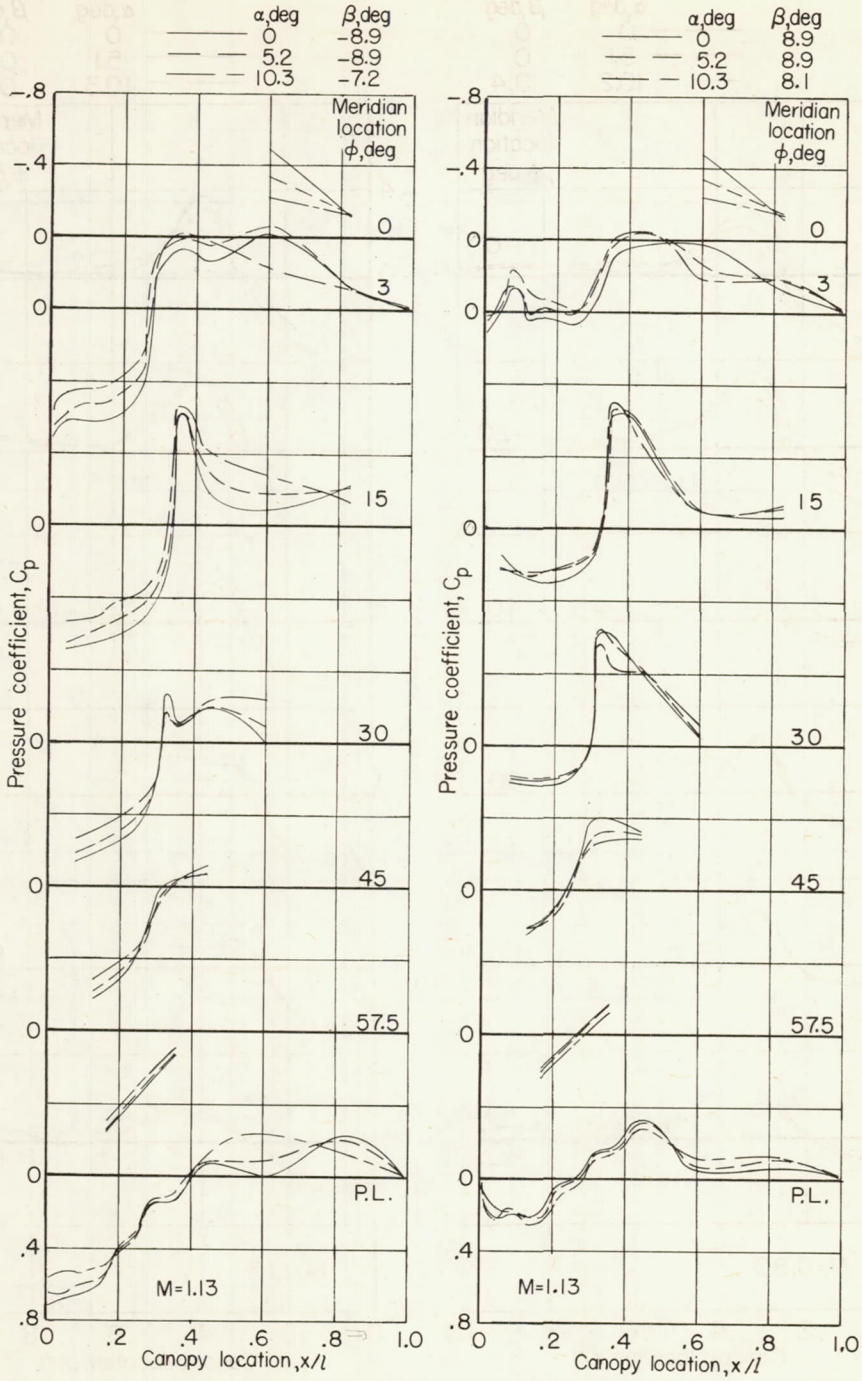
(b) Canopy 2.

Figure 9.- Continued.



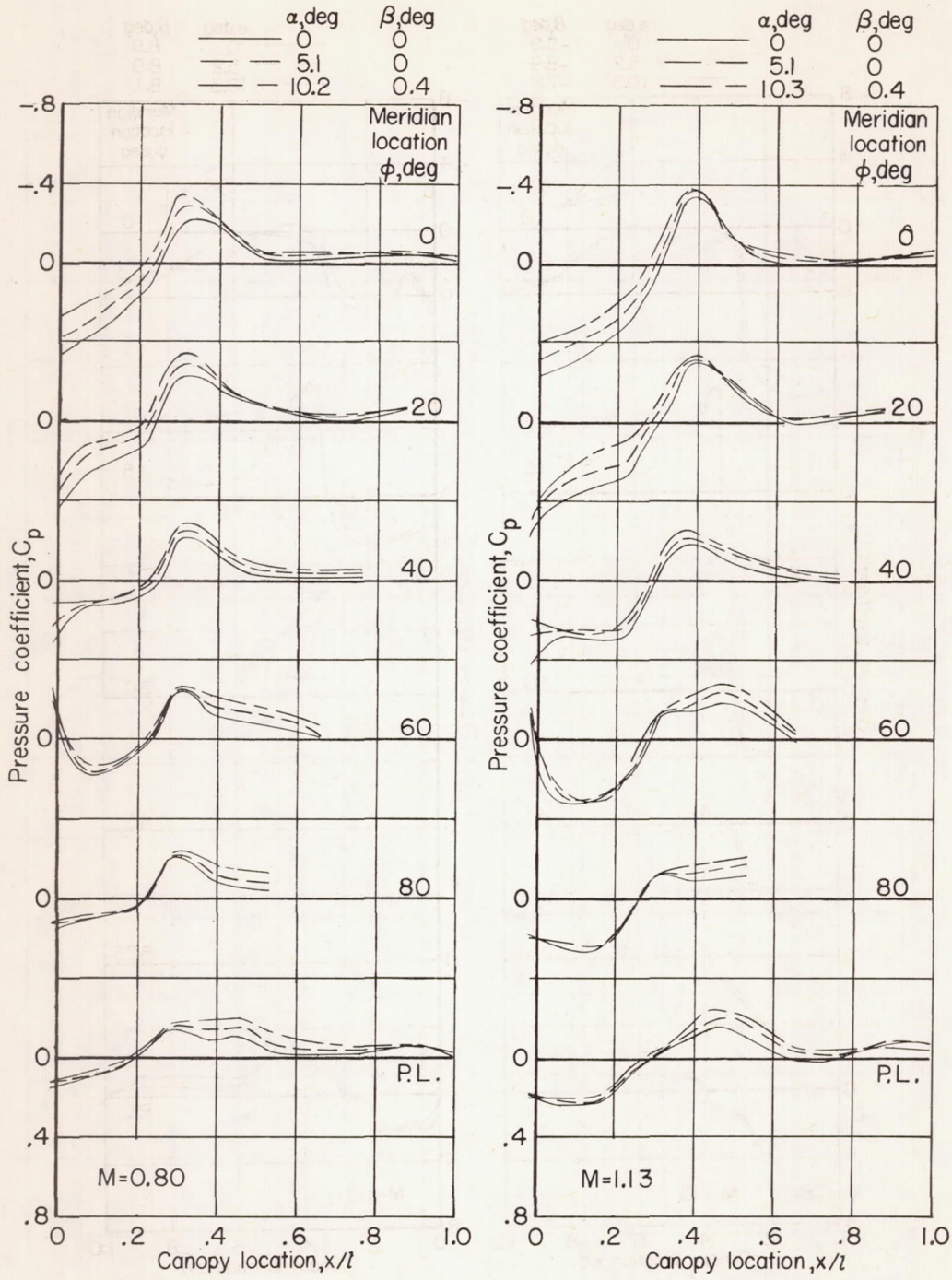
(b) Canopy 2. Continued.

Figure 9.- Continued.



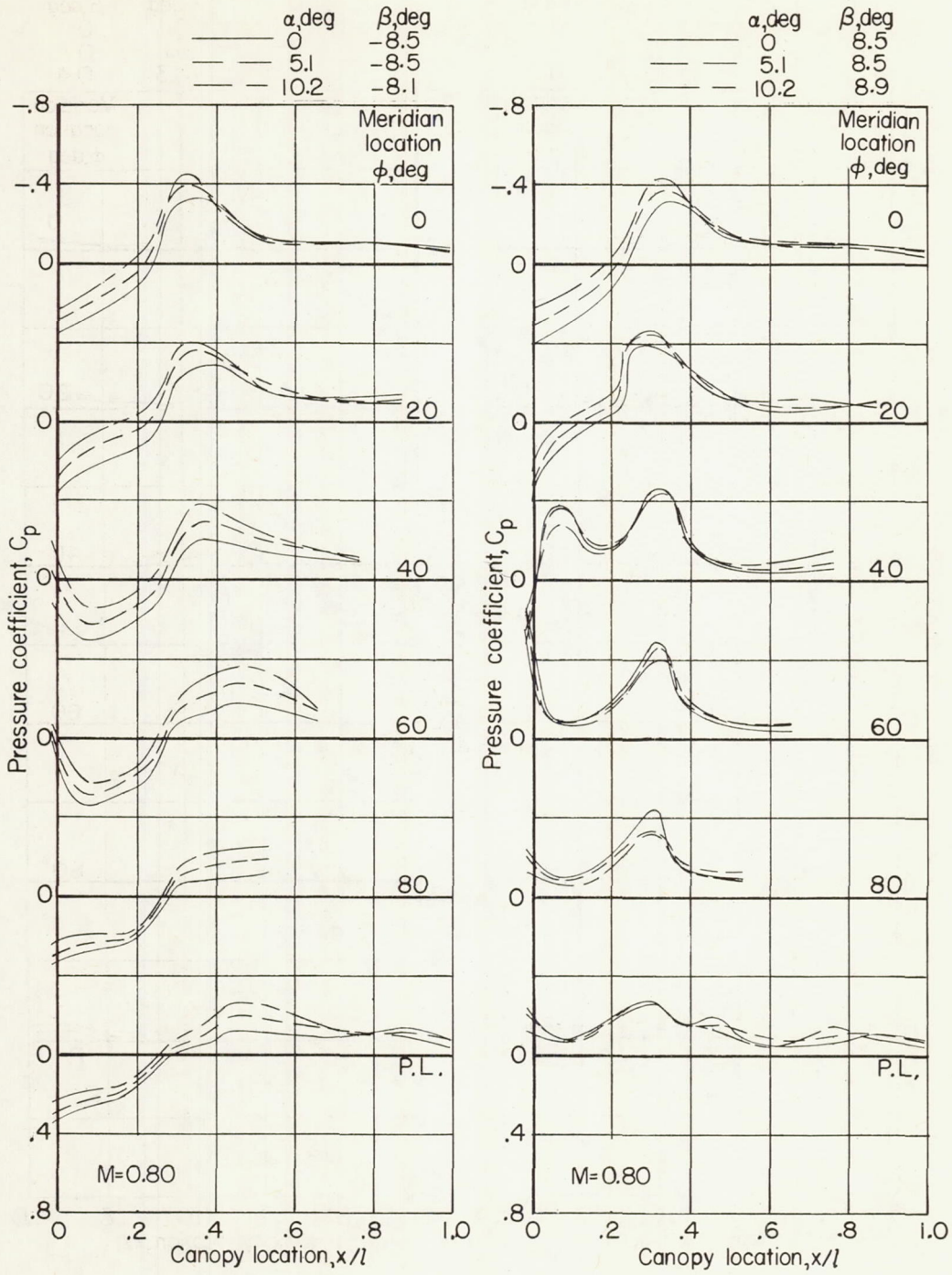
(b) Canopy 2. Concluded.

Figure 9.- Continued.



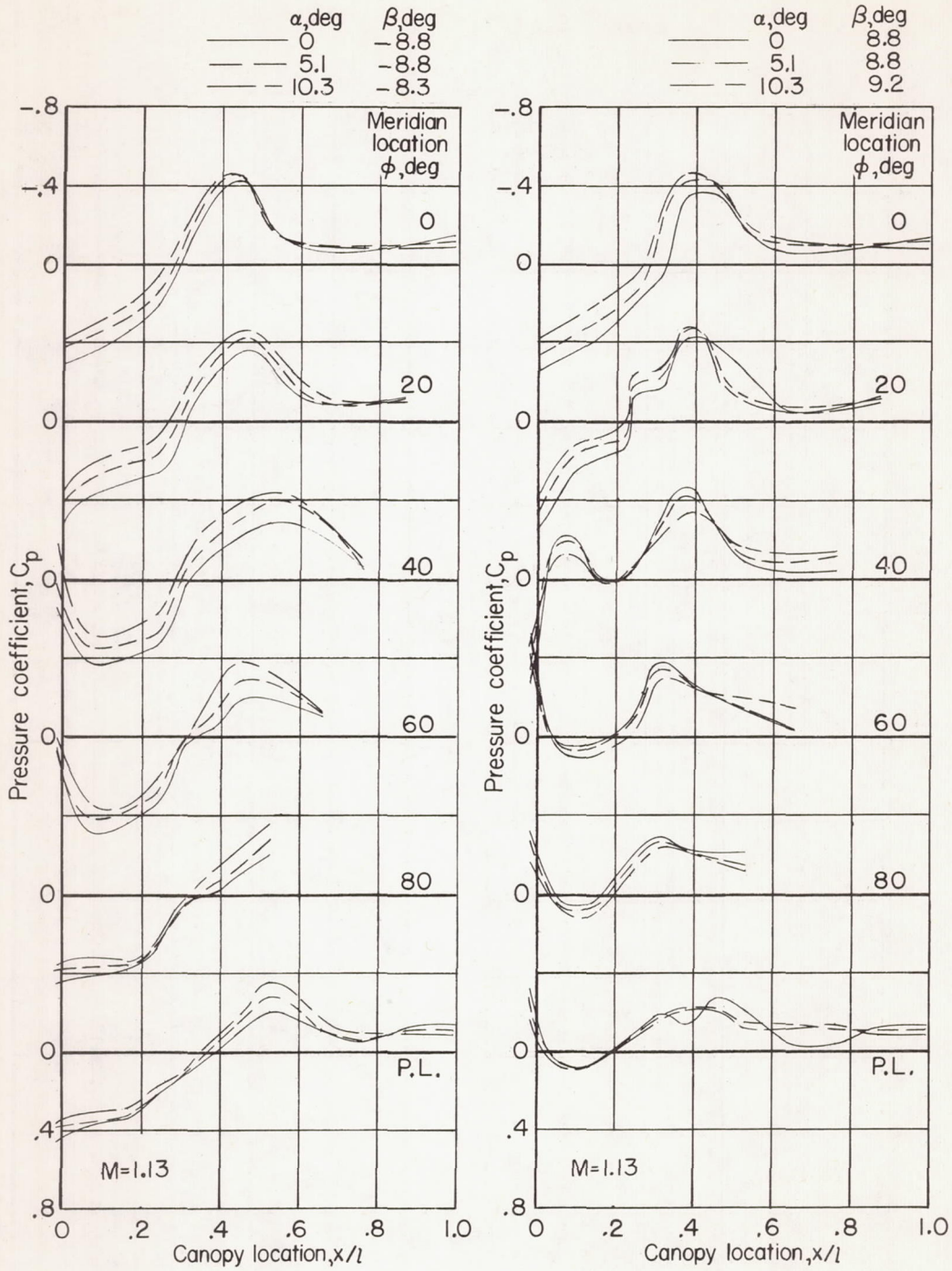
(c) Canopy 3.

Figure 9.- Continued.



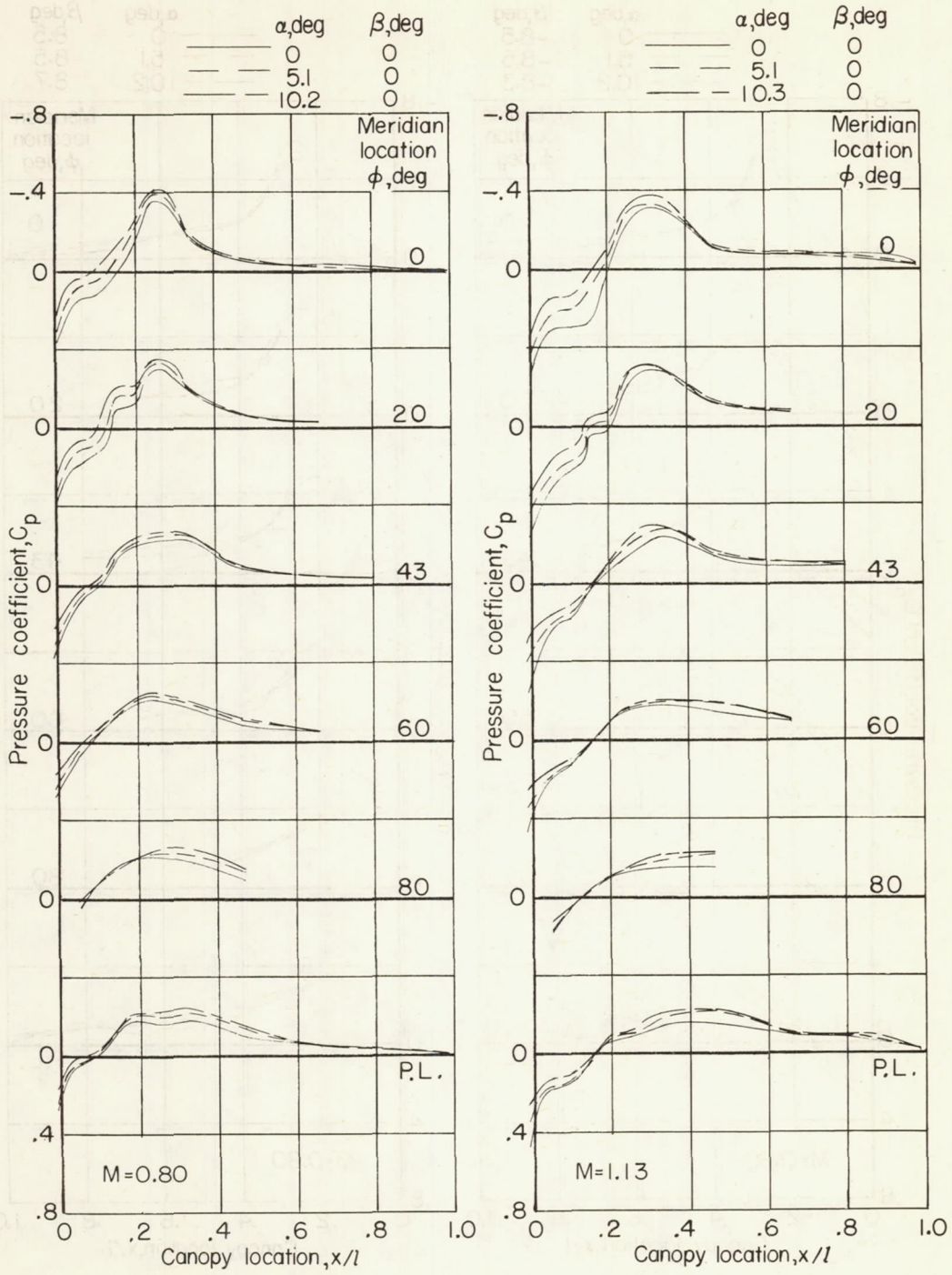
(c) Canopy 3. Continued.

Figure 9.- Continued.



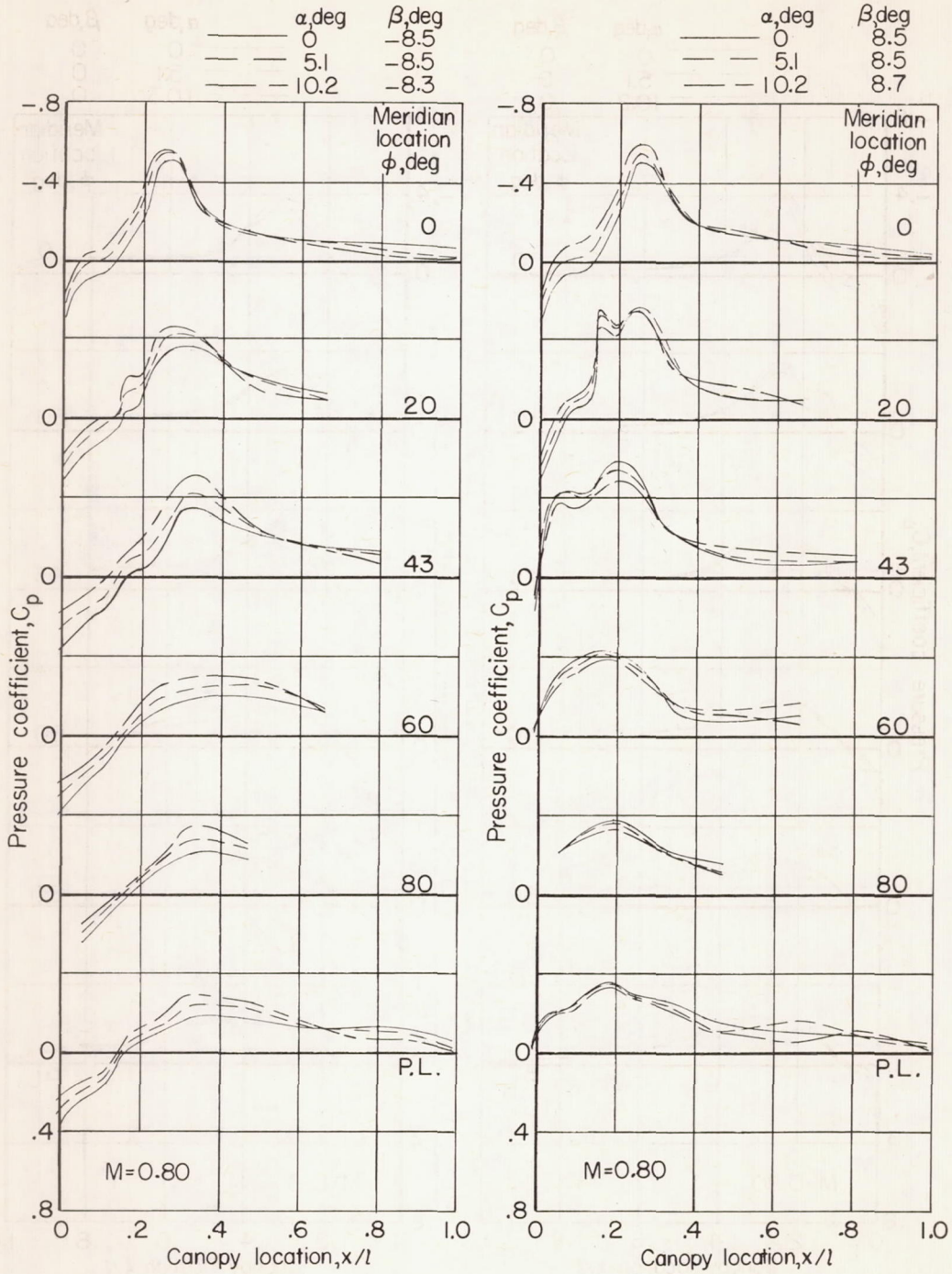
(c) Canopy 3. Concluded.

Figure 9.- Continued.



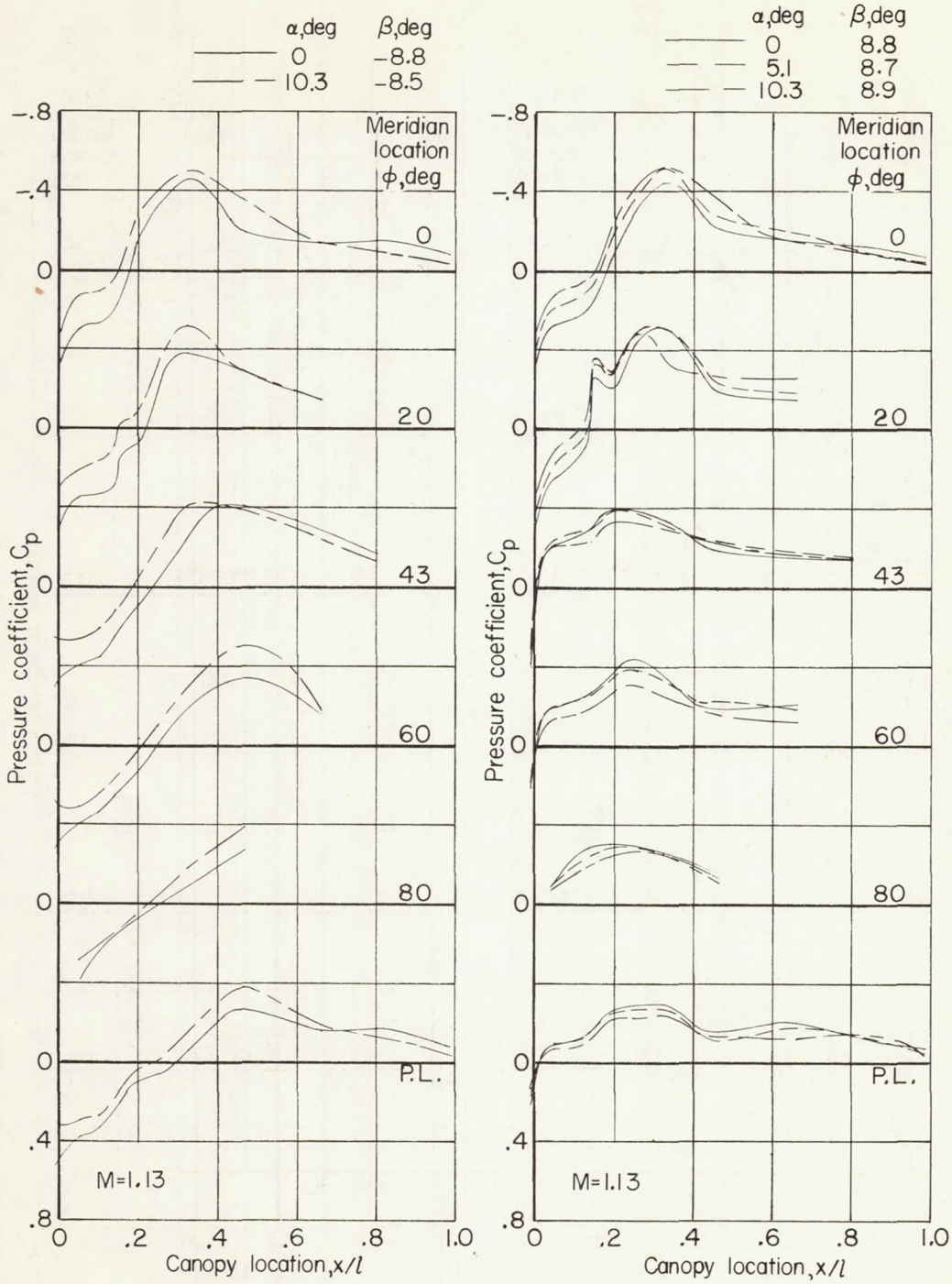
(d) Canopy 4.

Figure 9.- Continued.



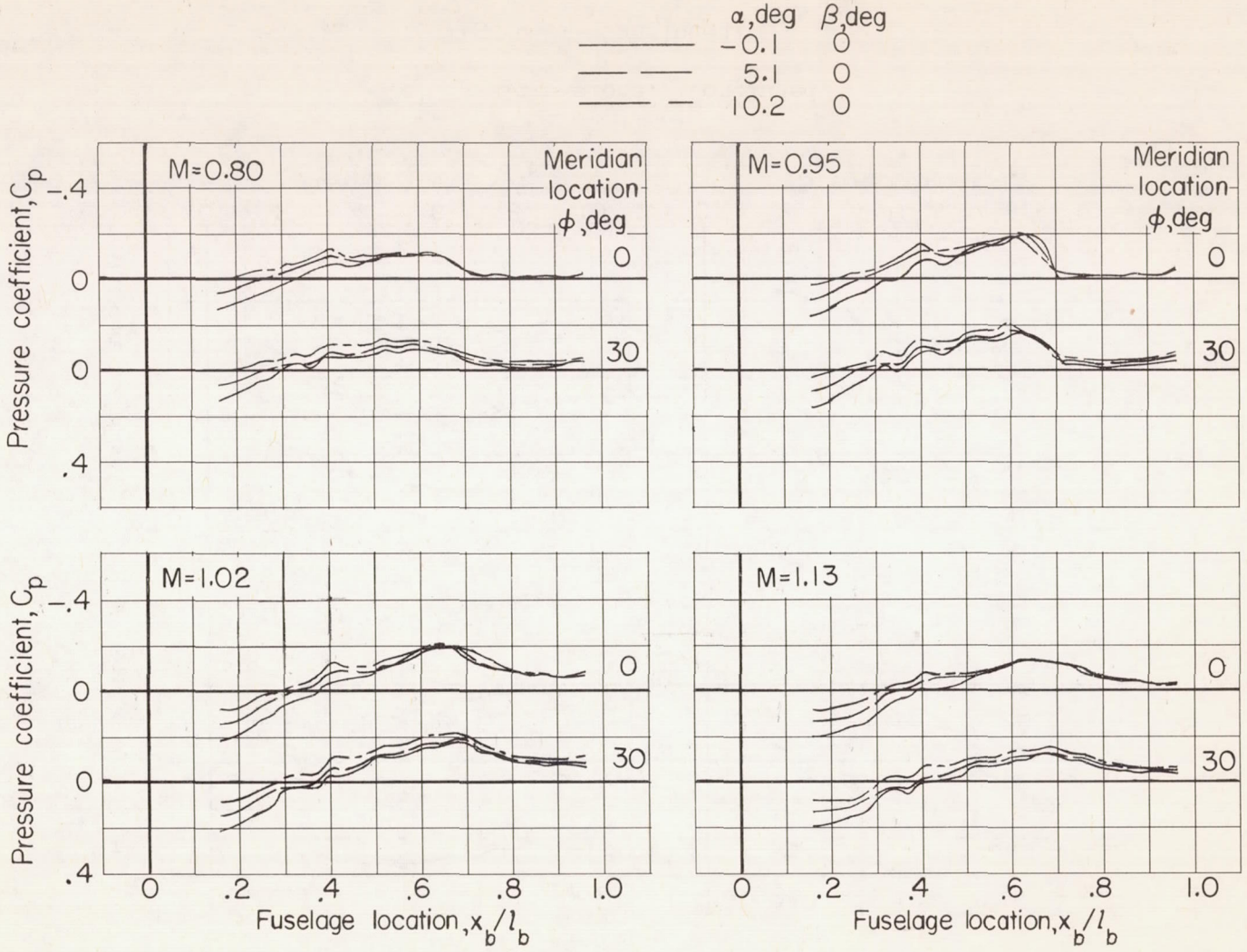
(d) Canopy 4. Continued.

Figure 9.- Continued.



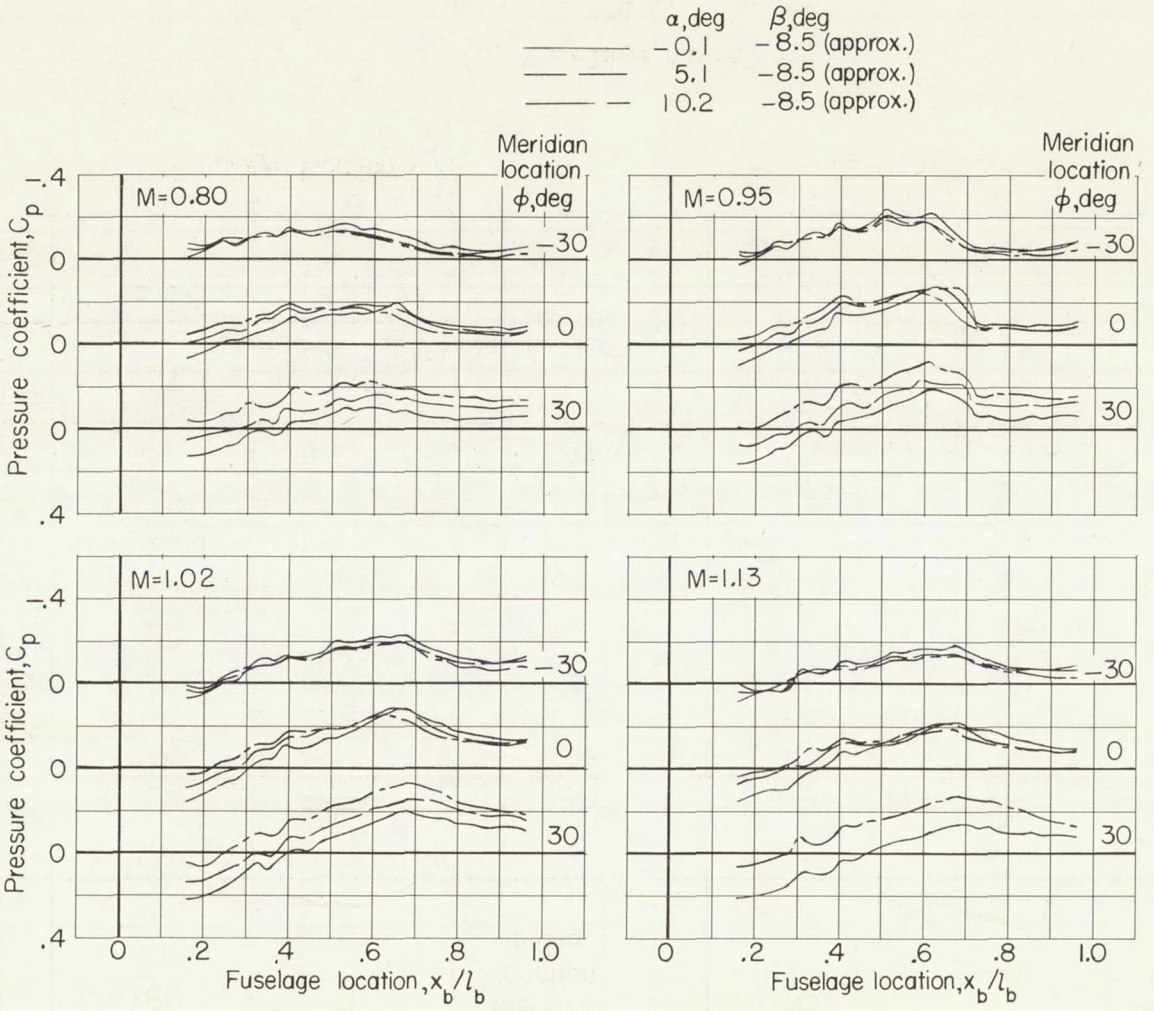
(d) Canopy 4. Concluded.

Figure 9.- Continued.



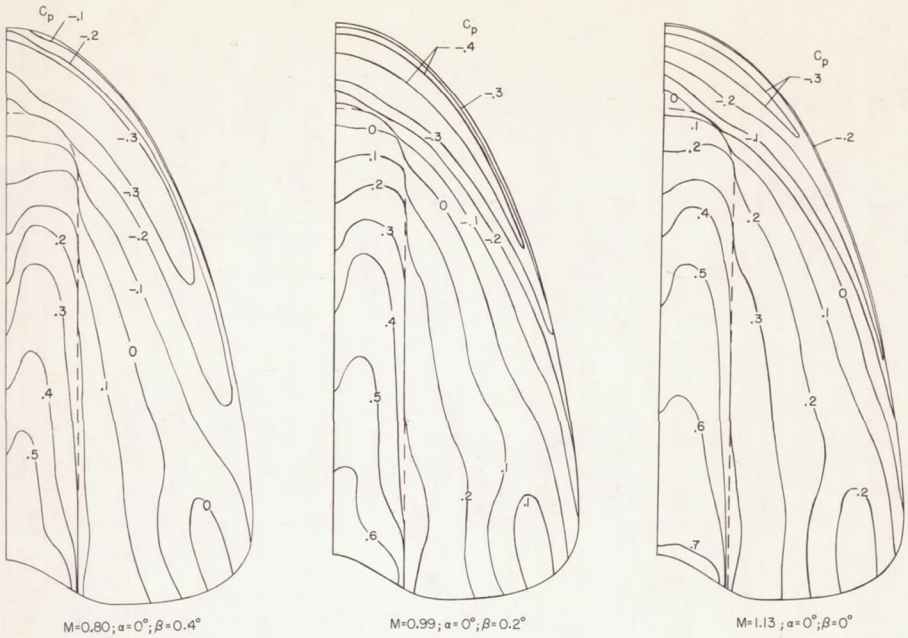
(e) Fuselage alone.

Figure 9.- Continued.

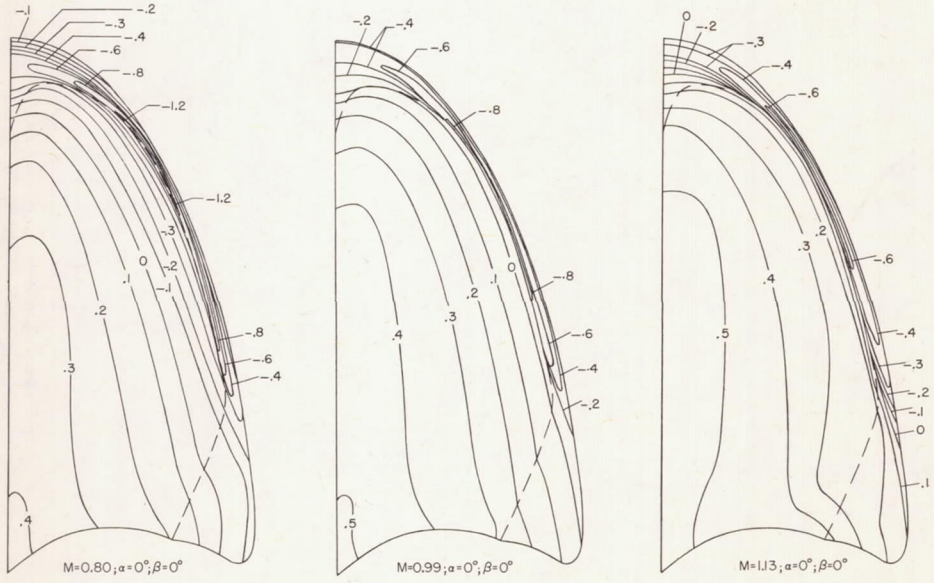


(e) Fuselage alone. Concluded.

Figure 9.- Concluded.

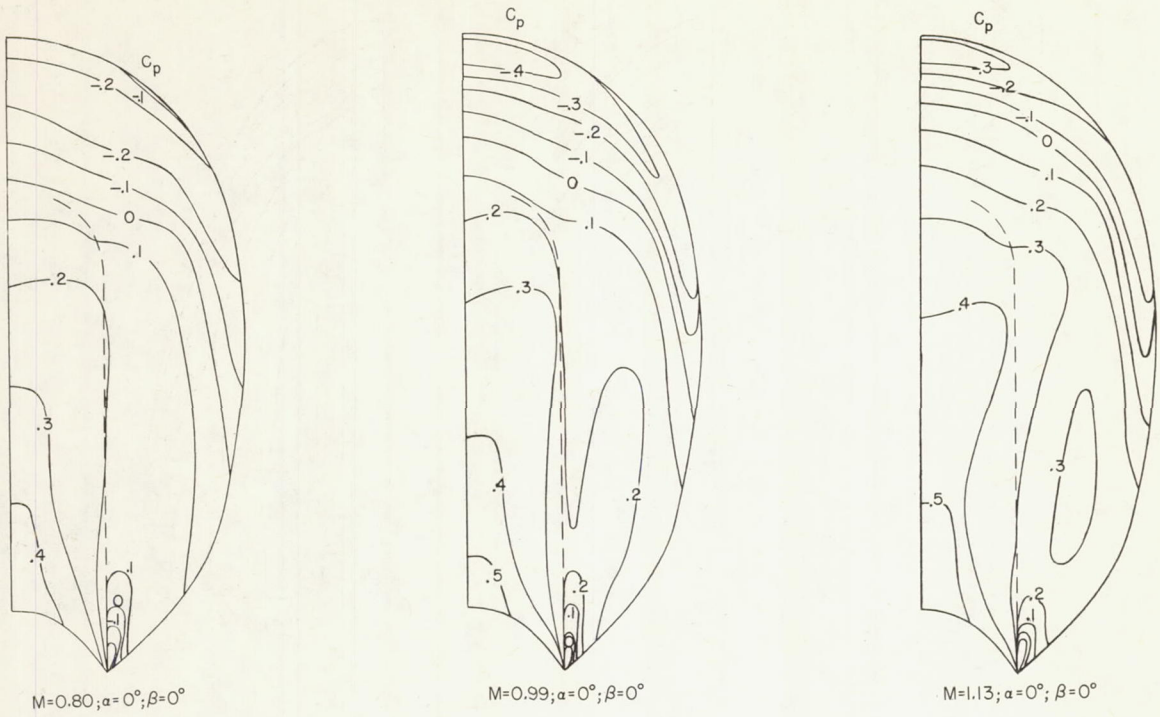


(a) Large flat-windshield canopy 1.

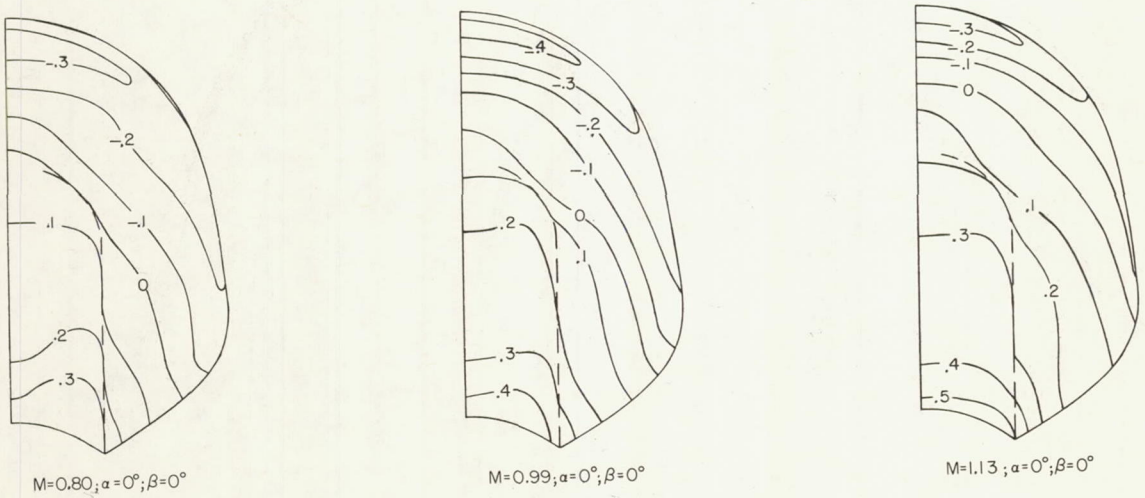


(b) Large vee-windshield canopy 2.

Figure 10.- Constant-pressure-coefficient contours on one-half the frontal projections of all canopies tested. M = 0.80, 0.99, and 1.13. (Dashed lines indicate windshield edges.)



(c) Forward-located flat-windshield canopy 3.



(d) Rearward-located flat-windshield canopy 4.

Figure 10.- Concluded.

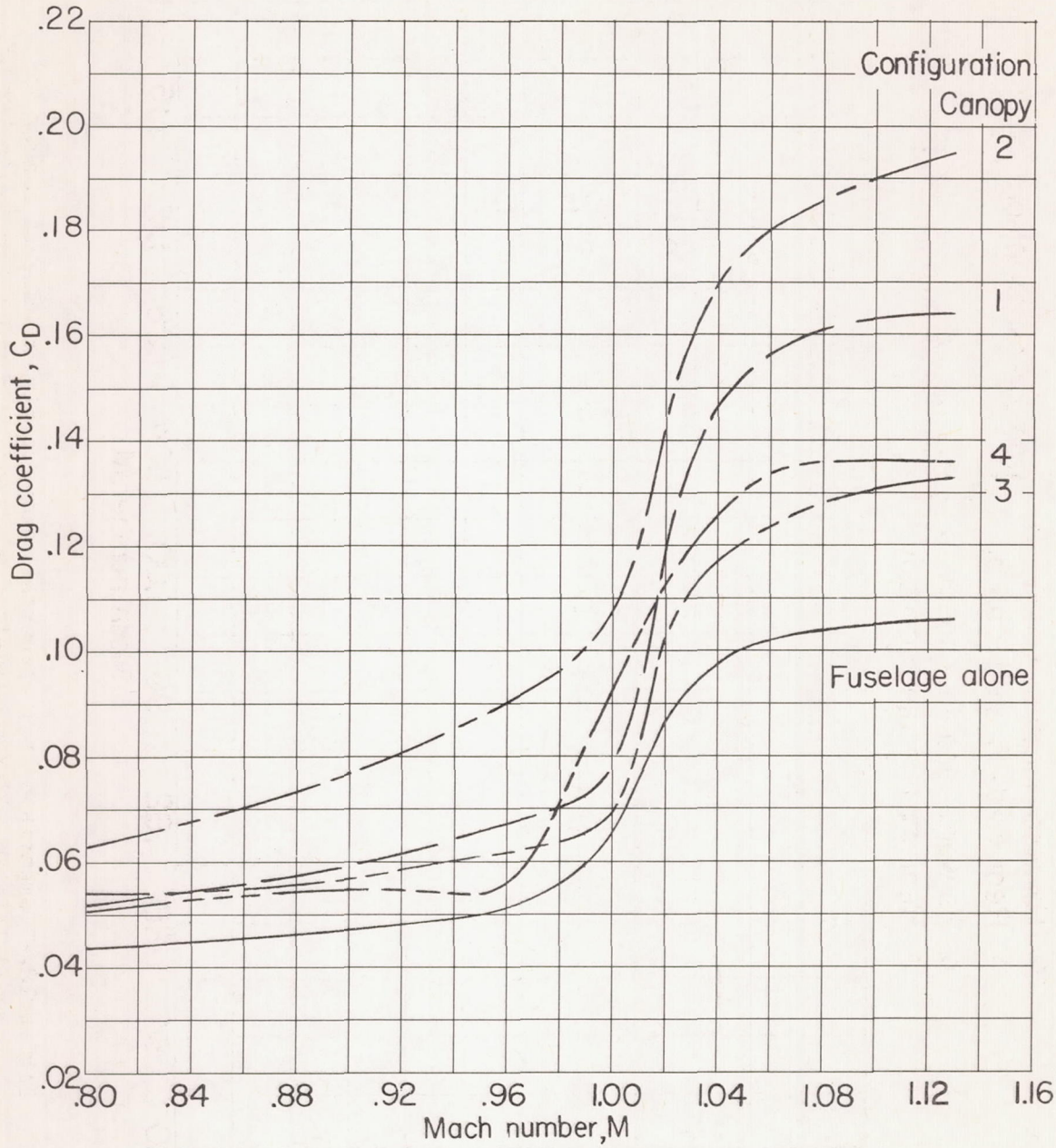


Figure 11.- Comparison of drag for the five models tested. $\alpha \approx 0^\circ$; $\beta = 0^\circ$.

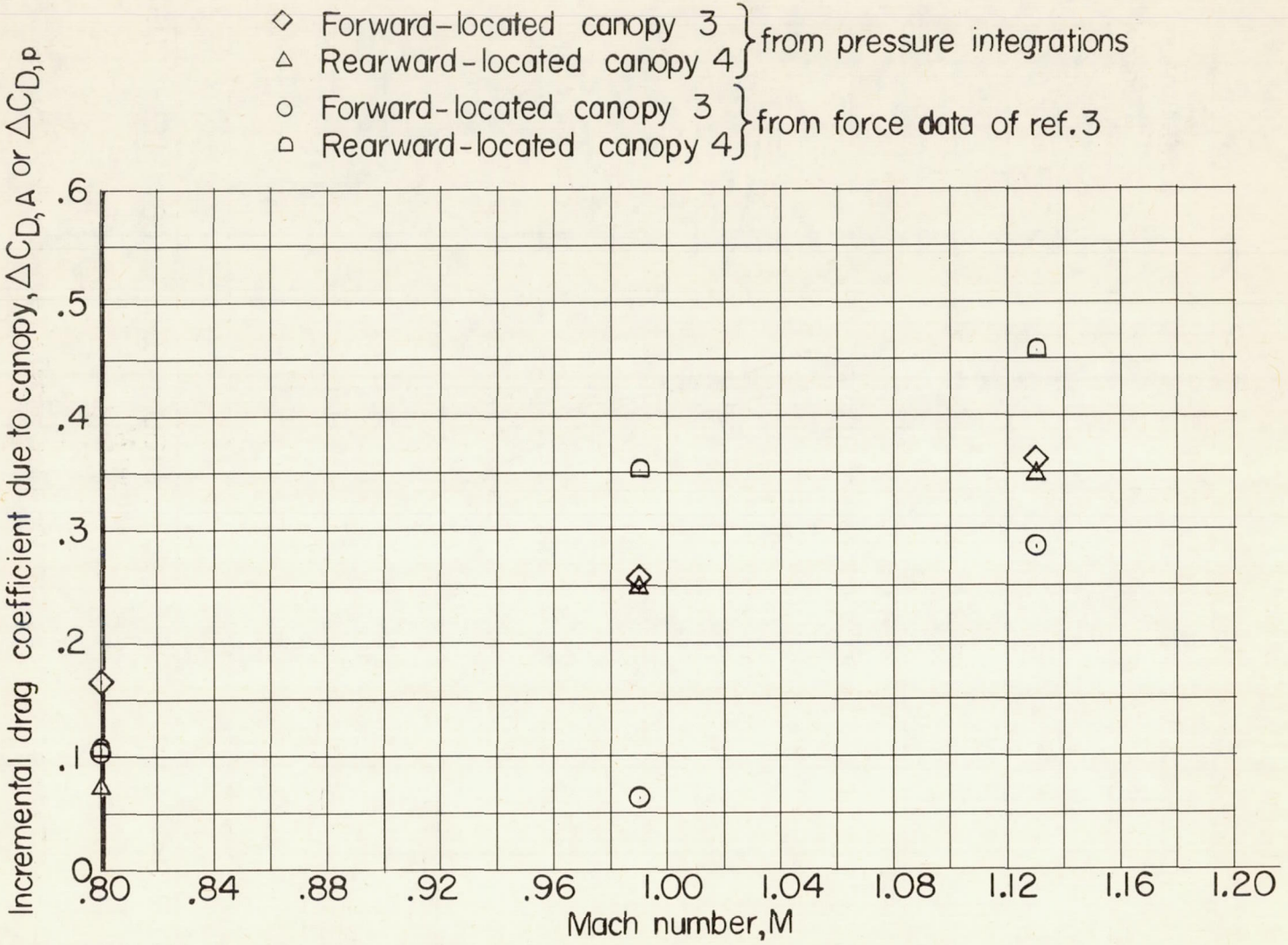


Figure 12.- Comparison of incremental drag coefficient due to canopy for forward-located and rearward-located canopies 3 and 4. $\alpha \approx 0^{\circ}$; $\beta \approx 0^{\circ}$.

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